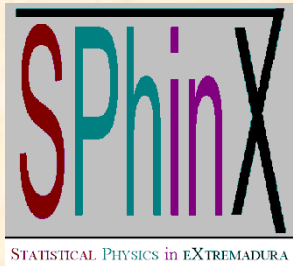


ENSKOG KINETIC THEORY FOR MONODISPERSE GRANULAR GASES



Vicente Garzó

Departamento de Física and Instituto de
Computación Científica Avanzada (ICCAEX),
Universidad de Extremadura, Badajoz, Spain

Rheology of disordered particles - suspensions, glassy and granular materials, June 2018, Kyoto

OUTLINE

1. *The model*: gas of hard spheres with *inelastic* collisions
2. *Enskog* kinetic equation for granular fluids.
Macroscopic balance equations
3. Homogeneous cooling state (**HCS**)
4. *Navier-Stokes* transport coefficients. Approximate methods
5. Comparison with *computer simulations*
6. Conclusions

Understanding the behavior of granular matter is a very relevant challenge, not only from a practical point of view but also from a more fundamental perspective.

Granular materials are ubiquitous both in nature and industry (second most used material after the water). They are also familiar to us in our daily lives (kitchen)

Behavior is extremely complex and sometimes *unexpected*



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THE MODEL

Granular matter: conglomeration of macroscopic discrete particles
(size around one micra) with **dissipative** interactions

Complex systems that are inherently **out** of equilibrium !!

Conventional methods of *equilibrium* statistical mechanics
and thermodynamics fail

Two states: compact and activated

Compact: grains form a *static* packed configuration within the container due to the combined effect of gravity and inelasticity in collisions

Any initial motion is quickly dissipated. Sugar or rice left *unshaken* in a jar appears to be inactive, although they have some kinetic energy due to the room temperature. However, their gravitational energy is much larger than their energy of motion

Problem: Stresses within the system and distribution of forces on the container (mitigate possible explosions in granular storage silos)

Activated: External energy compensates for the energy dissipated by collisions and effects of gravity

Rapid flow conditions: motion of grains is similar to motion of molecules or atoms in a classical gas. They behave like a fluid and flow. Hydrodynamic-like description. **Granular gas**

Kinetic theory does not make any assumption on the conservative or dissipative character of collisions. Appropriate tool !!

Transfer of momentum and energy is through *binary* collisions

Simplest microscopic model: *smooth inelastic hard spheres*

“*Smooth* hard spheres
with *inelastic* collisions”

$$\mathbf{V}_{12}^* \cdot \hat{\boldsymbol{\sigma}} = -\alpha \mathbf{V}_{12} \cdot \hat{\boldsymbol{\sigma}}$$

Coefficient of normal restitution

$$0 < \alpha \leq 1$$

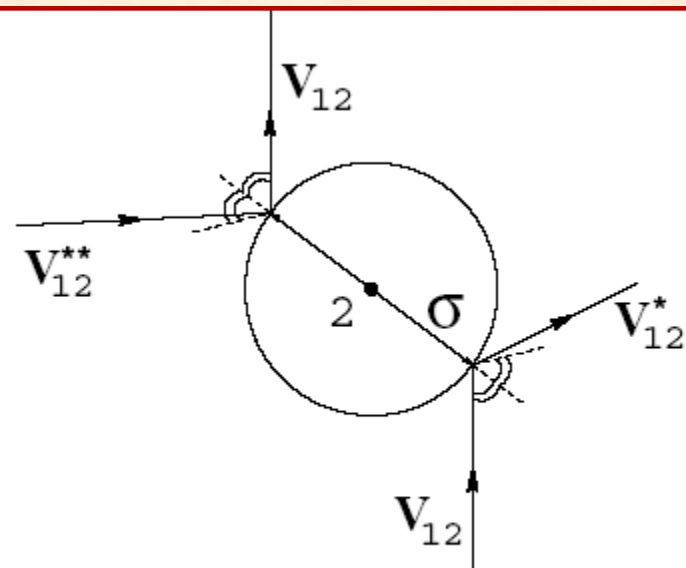


FIG. 1: Sketch of inelastic collisions (after T.P.C. van Noije & M.H. Ernst).

Direct collision: $(\mathbf{v}_1, \mathbf{v}_2) \rightarrow (\mathbf{v}'_1, \mathbf{v}'_2)$

Throughout the talk:

$$\mathbf{g}_{12} = \mathbf{v}_1 - \mathbf{v}_2$$

$$\mathbf{g}'_{12} = \mathbf{v}'_1 - \mathbf{v}'_2$$

$$(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}'_{12}) = -\alpha(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12})$$

Conservation of momentum: $\mathbf{v}_1 + \mathbf{v}_2 = \mathbf{v}'_1 + \mathbf{v}'_2$

$$\mathbf{v}'_1 = \mathbf{v}_1 - \frac{1}{2}(1 + \alpha)(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12})\hat{\boldsymbol{\sigma}}$$

$$\mathbf{v}'_2 = \mathbf{v}_2 + \frac{1}{2}(1 + \alpha)(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12})\hat{\boldsymbol{\sigma}}$$

Change in kinetic energy:

$$\Delta E \equiv E' - E = -\frac{m}{2}(\hat{\sigma} \cdot \mathbf{g}_{12})^2(1 - \alpha^2) \leq 0$$

Energy is lost in each collision, never gained

Restituting collisions: $(\mathbf{v}_1'', \mathbf{v}_2'') \rightarrow (\mathbf{v}_1, \mathbf{v}_2)$

$$(\hat{\sigma} \cdot \mathbf{g}_{12}'') = -\alpha^{-1}(\hat{\sigma} \cdot \mathbf{g}_{12})$$

$$d\mathbf{v}_1'' d\mathbf{v}_2'' = \alpha^{-1} d\mathbf{v}_1 d\mathbf{v}_2 \quad d\mathbf{v}_1' d\mathbf{v}_2' = \alpha d\mathbf{v}_1 d\mathbf{v}_2$$

KINETIC DESCRIPTION

One-particle velocity distribution function

$f(\mathbf{r}, \mathbf{v}, t) d\mathbf{r} d\mathbf{v} \rightarrow$ Average number of particles at t located around \mathbf{r} and moving with \mathbf{v}

Dilute gas: fraction of the volumen occupied by granular material is negligible compared to the total volume

Boltzmann kinetic equation

- *Dilute gas* (binary collisions)
- “*Molecular chaos*”

Rate of change of f with time:
$$\frac{\partial f}{\partial t} = \left(\frac{\partial f}{\partial t}\right)_{\text{str}} + \left(\frac{\partial f}{\partial t}\right)_{\text{coll}}$$

Interactions are absent (Knudsen gas):

$$\left(\frac{\partial f}{\partial t}\right)_{\text{str}} = -\mathbf{v} \cdot \nabla f - \frac{1}{m} \frac{\partial}{\partial \mathbf{v}} \cdot (\mathbf{F} f)$$


External force

Collisional change of $f(\mathbf{r}, \mathbf{v}_1, t) d\mathbf{r} d\mathbf{v}_1$ during $(t, t + dt)$

$$\left(\frac{\partial f}{\partial t}\right)_{\text{coll}} d\mathbf{v}_1 = (G - L) d\mathbf{v}_1$$

Gain term Loss term

Loss term $\longrightarrow (\mathbf{v}_1, \mathbf{v}_2) \rightarrow (\mathbf{v}'_1, \mathbf{v}'_2)$

Number of collisions per unit time into an element of solid angle between a beam of incident particles and a target particle

$$\sigma^{d-1} |(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12})| f(\mathbf{v}_1) d\hat{\boldsymbol{\sigma}} d\mathbf{v}_1$$

Since there is not only one target particle, then

$$\sigma^{d-1} |(\hat{\sigma} \cdot \mathbf{g}_{12})| f(\mathbf{v}_1) f(\mathbf{v}_2) d\hat{\sigma} d\mathbf{v}_1 d\mathbf{v}_2 dt$$

Average total number of collisions suffering particles with velocity \mathbf{V}_1

$$L d\mathbf{v}_1 = \sigma^{d-1} \int d\mathbf{v}_2 \int d\hat{\sigma} \Theta(\hat{\sigma} \cdot \mathbf{g}_{12}) (\hat{\sigma} \cdot \mathbf{g}_{12}) f(\mathbf{v}_1) f(\mathbf{v}_2) d\mathbf{v}_1$$

Gain term $\rightarrow (\mathbf{v}_1'', \mathbf{v}_2'') \rightarrow (\mathbf{v}_1, \mathbf{v}_2)$

$$G d\mathbf{v}_1 = \sigma^{d-1} \int d\mathbf{v}_2'' \int d\hat{\sigma} \Theta(\hat{\sigma} \cdot \mathbf{g}_{12}'') (\hat{\sigma} \cdot \mathbf{g}_{12}'') f(\mathbf{v}_1'') f(\mathbf{v}_2'') d\mathbf{v}_1''$$

$$\partial_t f + \mathbf{v} \cdot \nabla f + \frac{\partial}{\partial \mathbf{v}} \cdot \left(\frac{\mathbf{F}}{m} f \right) = J[\mathbf{v}|f(t), f(t)]$$

$$J[\mathbf{v}_1|f, f] = \sigma^{d-1} \int d\mathbf{v}_2 \int d\hat{\sigma} \Theta(\hat{\sigma} \cdot \mathbf{g}_{12}) (\hat{\sigma} \cdot \mathbf{g}_{12}) \\ \times \left[\alpha^{-2} f(\mathbf{r}, \mathbf{v}_1''; t) f(\mathbf{r}, \mathbf{v}_2''; t) - f(\mathbf{r}, \mathbf{v}_1; t) f(\mathbf{r}, \mathbf{v}_2; t) \right]$$

Collision rules:

$$\mathbf{v}_1'' = \mathbf{v}_1 - \frac{1}{2} (1 + \alpha^{-1}) (\hat{\sigma} \cdot \mathbf{g}_{12}) \hat{\sigma} \\ \mathbf{v}_2'' = \mathbf{v}_2 + \frac{1}{2} (1 + \alpha^{-1}) (\hat{\sigma} \cdot \mathbf{g}_{12}) \hat{\sigma}$$

Differences with elastic BE: Presence of α^{-2} in gain term and collision rules

ENSKOG KINETIC EQUATION

Extension of the BE *to moderate* densities. Mean free path is **NOT** much smaller than diameters of spheres

New ingredients

- Volume accesible per particle is smaller than that of a dilute gas. Probability of finding a particle at a given point is influenced by the presence of the remaining particles of the gas. Non-equilibrium pair correlation function
- The one- particle velocity distribution functions must be evaluated at

$$\mathbf{r}, \mathbf{r} \pm \hat{\sigma}$$

Limitation: Velocity correlations are still neglected
(*molecular chaos* hypothesis) !!

$$\partial_t f + \mathbf{v} \cdot \nabla f + \frac{\partial}{\partial \mathbf{v}} \cdot \left(\frac{\mathbf{F}}{m} f \right) = J_E [\mathbf{r}, \mathbf{v} | f(t), f(t)]$$

$$J_E(\mathbf{r}_1, \mathbf{v}_1; t) = \sigma^{d-1} \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} \Theta(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) (\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) \\ \times \left(\alpha^{-2} f_2(\mathbf{r}_1, \mathbf{v}_1'', \mathbf{r}_1 - \boldsymbol{\sigma}, \mathbf{v}_2''; t) - f_2(\mathbf{r}_1, \mathbf{v}_1, \mathbf{r}_1 + \boldsymbol{\sigma}, \mathbf{v}_2; t) \right)$$

$$f_2(\mathbf{r}_1, \mathbf{v}_1, \mathbf{r}_2, \mathbf{v}_2; t) = \chi(\mathbf{r}_1, \mathbf{r}_2) f(\mathbf{r}_1, \mathbf{v}_1; t) f(\mathbf{r}_2, \mathbf{v}_2; t)$$


Pair correlation function

Bad news for the Enskog equation (EE): Several MD simulations have shown that velocity correlations become *important* as density increases (McNamara&Luding, PRE (1998); Soto&Mareschal PRE (2001); Pagonabarraga et al. PRE (2002))

Good news for the EE: Good agreement at the level of *macroscopic* properties for moderate densities and finite dissipation
(**Simulations**: Brey et al., PF (2000) ; Lutsko, PRE (2001);
Dahl et al., PRE (2002); Lois et al. PRE (2007);
Bannerman et al., PRE (2009); Mitrano et al. PF (2011), PRE (2014)
Experiments: Yang et al., PRL (2002); PRE (2004))

I still think that the EE is *still* a valuable theory for granular fluids for *densities* beyond the Boltzmann limit and *dissipation* beyond the quasielastic limit.

Hydrodynamic fields

Number density $n(\mathbf{r}, t) = \int d\mathbf{v} f(\mathbf{r}, \mathbf{v}; t)$

Flow velocity $\mathbf{U}(\mathbf{r}, t) = \frac{1}{n(\mathbf{r}, t)} \int d\mathbf{v} \mathbf{v} f(\mathbf{r}, \mathbf{v}; t)$

Granular *temperature* $T(\mathbf{r}, t) = \frac{m}{dn(\mathbf{r}, t)} \int d\mathbf{v} [\mathbf{v} - \mathbf{U}(\mathbf{r}, t)]^2 f(\mathbf{r}, \mathbf{v}; t)$

MACROSCOPIC BALANCE EQUATIONS

$$I_\psi = \int d\mathbf{v}_1 \psi(\mathbf{v}_1) J_E(\mathbf{r}, \mathbf{v}_1 | f, f)$$

After some algebra.....

$$I_\psi = \frac{1}{2} \sigma^{d-1} \int d\mathbf{v}_1 \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} \Theta(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) (\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) \\ \times \left\{ \left[\psi(\mathbf{v}'_1) + \psi(\mathbf{v}'_2) - \psi(\mathbf{v}_1) - \psi(\mathbf{v}_2) \right] f_2(\mathbf{r}, \mathbf{v}_1, \mathbf{r} + \boldsymbol{\sigma}, \mathbf{v}_2; t) \right. \\ \left. + \nabla \cdot \boldsymbol{\sigma} \left[\psi(\mathbf{v}'_1) - \psi(\mathbf{v}_1) \right] \int_0^1 d\lambda f_2[\mathbf{r} - \lambda \boldsymbol{\sigma}, \mathbf{v}_1, \mathbf{r} + (1 - \lambda) \boldsymbol{\sigma}, \mathbf{v}_2; t] \right\}$$

Two contributions: (i) collisional effect due to scattering with a change in velocities;
(ii) pure collisional effect due to the spatial difference of the colliding pair

$$D_t n + n \nabla \cdot \mathbf{U} = 0$$

$$D_t \mathbf{U} + \rho^{-1} \nabla \cdot \mathbf{P} = \sigma_U$$

$$\frac{d}{2} n D_t T + \nabla \cdot \mathbf{q} + \mathbf{P} : \nabla \mathbf{U} = -\frac{d}{2} n T \zeta + \sigma_T$$

$$D_t \equiv \partial_t + \mathbf{U} \cdot \nabla$$

Production of momentum due to external force

$$\sigma_U = \int d\mathbf{v} \mathbf{F} f(\mathbf{v})$$

Production of energy due to external force

$$\sigma_T = \int d\mathbf{v} \mathbf{V} \cdot \mathbf{F} f(\mathbf{v}) \quad \mathbf{V} = \mathbf{v} - \mathbf{U}$$

Pressure tensor

Kinetic plus collisional contributions $\mathbf{P} = \mathbf{P}^k + \mathbf{P}^c$

$$\mathbf{P}^k = \int d\mathbf{v} m \mathbf{V} \mathbf{V} f(\mathbf{v})$$

$$\begin{aligned} \mathbf{P}^c = & \frac{1 + \alpha}{4} m \sigma^d \int d\mathbf{v}_1 \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} \Theta(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) (\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12})^2 \hat{\boldsymbol{\sigma}} \hat{\boldsymbol{\sigma}} \\ & \times \int_0^1 d\lambda \chi[\mathbf{r} - \lambda \boldsymbol{\sigma}, \mathbf{r} + (1 - \lambda) \boldsymbol{\sigma}] f(\mathbf{r} - \lambda \boldsymbol{\sigma}, \mathbf{v}_1; t) f[\mathbf{r} + (1 - \lambda) \boldsymbol{\sigma}, \mathbf{v}_2; t] \end{aligned}$$

Heat flux

$$\mathbf{q} = \mathbf{q}^k + \mathbf{q}^c$$

$$\mathbf{q}^k = \int d\mathbf{v} \frac{m}{2} V^2 \mathbf{V} f(\mathbf{v})$$

$$\begin{aligned} \mathbf{q}^c = & \frac{1 + \alpha}{4} m \sigma^d \int d\mathbf{v}_1 \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} \Theta(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) (\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12})^2 \hat{\boldsymbol{\sigma}} (\hat{\boldsymbol{\sigma}} \cdot \mathbf{G}_{12}) \\ & \times \int_0^1 d\lambda \chi[\mathbf{r} - \lambda \boldsymbol{\sigma}, \mathbf{r} + (1 - \lambda) \boldsymbol{\sigma}] f(\mathbf{r} - \lambda \boldsymbol{\sigma}, \mathbf{v}_1; t) f[\mathbf{r} + (1 - \lambda) \boldsymbol{\sigma}, \mathbf{v}_2; t] \end{aligned}$$

$$\mathbf{G}_{12} = \frac{\mathbf{V}_1 + \mathbf{V}_2}{2}$$

Collisional transfer contributions to fluxes vanish in the low-density limit but dominates at high density

Cooling rate

It provides the energy loss rate due to inelastic collisions.

It vanishes for elastic collisions

$$\zeta = (1 - \alpha^2) \frac{m\sigma^{d-1}}{4dnT} \int d\mathbf{v}_1 \int d\mathbf{v}_2 \int d\hat{\sigma} \Theta(\hat{\sigma} \cdot \mathbf{g}_{12}) (\hat{\sigma} \cdot \mathbf{g}_{12})^3 \\ \times \chi(\mathbf{r}, \mathbf{r} + \boldsymbol{\sigma}) f(\mathbf{r}, \mathbf{v}_1; t) f(\mathbf{r} + \boldsymbol{\sigma}, \mathbf{v}_2; t)$$

Macroscopic equations are *exact* within the Enskog equation

DILUTE GAS

$$\chi \rightarrow 1, \quad f(\mathbf{r} \pm \boldsymbol{\sigma}, \mathbf{v}; t) \simeq f(\mathbf{r}, \mathbf{v}; t)$$

$$\mathbf{P} \rightarrow \mathbf{P}^k \quad \mathbf{q} \rightarrow \mathbf{q}^k$$

$$\zeta = (1 - \alpha^2) \frac{m\sigma^{d-1}}{4dnT} \int d\mathbf{v}_1 \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} \Theta(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) (\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12})^3 f(\mathbf{r}, \mathbf{v}_1; t) f(\mathbf{r}, \mathbf{v}_2; t)$$

HOMOGENEOUS COOLING STATE

Spatially homogeneous isotropic time-dependent state

$$\frac{\partial}{\partial t} f(v; t) = \chi J_{\mathbf{B}}[\mathbf{v}|f, f]$$

Energy equation $\frac{\partial T}{\partial t} = -\zeta T$

Dimensional analysis shows that $\zeta(t) \propto \sqrt{T(t)}$

$$T(t) = \frac{T(0)}{\left(1 + \frac{1}{2}\zeta(0)t\right)^2}$$

Haff's cooling law (JFM 1983)

Since $T(t)$, the solution is not the local equilibrium distribution. Its explicit form is not known

However, for times longer than the mean free time it is expected that

$$f(v; t) = n v_{\text{th}}^{-d} \varphi \left(\frac{v}{v_{\text{th}}} \right), \quad v_{\text{th}}(t) = \sqrt{2T(t)/m}$$

In reduced units, the scaled distribution obeys the Boltzmann-Enskog equation

$$\frac{1}{2} \zeta^* \frac{\partial}{\partial \mathbf{c}} \cdot (\mathbf{c} \varphi) = J_{\text{B}}^*[\varphi, \varphi]$$

$$\zeta^* = \zeta / (\chi \nu), \quad \mathbf{c} = \mathbf{v} / v_{\text{th}}$$

Deviation of the scaled distribution with respect to its Gaussian form. Kurtosis

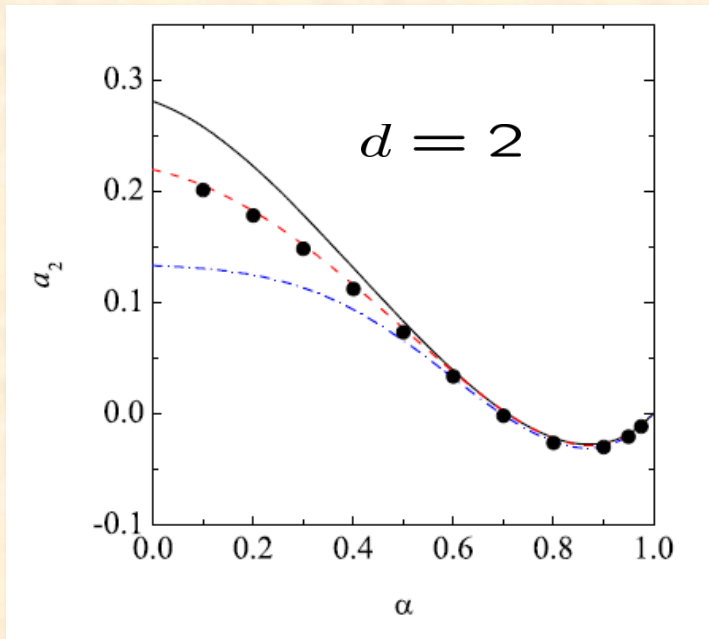
$$a_2 = \frac{\langle c^4 \rangle}{\langle c^4 \rangle_M} - 1$$

To get kurtosis one considers the leading term of the expansion of the scaled distribution in Sonine or Laguerre polynomials

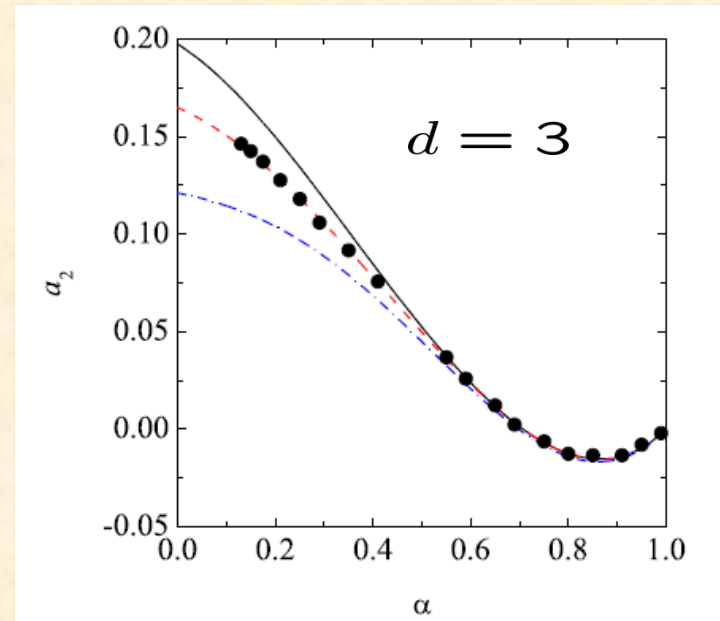
$$\varphi(c) \rightarrow \pi^{-d/2} e^{-c^2} \left[1 + \frac{a_2}{2} \left(c^4 - (d+2)c^2 + \frac{d(d+2)}{4} \right) \right]$$

Analytic expressions of kurtosis can be obtained by neglecting nonlinear terms

Comparison with DSMC simulations



Santos, Montanero GM **11**, 157 (2009)



Brilliantov, Pöschel, EPL **74**, 424 (2006)

Best accuracy:

$$a_2 = \frac{16(1 - \alpha)(1 - 2\alpha^2)}{25 + 24d - \alpha(57 - 8d) - 2(1 - \alpha)\alpha^2}$$

CHAPMAN-ENSKOG NORMAL SOLUTION

Assumption: For long times (much longer than the mean free time) and far away from boundaries (bulk region) the system reaches a *hydrodynamic* regime.

Normal solution $f(\mathbf{r}, \mathbf{v}; t) = f(\mathbf{v} | \{n(\mathbf{r}, t)\}, \mathbf{U}(\mathbf{r}, t), T(\mathbf{r}, t))$

In some situations, gradients are controlled by boundary or initial conditions. Small spatial gradients:

$$f = f^{(0)} + \epsilon f^{(1)} + \dots$$

The expansion generates a similar expansion for the fluxes and the cooling rate.
 In addition, the Enskog operator and the time derivatives are given by

$$J_E = J_E^{(0)} + \epsilon J_E^{(1)} + \dots, \quad \partial_t = \partial_t^{(0)} + \epsilon \partial_t^{(1)} + \dots$$

Time dependence is only through the hydrodynamic fields

$$\partial_t^{(k)} = (\partial_t^{(k)} n) \partial_n + (\partial_t^{(k)} U_i) \partial_{U_i} + (\partial_t^{(k)} T) \partial_T$$

From the balance equations

$$\partial_t^{(0)} n = \partial_t^{(0)} U_i = 0, \quad \partial_t^{(0)} T = -T \zeta^{(0)}$$

$$D_t^{(1)} n = -n \nabla \cdot \mathbf{U}, \quad D_t^{(1)} \mathbf{U} = -\rho^{-1} \nabla p + \mathbf{g}, \quad D_t^{(1)} T = -\frac{2}{d} T \nabla \cdot \mathbf{U} - T \zeta^{(1)}$$

$$D_t^{(1)} = \partial_t^{(1)} + \mathbf{U} \cdot \nabla$$

Some *controversy* about the possibility of going from kinetic theory to hydrodynamics by using the CE method

The **time scale** for T is set by the (inverse) **cooling rate** instead of spatial gradients. This new time scale, T is *much faster* than in the usual hydrodynamic scale. Some hydrodynamic excitations decay much slower than T

For **large inelasticity** (ζ^{-1} small), *perhaps* there were **NO** time scale separation between hydrodynamic and kinetic excitations:
NO AGING to hydrodynamics!!

We assume the validity of a hydrodynamic description and compare with computer simulations

Several first previous attempts to determine the Navier-Stokes transport coefficients

- C.K.K. Lun, S.B. Savage, D. J. Jeffrey, N. Chepuruiy, JFM **140**, 223 (1984)
- J. Jenkins, M. W. Richman, PF **28**, 3485 (1985)
- J. Jenkins, M. W. Richman, Arch. Ration.Mech.Anal. **87**, 355 (1985)
- A. Goldshtein, M. Shapiro, JFM **282**, 75 (1995)

Limitation: *Nearly* elastic spheres. Reference state is the Maxwell-Boltzmann distribution function. Solution to zeroth-order must not be chosen *a priori* and must be consistently obtained !!

ZERO-ORDER SOLUTION

$$\partial_t^{(0)} f^{(0)} = \chi J_B[f^{(0)}, f^{(0)}]$$

This equation has the same form as the EE for the HCS, but now the zeroth-order solution is a *local* HCS distribution

$$f^{(0)}(\mathbf{r}, \mathbf{v}; t) = n(\mathbf{r}, t) v_{\text{th}}(\mathbf{r}, t)^{-d} \varphi(c)$$

Normal solution: $\partial_t^{(0)} f^{(0)} = \partial_T f^{(0)} \partial_t^{(0)} T = -\zeta^{(0)} T \partial_T f^{(0)}$

$$\frac{1}{2} \zeta^{(0)} \frac{\partial}{\partial \mathbf{V}} \cdot (\mathbf{V} f^{(0)}) = \chi J_B[f^{(0)}, f^{(0)}]$$

The zeroth-order distribution is isotropic in velocity

$$\mathbf{q}^{(0)} = \mathbf{0}$$

$$P_{ij}^{(0)} = p\delta_{ij}, \quad p = nT \left[1 + 2^{d-2}(1 + \alpha)\phi\chi \right]$$

$$\zeta^{(0)} = \frac{\pi^{(d-1)/2}}{4d\Gamma\left(\frac{d+3}{2}\right)} (1-\alpha^2) \frac{m\sigma^{d-1}}{nT} \chi \int d\mathbf{v}_1 \int d\mathbf{v}_2 g_{12}^3 f^{(0)}(\mathbf{v}_1) f^{(0)}(\mathbf{v}_2)$$

Solid volume fraction

$$\phi = \frac{\pi^{d/2}}{2^{d-1}d\Gamma\left(\frac{d}{2}\right)} n\sigma^d$$

FIRST-ORDER SOLUTION

Motivation: determine the transport coefficients *without* limitation to the degree of dissipation

After some efforts....

$$\begin{aligned} \left(\partial_t^{(0)} + \mathcal{L} \right) f^{(1)} = & \mathbf{A}(\mathbf{V}) \cdot \nabla \ln T + \mathbf{B}(\mathbf{V}) \cdot \nabla \ln n \\ & + C_{ij}(\mathbf{V}) \frac{1}{2} \left(\frac{\partial U_i}{\partial r_j} + \frac{\partial U_j}{\partial r_i} - \frac{2}{d} \delta_{ij} \nabla \cdot \mathbf{U} \right) + \mathbf{D}(\mathbf{V}) \nabla \cdot \mathbf{U} \end{aligned}$$

Boltzmann-Enskog linearized operator

$$\mathcal{L}X = -\chi \left(J_{\mathbf{B}}[f^{(0)}, X] + J_{\mathbf{B}}[X, f^{(0)}] \right)$$

$$\mathbf{A}(\mathbf{V}|n, \mathbf{U}, T) = \frac{1}{2} \mathbf{V} \frac{\partial}{\partial \mathbf{V}} \cdot (\mathbf{V} f^{(0)}) - \frac{p}{\rho} \frac{\partial f^{(0)}}{\partial \mathbf{V}} + \frac{1}{2} \boldsymbol{\kappa} \left[\frac{\partial}{\partial \mathbf{V}} \cdot (\mathbf{V} f^{(0)}) \right]$$

$$\mathbf{B}(\mathbf{V}|n, \mathbf{U}, T) = -\mathbf{V} f^{(0)} - \frac{p}{\rho} \left(1 + \phi \frac{\partial \ln p^*}{\partial \phi} \right) \frac{\partial f^{(0)}}{\partial \mathbf{V}} - \left(1 + \frac{1}{2} \phi \frac{\partial \ln \chi}{\partial \phi} \right) \boldsymbol{\kappa} [f^{(0)}]$$

$$C_{ij}(\mathbf{V}|n, \mathbf{U}, T) = V_i \frac{\partial f^{(0)}}{\partial V_j} + \mathcal{K}_i \left[\frac{\partial f^{(0)}}{\partial V_j} \right]$$

$$D(\mathbf{V}|n, \mathbf{U}, T) = \frac{1-p^*}{d} \frac{\partial}{\partial \mathbf{V}} \cdot (\mathbf{V} f^{(0)}) + \frac{1}{d} \mathcal{K}_i \left[\frac{\partial f^{(0)}}{\partial V_i} \right] - \frac{1}{2} \zeta_U \frac{\partial}{\partial \mathbf{V}} \cdot (\mathbf{V} f^{(0)})$$

where $p^* \equiv p/(nT)$, $\zeta^{(1)} = \zeta_U \nabla \cdot \mathbf{U}$

$$\boldsymbol{\kappa}[X] = \sigma^d \chi \int d\mathbf{v}_2 \int d\hat{\boldsymbol{\sigma}} \Theta(\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) (\hat{\boldsymbol{\sigma}} \cdot \mathbf{g}_{12}) \hat{\boldsymbol{\sigma}} \left[\alpha^{-2} f^{(0)}(\mathbf{v}_1'') X(\mathbf{v}_2'') + f^{(0)}(\mathbf{v}_1) X(\mathbf{v}_2) \right]$$

The first-order solution has the form

$$f^{(1)} = \mathbf{A}(\mathbf{V}) \cdot \nabla \ln T + \mathbf{B}(\mathbf{V}) \cdot \nabla \ln n + c_{ij}(\mathbf{V}) \frac{1}{2} \left(\frac{\partial U_i}{\partial r_j} + \frac{\partial U_j}{\partial r_i} - \frac{2}{d} \delta_{ij} \nabla \cdot \mathbf{U} \right) + \mathcal{D}(\mathbf{V}) \nabla \cdot \mathbf{U}$$

To obtain the integral equations verifying the unknowns, one has to take into account

$$\partial_t^{(0)} \begin{pmatrix} \mathbf{A} \\ \mathbf{B} \end{pmatrix} = (\partial_t^{(0)} T) \partial_T \begin{pmatrix} \mathbf{A} \\ \mathbf{B} \end{pmatrix} = \frac{1}{2} \zeta^{(0)} \frac{\partial}{\partial \mathbf{V}} \cdot \begin{pmatrix} \mathbf{V} \mathbf{A} \\ \mathbf{V} \mathbf{B} \end{pmatrix}$$

$$\partial_t^{(0)} \begin{pmatrix} c_{ij} \\ \mathcal{D} \end{pmatrix} = (\partial_t^{(0)} T) \partial_T \begin{pmatrix} c_{ij} \\ \mathcal{D} \end{pmatrix} = \frac{1}{2} \zeta^{(0)} \begin{pmatrix} c_{ij} \\ \mathcal{D} \end{pmatrix} + \frac{1}{2} \zeta^{(0)} \frac{\partial}{\partial \mathbf{V}} \cdot \begin{pmatrix} \mathbf{V} c_{ij} \\ \mathbf{V} \mathcal{D} \end{pmatrix}$$

$$\partial_t^{(0)} \nabla \ln T = \nabla \left(T^{-1} \partial_t^{(0)} T \right) = -\zeta^{(0)} \left(1 + \phi \frac{\partial \ln \chi}{\partial \phi} \right) \nabla \ln n - \frac{1}{2} \zeta^{(0)} \nabla \ln T$$

Since the hydrodynamic gradients are *all* independent, then

$$\frac{1}{2}\zeta^{(0)}\frac{\partial}{\partial\mathbf{V}}\cdot(\mathbf{V}\mathcal{A}) - \frac{1}{2}\zeta^{(0)}\mathcal{A} + \mathcal{L}\mathcal{A} = \mathbf{A}$$

$$\frac{1}{2}\zeta^{(0)}\frac{\partial}{\partial\mathbf{V}}\cdot(\mathbf{V}\mathcal{B}) + \mathcal{L}\mathcal{B} = \mathbf{B} + \zeta^{(0)}\left(1 + \phi\frac{\partial\ln\chi}{\partial\phi}\right)\mathcal{A}$$

$$\frac{1}{2}\zeta^{(0)}\frac{\partial}{\partial\mathbf{V}}\cdot(\mathbf{V}C_{ij}) + \frac{1}{2}\zeta^{(0)}C_{ij} + \mathcal{L}C_{ij} = C_{ij}$$

$$\frac{1}{2}\zeta^{(0)}\frac{\partial}{\partial\mathbf{V}}\cdot(\mathbf{V}\mathcal{D}) + \frac{1}{2}\zeta^{(0)}\mathcal{D} + \mathcal{L}\mathcal{D} = \mathcal{D}$$

NAVIER-STOKES TRANSPORT COEFFICIENTS

$$P_{ij}^{(1)} = -\eta \left(\partial_j U_i + \partial_i U_j - \frac{2}{d} \delta_{ij} \nabla \cdot \mathbf{U} \right) - \delta_{ij} \eta_b \nabla \cdot \mathbf{U}$$

Shear viscosity

Bulk viscosity

$$\mathbf{q}^{(1)} = -\kappa \nabla T - \mu \nabla n$$

Thermal conductivity

Diffusive heat conductivity

Bulk viscosity has only *collisional* contributions

$$\eta_b = \frac{\pi^{(d-1)/2} d + 1}{\Gamma\left(\frac{d+3}{2}\right) 4d^2} m \sigma^{d+1} \chi (1 + \alpha) n^2 v_{\text{th}} I_\eta$$

$$I_\eta = \frac{1}{n^2 v_{\text{th}}} \int d\mathbf{v}_1 \int d\mathbf{v}_2 f^{(0)}(\mathbf{V}_1) f^{(0)}(\mathbf{V}_2) g_{12}$$

Shear viscosity $\eta = \eta_k + \eta_c$

$$\eta_c = \frac{2^{d-1}}{d+2} \phi \chi (1 + \alpha) \eta_k + \frac{d}{d+2} \eta_b$$

$$\eta_k = \frac{\eta_0}{\nu_\eta^* - \frac{1}{2} \zeta_0^*} \left[1 - \frac{2^{d-2}}{d+2} (1 + \alpha) (1 - 3\alpha) \phi \chi \right]$$

Shear viscosity of a low-density *elastic* gas of hard spheres

$$\eta_0 = \frac{(d+2)}{8} \frac{\Gamma\left(\frac{d}{2}\right)}{\pi^{(d-1)/2}} \sigma^{1-d} \sqrt{mT}$$

Solid volume fraction $\phi = \frac{\pi^{d/2}}{2^{d-1} d \Gamma\left(\frac{d}{2}\right)} n \sigma^d$

$$\zeta_0^* \equiv \zeta^{(0)} / \nu_0, \quad \nu_\eta^* \equiv \nu_\eta / \nu_0 \quad \nu_0 = nT / \eta_0$$

Effective collision frequency associated with momentum transport

$$\nu_\eta = \frac{\int d\mathbf{v} R_{ij}(\mathbf{V}) \mathcal{L} \mathcal{C}_{ij}(\mathbf{V})}{\int d\mathbf{v} R_{ij}(\mathbf{V}) \mathcal{C}_{ij}(\mathbf{V})}$$

$$R_{ij}(\mathbf{V}) = m \left(V_i V_j - \frac{1}{d} \delta_{ij} V^2 \right)$$

Thermal conductivity $\kappa = \kappa_k + \kappa_c$

$$\kappa_c = 3 \frac{2^{d-2}}{d+2} \phi \chi (1+\alpha) \kappa_k + \frac{\pi^{(d-1)/2}}{8d \Gamma\left(\frac{d+3}{2}\right)} \frac{m \sigma^{d+1} \chi}{T} (1+\alpha) n^2 v_{\text{th}}^3 I_\kappa$$

$$I_\kappa = \frac{1}{n^2 v_{\text{th}}^3} \int d\mathbf{v}_1 \int d\mathbf{v}_2 f^{(0)}(\mathbf{V}_1) f^{(0)}(\mathbf{V}_2) \left[g_{12}^{-1} (\mathbf{g}_{12} \cdot \mathbf{G}_{12})^2 + g_{12} G_{12}^2 + \frac{3}{2} g_{12} (\mathbf{g}_{12} \cdot \mathbf{G}_{12}) + \frac{1}{4} g_{12}^3 \right]$$

$$\kappa_k = \kappa_0 \frac{d-1}{d} (\nu_\kappa^* - 2\zeta_0^*)^{-1} \left\{ 1 + 2a_2 + 3 \frac{2^{d-3}}{d+2} \phi \chi (1+\alpha)^2 [2\alpha - 1 + a_2(1+\alpha)] \right\}$$

Thermal conductivity of a low-density *elastic* gas of elastic hard spheres

$$\kappa_0 = \frac{d(d+2)\eta_0}{2(d-1)m}$$

Effective collision frequency associated with energy transport

$$\nu_\kappa = \frac{\int d\mathbf{v} \mathbf{S}(\mathbf{V}) \cdot \mathcal{L} \mathcal{A}(\mathbf{V})}{\int d\mathbf{v} \mathbf{S}(\mathbf{V}) \cdot \mathcal{A}(\mathbf{V})}$$

$$\mathbf{S}(\mathbf{V}) = \left(\frac{1}{2} m V^2 - \frac{d+2}{2} T \right) \mathbf{V}$$

Heat diffusivity coefficient $\mu = \mu_k + \mu_c$

$$\mu_c = 3 \frac{2^{d-2}}{d+2} \phi \chi (1 + \alpha) \mu_k$$

$$\mu_k = 2 \frac{\kappa_0 T}{n} (2\nu_\mu^* - 3\zeta_0^*)^{-1} \left\{ \zeta_0^* \kappa_k^* \left(1 + \phi \frac{\partial \ln \chi}{\partial \phi} \right) + \frac{d-1}{d} a_2 - 3 \frac{2^{d-2} (d-1)}{d(d+2)} \phi \chi (1 + \alpha) \left(1 + \frac{1}{2} \phi \frac{\partial \ln \chi}{\partial \phi} \right) [\alpha(1 - \alpha) - \frac{a_2}{6} (10 + 2d - 3\alpha + 3\alpha^2)] \right\}$$

$$\nu_\mu = \frac{\int d\mathbf{v} \mathbf{S}(\mathbf{V}) \cdot \mathcal{L} \mathcal{B}(\mathbf{V})}{\int d\mathbf{v} \mathbf{S}(\mathbf{V}) \cdot \mathcal{B}(\mathbf{V})}$$

$$\kappa_k^* \equiv \kappa_k / \kappa_0$$

First-order contribution to the cooling rate

Up to first order in spatial gradients

$$\zeta = \zeta^{(0)} + \zeta_U \nabla \cdot \mathbf{U}$$

$$\zeta_U = -\frac{3}{4d} 2^d \phi \chi (1 - \alpha^2) + \frac{\pi^{(d-1)/2}}{2d \Gamma\left(\frac{d+3}{2}\right)} (1 - \alpha^2) \frac{m \sigma^{d-1} \chi}{nT} \int d\mathbf{v}_1 \int d\mathbf{v}_2 f^{(0)}(\mathbf{V}_1) \mathcal{D}(\mathbf{V}_2) g_{12}^3$$

Dilute gas expressions: $\phi \rightarrow 0, \quad \chi \rightarrow 1$

$$\eta = \frac{\eta_0}{\nu_{\eta}^* - \frac{1}{2}\zeta_0^*}$$

$$\kappa = \frac{d-1}{d} \frac{\kappa_0}{\nu_{\kappa}^* - 2\zeta_0^*} (1 + 2a_2)$$

$$\mu = 2 \frac{\frac{T}{n} \zeta_0^* \kappa + \frac{d-1}{d} \kappa_0 a_2}{2\nu_{\mu}^* - 3\zeta_0^*}$$

Brey, Dufty, Kim, Santos PRE **58**, 4638 (1998)

So far, all the results are formally *exact* !!

However, transport coefficients given in terms of

$$\left\{ \zeta_0^*, a_2, I_\eta, I_\kappa, \nu_\eta^*, \nu_\kappa^*, \nu_\mu^* \right\}$$

.....whose forms are not exactly known !!!

In the case of the zeroth-order distribution, one takes the leading term in a Sonine polynomial expansion. In this case,

$$\zeta_0^* = \frac{d+2}{4d} \chi(1-\alpha^2) \left(1 + \frac{3}{16}a_2\right)$$

$$a_2 = \frac{16(1-\alpha)(1-2\alpha^2)}{25 + 24d - \alpha(57 - 8d) - 2(1-\alpha)\alpha^2}$$

$$I_\eta = \sqrt{2} \frac{\Gamma\left(\frac{d+1}{2}\right)}{\Gamma\left(\frac{d}{2}\right)} \left(1 - \frac{a_2}{16}\right), \quad I_\kappa = \sqrt{2} \frac{\Gamma\left(\frac{d+3}{2}\right)}{\Gamma\left(\frac{d}{2}\right)} \left(1 + \frac{7}{16}a_2\right)$$

The knowledge of the effective collision frequencies requires to solve linear integral equations. To get explicit results, one has to resort to some approximations.

Standard first Sonine approximation

Method used in ordinary gases: truncate the Sonine polynomial expansion of the unknowns after the first term

$$\begin{pmatrix} \mathcal{A}(\mathbf{V}) \\ \mathcal{B}(\mathbf{V}) \\ C_{ij}(\mathbf{V}) \end{pmatrix} \rightarrow -f_M(\mathbf{V}) \begin{pmatrix} \frac{2}{d+2} \frac{m}{nT^2} \kappa_k \mathbf{S}(\mathbf{V}) \\ \frac{2}{d+2} \frac{m}{nT^2} \mu_k \mathbf{S}(\mathbf{V}) \\ \frac{\eta_k}{nT^2} R_{ij}(\mathbf{V}) \end{pmatrix}$$

Maxwellian distribution

Modified first Sonine approximation

Non-Gaussian properties of the zeroth-order distribution might be relevant for strong dissipation. Possible source of discrepancy between theory and simulations.

Alternative route to the standard method: replace Maxwellian distribution by the HCS distribution

$$\begin{pmatrix} \mathcal{A}(\mathbf{V}) \\ \mathcal{B}(\mathbf{V}) \\ \mathcal{C}_{ij}(\mathbf{V}) \end{pmatrix} \rightarrow -f^{(0)}(\mathbf{V}) \begin{pmatrix} \frac{2}{d+2} \frac{m}{nT^2} \frac{\kappa_k}{1 + \frac{d+8}{2} a_2} \left(\mathbf{S} - \frac{d+2}{2} a_2 T \mathbf{V} \right) \\ \frac{2}{d+2} \frac{m}{nT^2} \frac{\mu_k}{1 + \frac{d+8}{2} a_2} \left(\mathbf{S} - \frac{d+2}{2} a_2 T \mathbf{V} \right) \\ \frac{1}{1 + a_2} \frac{\eta_k}{nT^2} R_{ij} \end{pmatrix}$$

HCS distribution

Table 3.1 Explicit expressions of the Navier–Stokes transport coefficients

$$\begin{aligned}\eta &= \eta_k \left[1 + \frac{2^{d-1}}{d+2} \phi \chi (1 + \alpha) \right] + \frac{d}{d+2} \eta_b, \\ \eta_k &= \left(v_\eta^* - \frac{1}{2} \zeta_0^* \right)^{-1} \left[1 - \frac{2^{d-2}}{d+2} (1 + \alpha) (1 - 3\alpha) \phi \chi \right] \eta_0, \\ \eta_b &= \frac{2^{2d+1}}{\pi(d+2)} \phi^2 \chi (1 + \alpha) \left(1 - \frac{a_2}{16} \right) \eta_0, \\ \kappa &= \kappa_k \left[1 + 3 \frac{2^{d-2}}{d+2} \phi \chi (1 + \alpha) \right] + \frac{2^{2d+1}(d-1)}{(d+2)^2 \pi} \phi^2 \chi (1 + \alpha) \left(1 + \frac{7}{16} a_2 \right) \kappa_0, \\ \kappa_k &= \frac{d-1}{d} \left(v_\kappa^* - 2 \zeta_0^* \right)^{-1} \left\{ 1 + 2a_2 + 3 \frac{2^{d-3}}{d+2} \phi \chi (1 + \alpha)^2 [2\alpha - 1 + a_2(1 + \alpha)] \right\} \kappa_0, \\ \mu &= \mu_k \left[1 + 3 \frac{2^{d-2}}{d+2} \phi \chi (1 + \alpha) \right], \\ \mu_k &= \frac{2T}{n} \left(2v_\mu^* - 3\zeta_0^* \right)^{-1} \left\{ \zeta_0^* \kappa_k^* \left(1 + \phi \frac{\partial \ln \chi}{\partial \phi} \right) + \frac{d-1}{d} a_2 - 3 \frac{2^{d-2}(d-1)}{d(d+2)} \phi \chi (1 + \alpha) \right. \\ &\quad \left. \times \left(1 + \frac{1}{2} \phi \frac{\partial \ln \chi}{\partial \phi} \right) \left[\alpha(1 - \alpha) - \frac{a_2}{6} (10 + 2d - 3\alpha + 3\alpha^2) \right] \right\} \kappa_0.\end{aligned}$$

Standard first Sonine approximation

$$\begin{aligned}v_\eta^* &= \frac{3}{4d} \chi \left(1 - \alpha + \frac{2}{3} d \right) (1 + \alpha) \left(1 - \frac{a_2}{32} \right), \\ v_\kappa^* = v_\mu^* &= \frac{1 + \alpha}{d} \chi \left[\frac{d-1}{2} + \frac{3}{16} (d+8)(1 - \alpha) + \frac{4 + 5d - 3(4-d)\alpha}{512} a_2 \right].\end{aligned}$$

Modified first Sonine approximation

$$\begin{aligned}v_\eta^* &= \frac{3}{4d} \chi \left(1 - \alpha + \frac{2}{3} d \right) (1 + \alpha) \left(1 + \frac{7}{16} a_2 \right), \\ v_\kappa^* = v_\mu^* &= \frac{1 + \alpha}{d} \chi \left[\frac{d-1}{2} + \frac{3}{16} (d+8)(1 - \alpha) + \frac{296 + 217d - 3(160 + 11d)\alpha}{256} a_2 \right].\end{aligned}$$

Computer-aided method

Method developed by Noskowicz, Bar-Lev, Serero, and Goldhirsch,
EPL **79**, 60001 (2007)

Modern symbolic manipulators can be employed to obtain accurate estimates of the transport coefficients. Restricted to *dilute* gases.

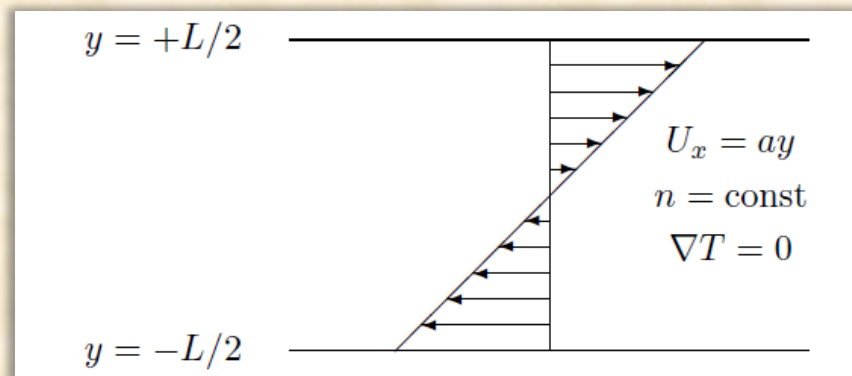
Unknowns are expanded in powers of Sonine polynomials but using a *wrong* temperature. It avoids possible divergence of the Sonine expansion

Limitation: one has to numerically solve a system of algebraic equations

COMPARISON WITH COMPUTER SIMULATIONS

Shear viscosity of a moderate dense granular gas

Simple or uniform shear flow (USF)



The USF state is quite different in ordinary and granular fluids. For **elastic** collisions, temperature increases in time due to viscous heating term. This effect can be controlled by the introduction of a *thermostat*. However, in the absence of thermostat, the **reduced** shear rate tends to zero for long times

$$a^*(t) = \lim_{t \rightarrow \infty} \frac{a}{\nu(t)} \rightarrow 0, \quad \nu(t) \propto \sqrt{T(t)}$$

Thus, viscous heating effect can be employed to measure the NS shear viscosity of hard spheres (Naito and Ono, J. Chem. Phys. **70**, 4515 (1979))

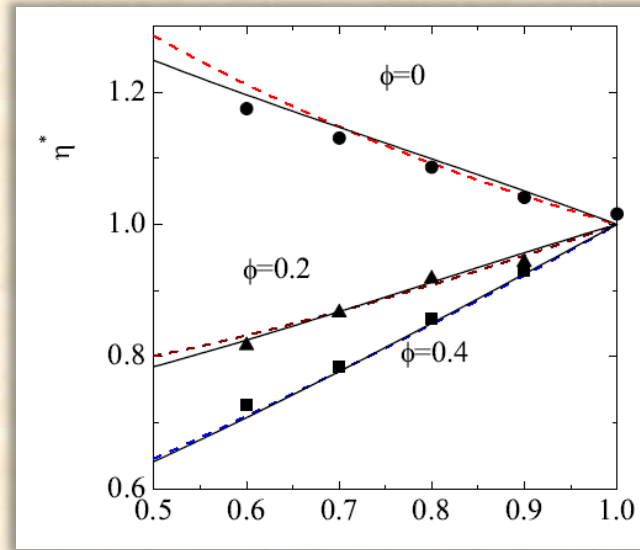
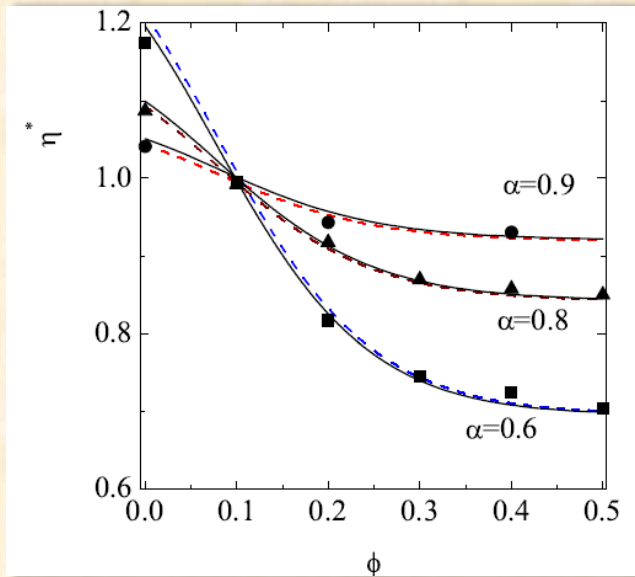
One is tempted to do the same for granular fluids but.....unfortunately viscous heating is compensated by collisional cooling and a **steady** state is achieved

Strategy for measuring shear viscosity of a granular fluid. We consider the USF state modified by the introduction of **two** different terms:

- A deterministic external “friction” (drag) force with negative friction coefficient to compensate for collisional dissipation .
- A stochastic process to mimic the conditions appearing in the Chapman-Enskog solution.

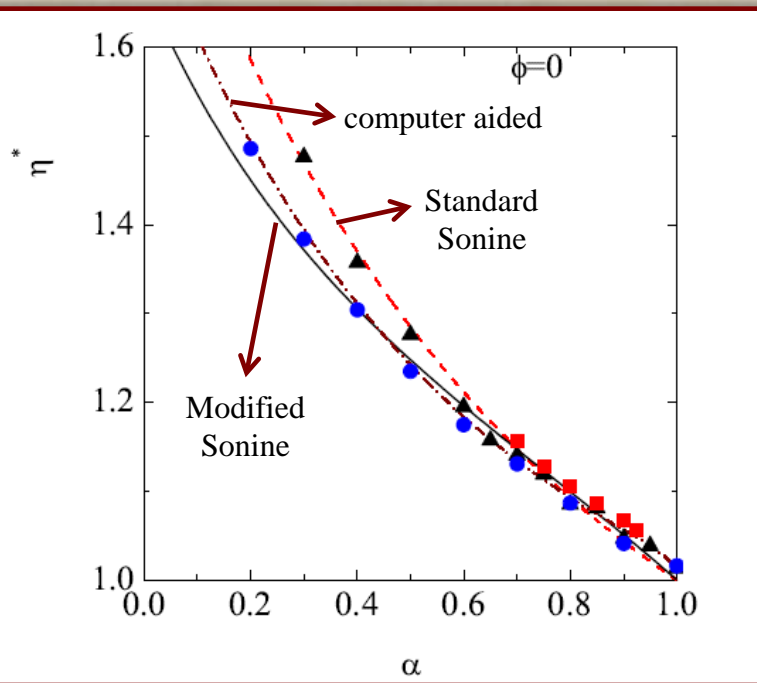
Montanero, Santos and Garzó, AIP Conf. Proc. **762**, 797 (2005)

DSMC method (Monte Carlo simulations)



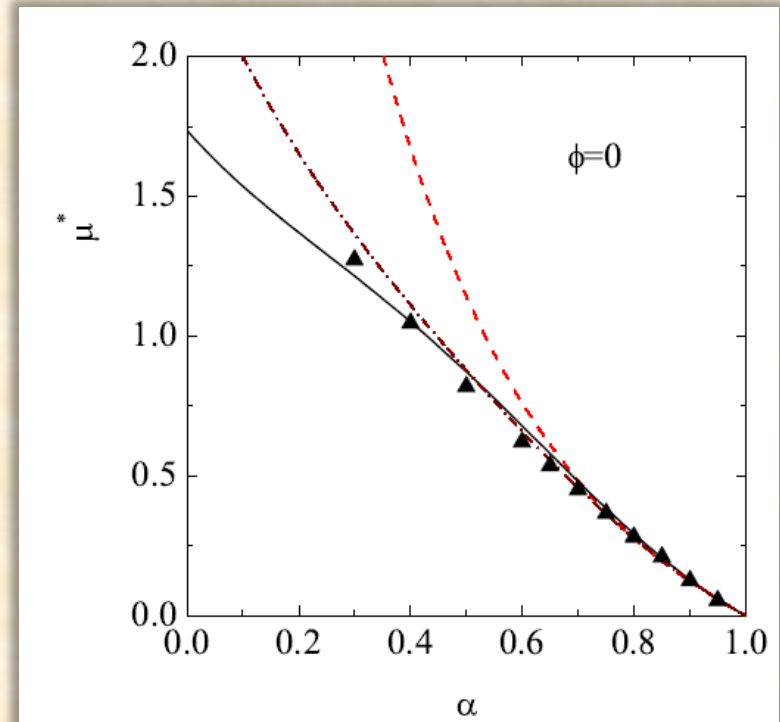
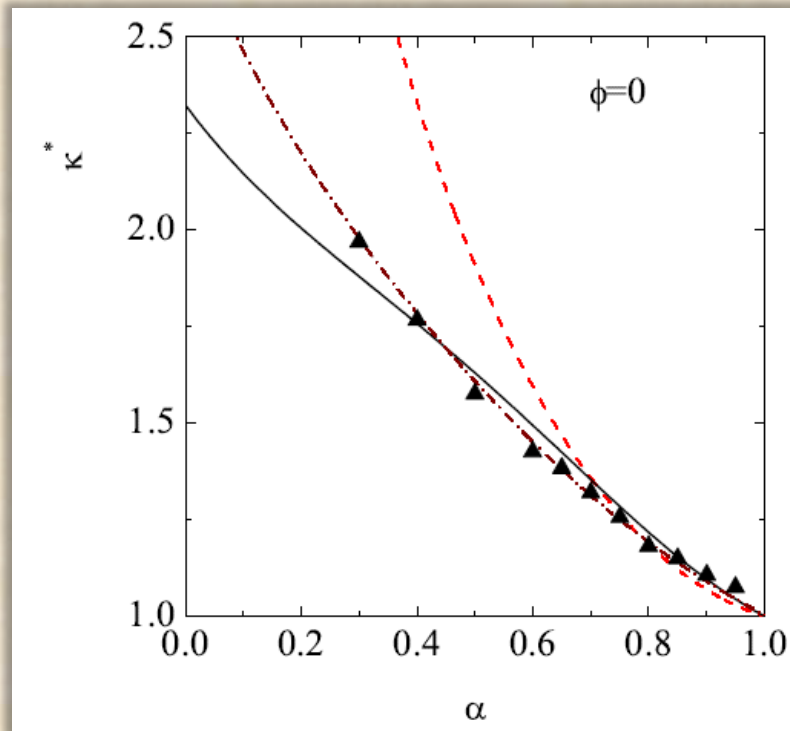
$$\eta^*(\alpha, \phi) \equiv \frac{\eta(\alpha, \phi)}{\eta(1, \phi)}$$

Dilute gases: three alternative methods



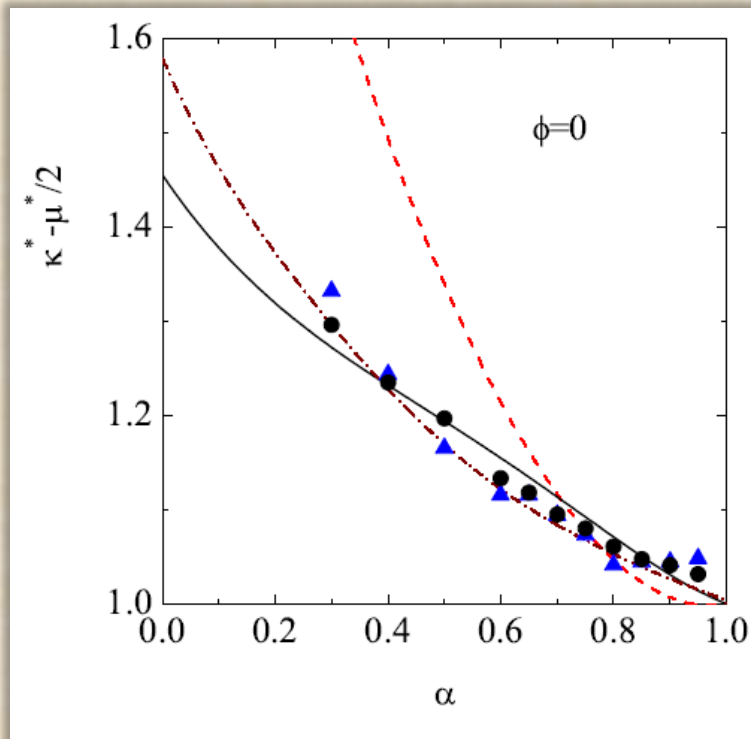
- Green-Kubo formula for two-time correlation functions.
DSMC simulations by
Brey et al. PRE **70**,051301 (2004);
J.Phys.:Condens. Matter **17**, S2489 (2005)
(triangles)
- Decay of a sinusoidal perturbation.
Brey et al., EPL **48**, 359 (1999)
(squares)
- Application of external force to USF.
Montanero et al. (2005) (circles)

Heat flux transport coefficients



$$\kappa^*(\alpha, 0) \equiv \frac{\kappa(\alpha, 0)}{\kappa(1, 0)}$$

$$\mu^*(\alpha, 0) \equiv \frac{n\mu(\alpha, 0)}{T\kappa_0}$$



DSMC simulations:
 (1) Green-Kubo relations,
 Brey et. al, 2004 (triangles);
 (2) External force, Montanero, Santos, Garz3
 Physica A **376** , 75 (2007) (circles)

CONCLUSIONS

- ✓ Hydrodynamic equations have been *exactly* derived from Enskog kinetic theory. They appear to be a powerful tool for analysis and predictions of rapid flow gas dynamics at *moderate* densities.
- ✓ A *normal* solution to the Enskog equation has been then obtained for states close to the HCS. *Navier-Stokes* transport coefficients and cooling rate have been *exactly* given in terms of solutions of a set of coupled linear integral equations
- ✓ *Approximate* forms for the transport coefficients have been obtained by three different methods: (i) *standard* first-Sonine solution, (ii) *modified* first-Sonine solution, and (iii) *computer-aided* method

CONCLUSIONS

- ✓ Theoretical results have been compared against **two** types of simulations: **DSMC** (to confirm approximations to the kinetic equation) and **MD** (to confirm results beyond kinetic theory limitations)
- ✓ In general, the agreement between theory and simulations is very good, even for moderately dense systems and strong collisional dissipation
- ✓ The above good agreement encourages the use of kinetic theory as a reliable and accurate tool to reproduce the trends observed in granular flows, specially those related to collisional dissipation

UEx (Spain)

- José María Montanero
- Andrés Santos

External collaborations

- James W. Dufty (University of Florida, USA)

<http://www.eweb.unex.es/eweb/fisteor/vicente/>

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Rheology of disordered particles - suspensions, glassy and granular materials, June 2018, Kyoto

