

Anisotropy of sheared dense suspensions: normal stress differences and microstructure

Ryohei Seto

Kyoto University, Dept. of Chemical Engineering

Giulio G. Giusteri
Politecnico di Milano

Seto and Giusteri, [arXiv:1806.09423](https://arxiv.org/abs/1806.09423)



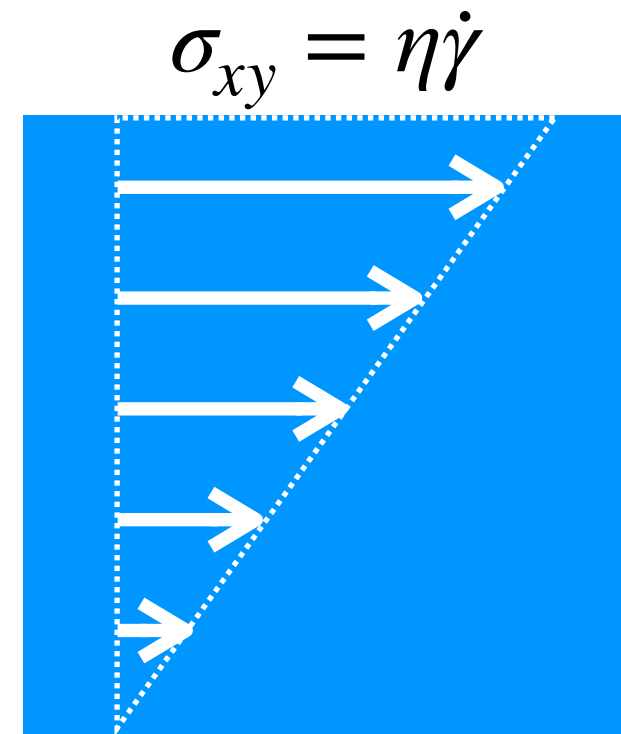
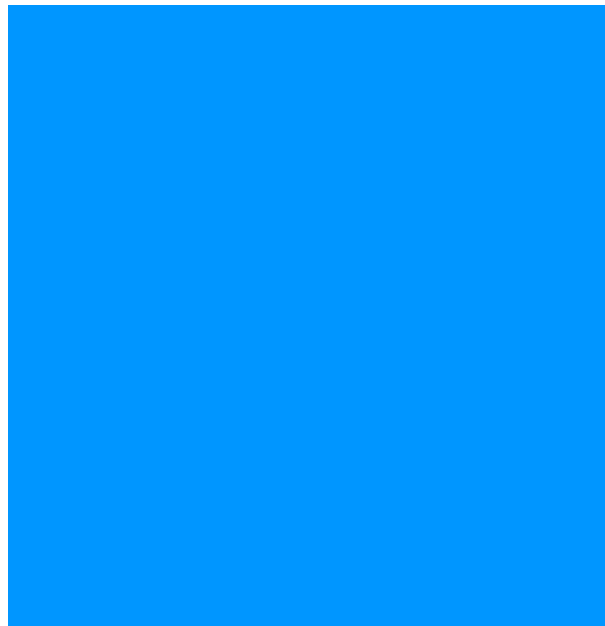
Newtonian fluids...



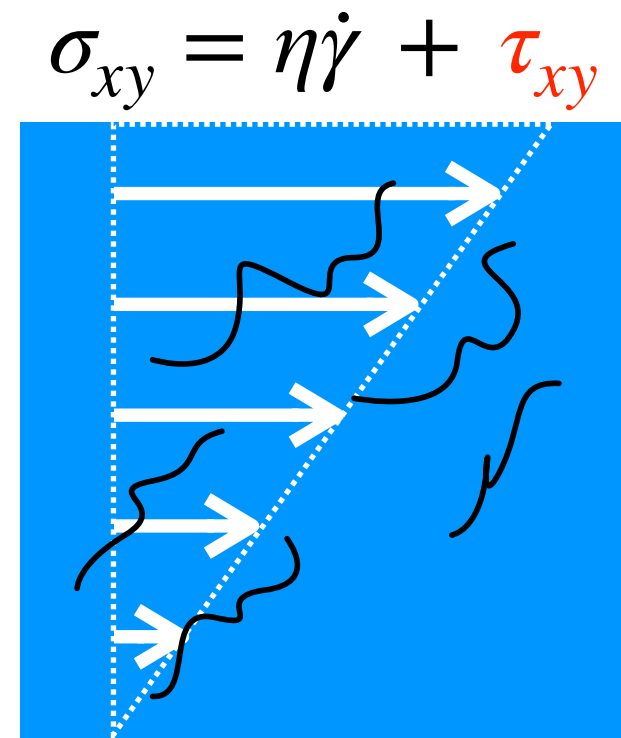
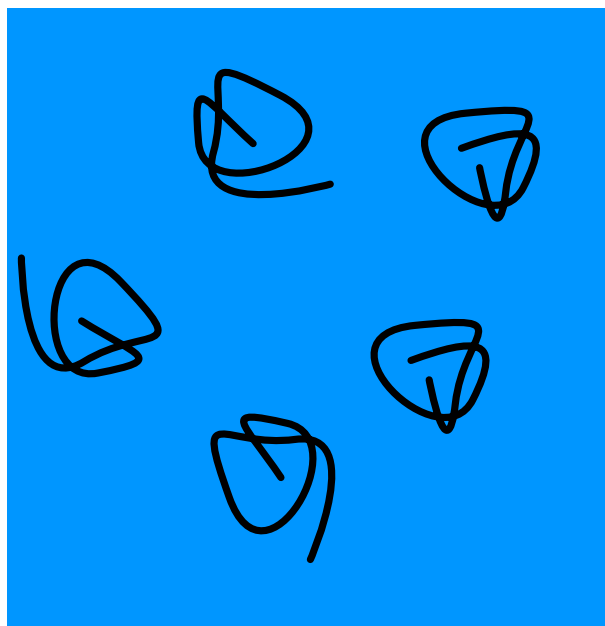
$$\rho \left[\frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right] = \nabla \cdot \boldsymbol{\sigma} \text{ with } \nabla \cdot \mathbf{u} = 0$$

$$\boldsymbol{\sigma} = -p\mathbf{I} + 2\eta \mathbf{D} \quad \mathbf{D} \equiv \frac{1}{2}(\nabla \mathbf{v} + \nabla \mathbf{v}^T)$$

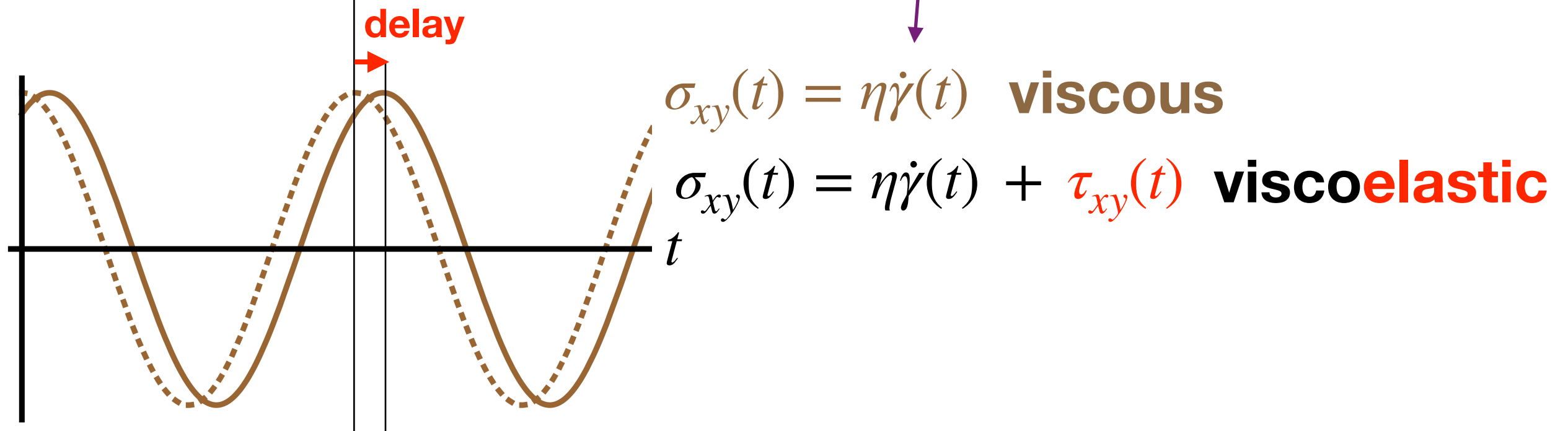
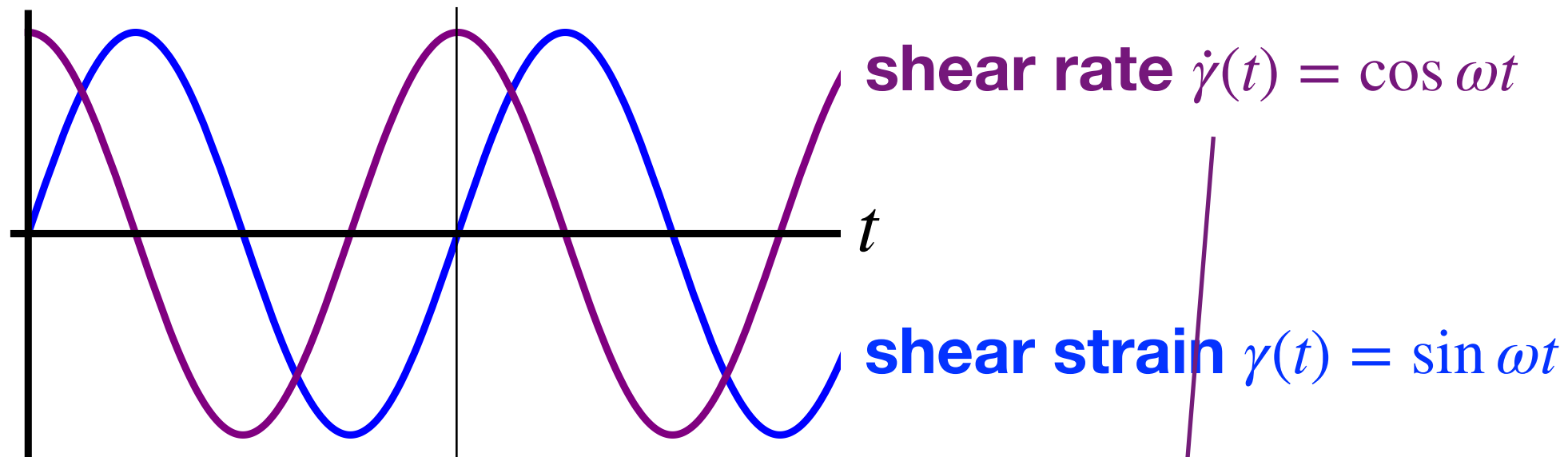
Newtonian liquid



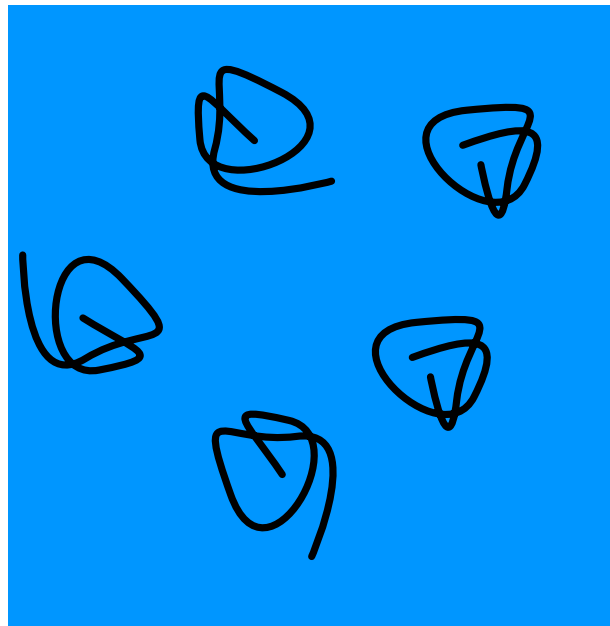
**Newtonian liquid
+ elastic chains**



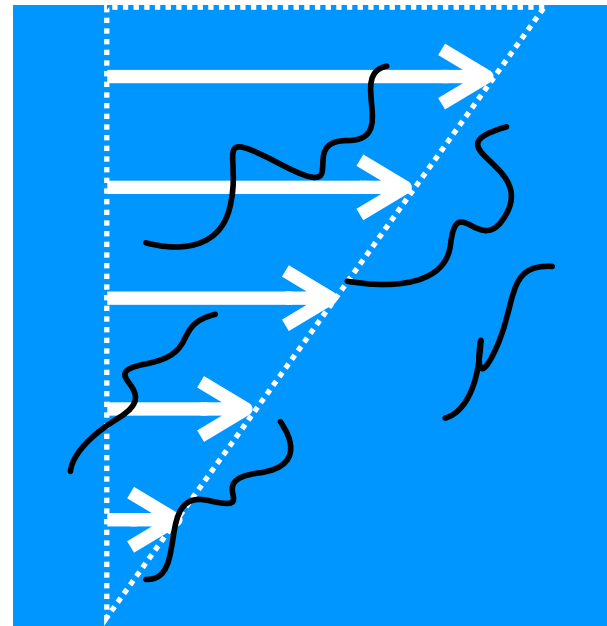
Oscillatory rheology

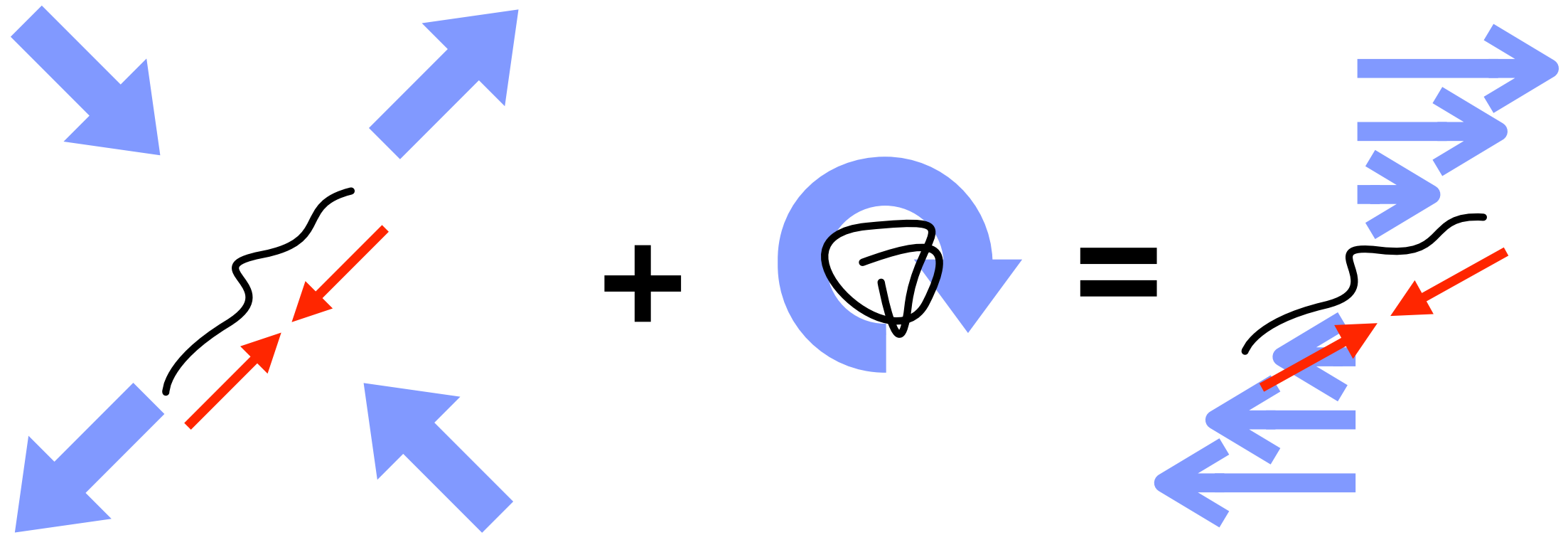


Can we distinguish them by ***steady shear*** rheology?



$$\sigma_{xy} = \eta \dot{\gamma} + \tau_{xy}$$





Stress “tensor” (not only σ_{xy})

$$\boldsymbol{\sigma} = -p\mathbf{I} + 2\eta\mathbf{D} + \boldsymbol{\tau}_{\text{elastic}}$$

$$\sigma_{xx} > \sigma_{yy}$$

i.e. $N_1 \equiv \sigma_{xx} - \sigma_{yy} > 0$

note: Contributions from stretched chains are positive: $\sigma_{xx} > 0$, $\sigma_{yy} > 0$

Viscometric functions

simple shear flow



stress tensor

$$\nabla \mathbf{u} = \begin{pmatrix} 0 & \dot{\gamma} & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} = \mathbf{D} + \mathbf{W}$$

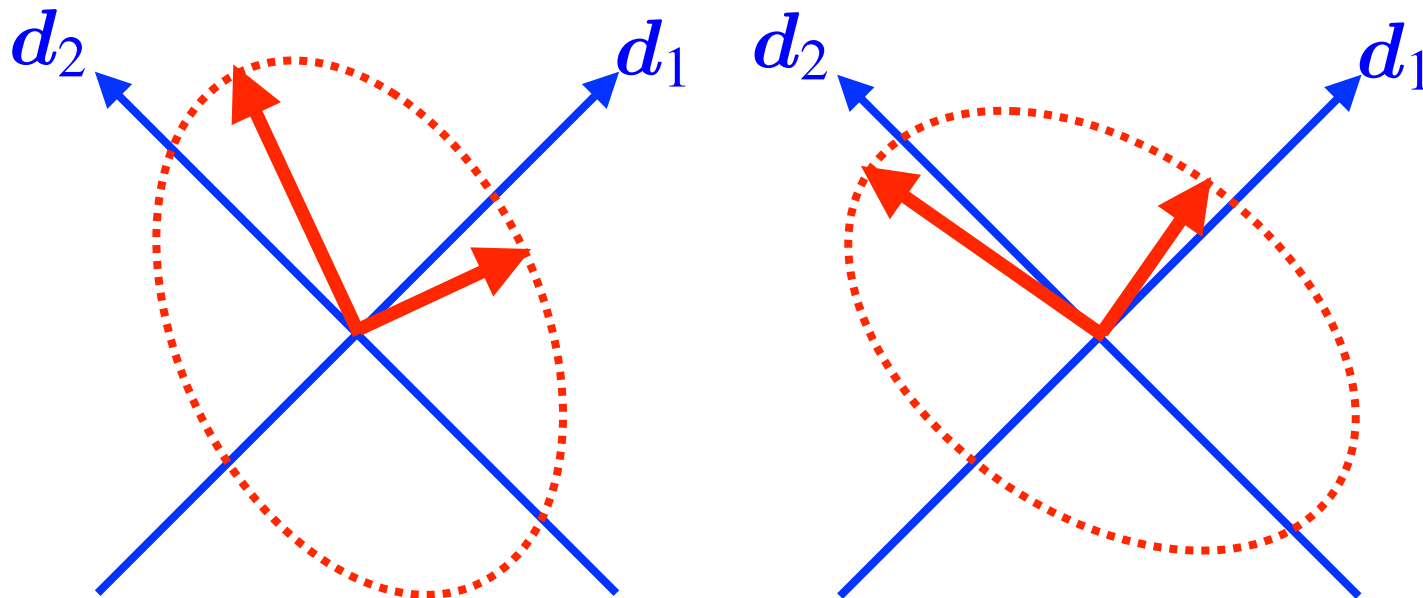
$$\boldsymbol{\sigma} = \begin{pmatrix} \sigma_{xx} & \sigma_{xy} & 0 \\ \sigma_{xy} & \sigma_{yy} & 0 \\ 0 & 0 & \sigma_{zz} \end{pmatrix}$$

$$\mathbf{D} = \begin{pmatrix} 0 & \dot{\gamma}/2 & 0 \\ \dot{\gamma}/2 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \quad \mathbf{W} = \begin{pmatrix} 0 & \dot{\gamma}/2 & 0 \\ -\dot{\gamma}/2 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

viscometric functions

$$\begin{cases} \eta \equiv \sigma_{xy}/\dot{\gamma} \\ N_1 \equiv \sigma_{xx} - \sigma_{yy} \\ N_2 \equiv \sigma_{yy} - \sigma_{zz} \end{cases}$$

$$p \equiv -\frac{1}{3} \text{Tr } \boldsymbol{\sigma}$$



$$N_1 > 0$$

$$N_1 < 0$$

Characterization with different flows

(Fluids may behave differently in different flows)

planar extensional flow



stress tensor

$$\nabla \mathbf{u} = \begin{pmatrix} \dot{\epsilon} & 0 & 0 \\ 0 & -\dot{\epsilon} & 0 \\ 0 & 0 & 0 \end{pmatrix} = \mathbf{D}$$

$$\boldsymbol{\sigma} = \begin{pmatrix} -p + A & 0 & 0 \\ 0 & -p + B & 0 \\ 0 & 0 & -p - (A + B) \end{pmatrix}$$

**2 components:
viscosity**

**+ anisotropy due to
the planarity of the flow**

uniaxial extensional flow



stress tensor

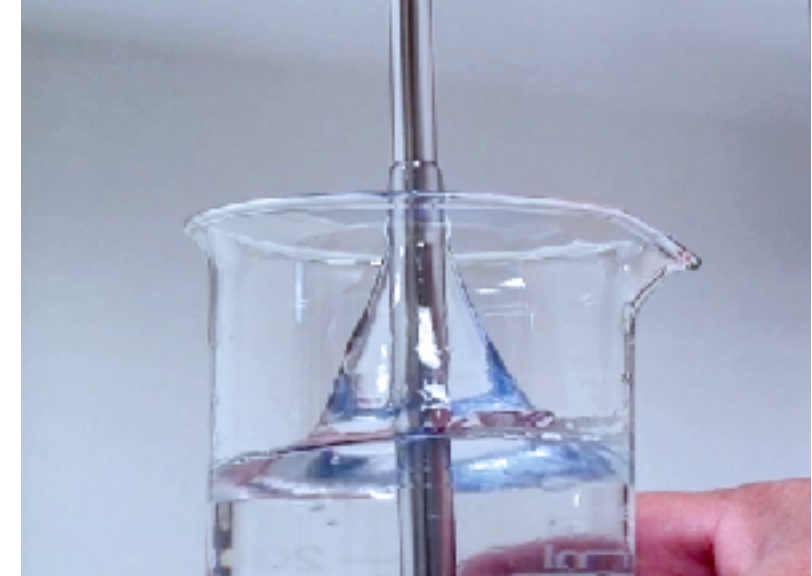
$$\nabla \mathbf{u} = \begin{pmatrix} -\dot{\epsilon}/2 & 0 & 0 \\ 0 & -\dot{\epsilon}/2 & 0 \\ 0 & 0 & \dot{\epsilon} \end{pmatrix} = \mathbf{D}$$

$$\boldsymbol{\sigma} = \begin{pmatrix} -p - A & 0 & 0 \\ 0 & -p - A & 0 \\ 0 & 0 & -p + 2A \end{pmatrix}$$

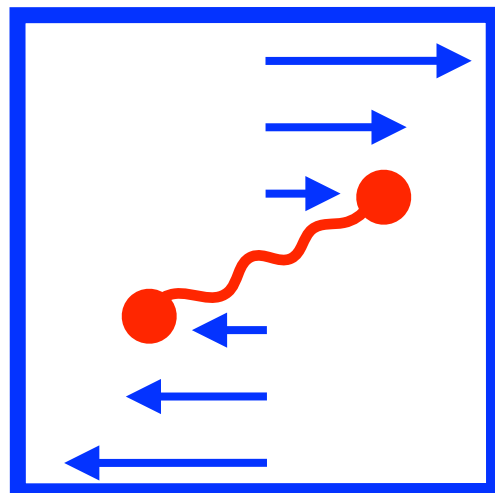
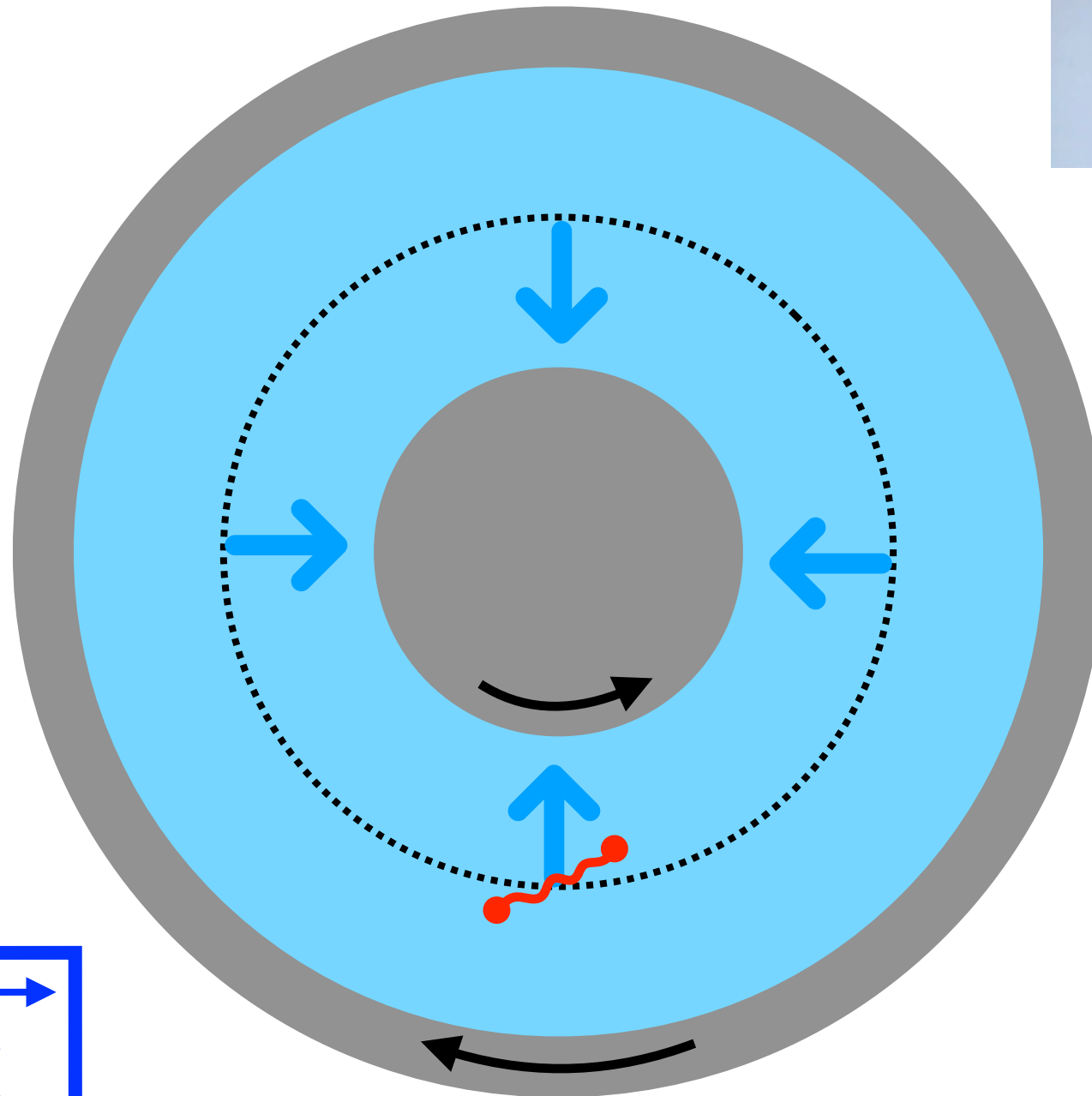
**1 component:
only viscosity**

Giusteri and Seto (2018) J. Rheol.

Weissenberg effect

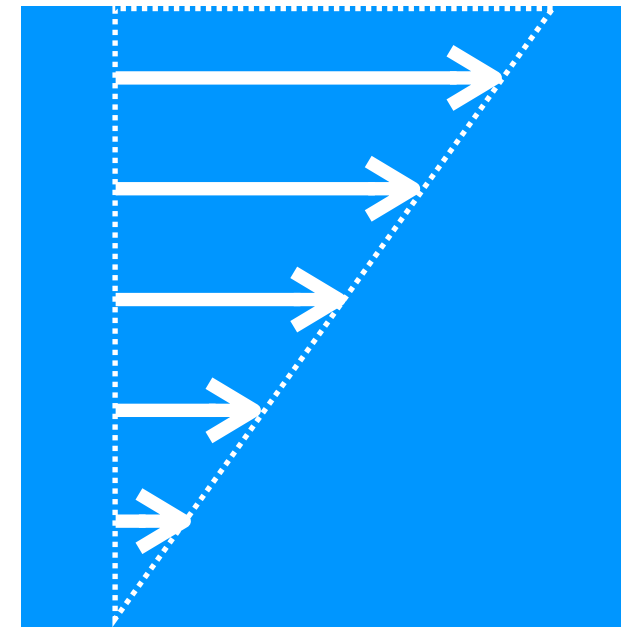
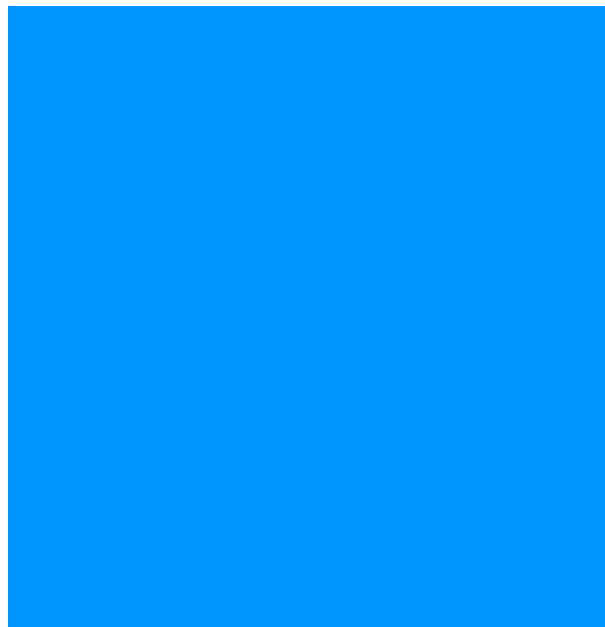


wikipedia



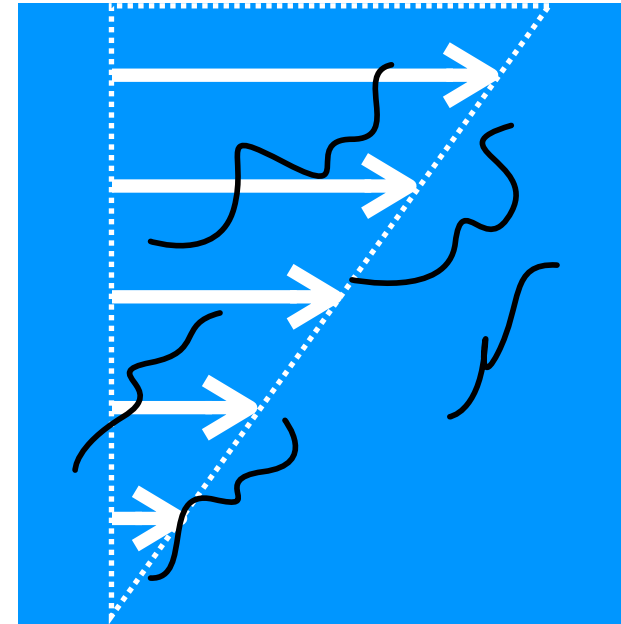
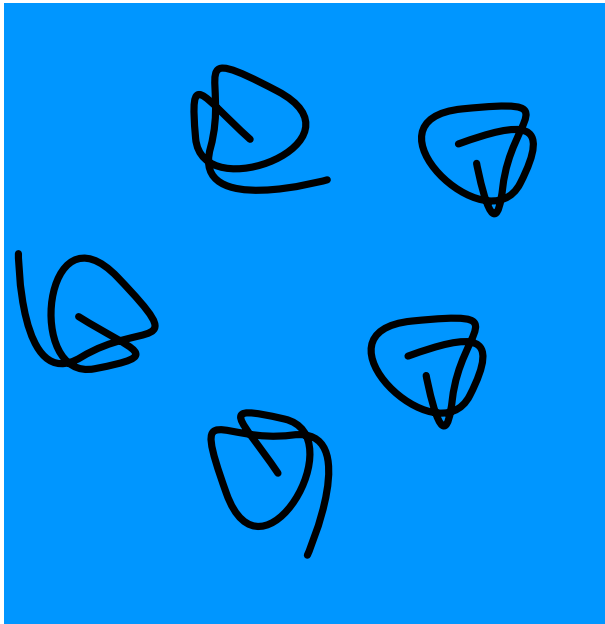
Newtonian liquid

$$\sigma_{xy} = \eta \dot{\gamma}$$



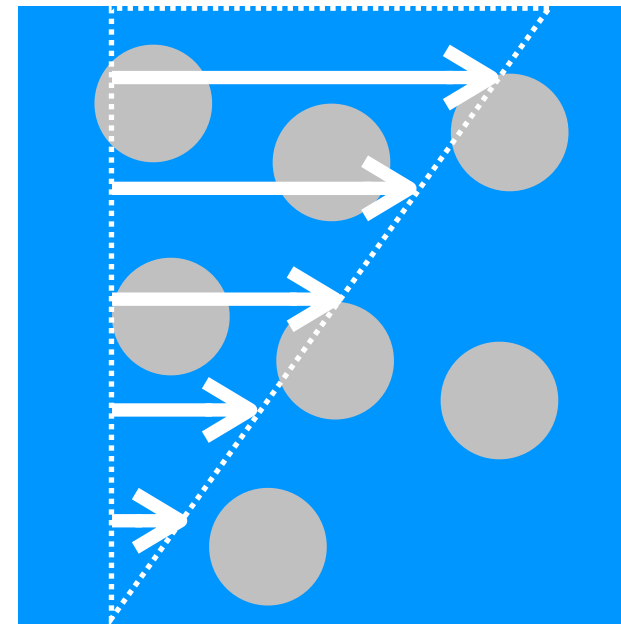
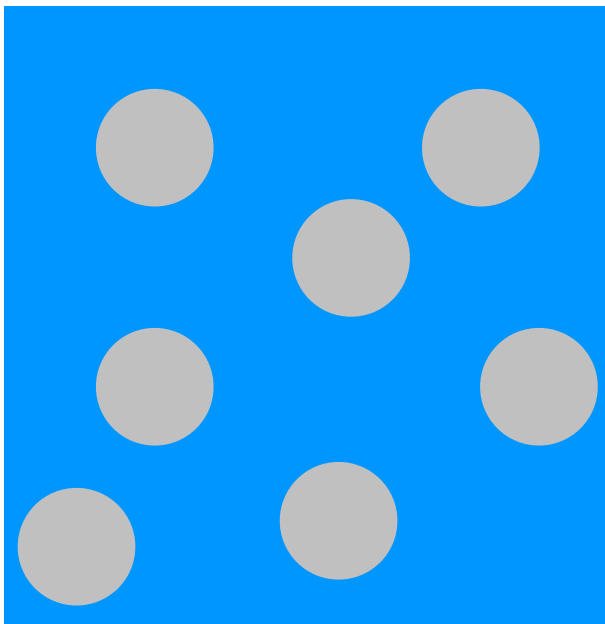
Newtonian liquid + elastic chains

$$\sigma_{xy} = \eta \dot{\gamma} + \tau_{xy}$$

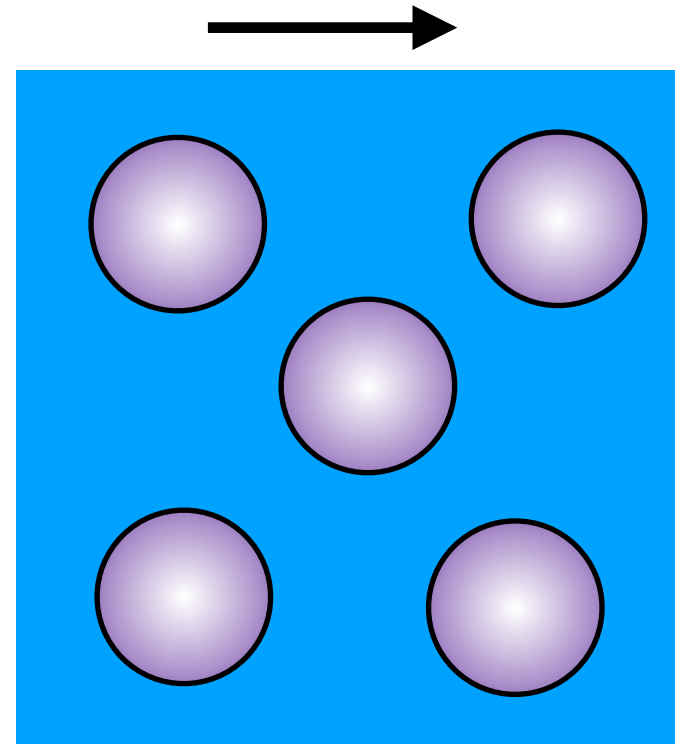


Newtonian liquid + rigid balls

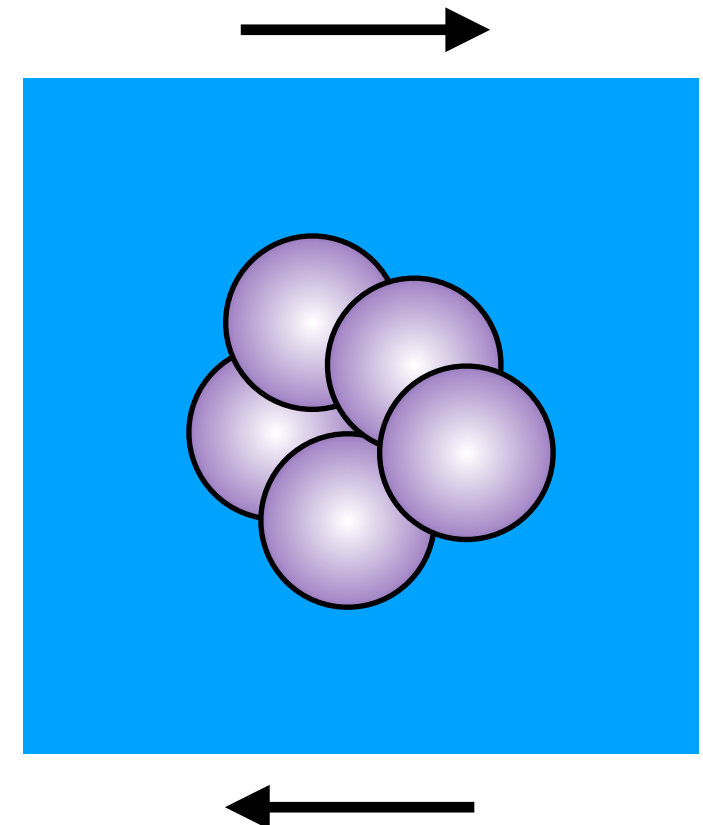
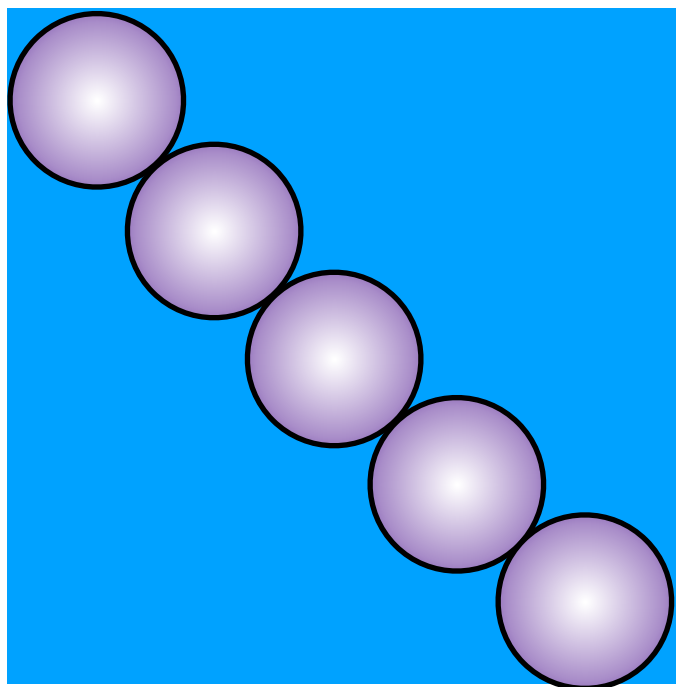
$$\sigma_{xy} = \eta \dot{\gamma} + \tau_{xy}$$



Negligible inertia...

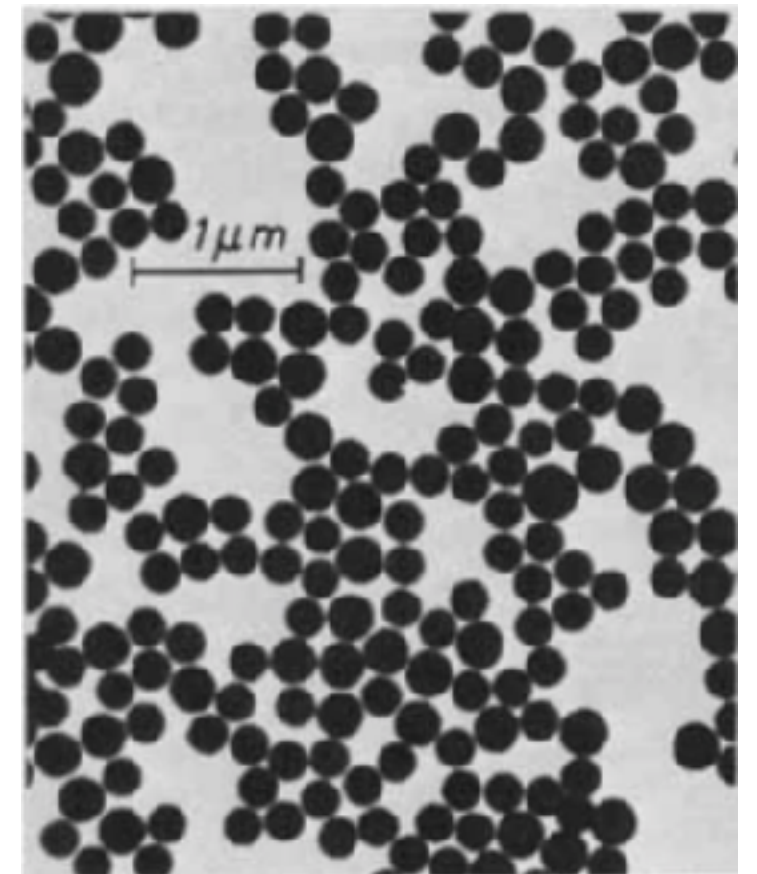
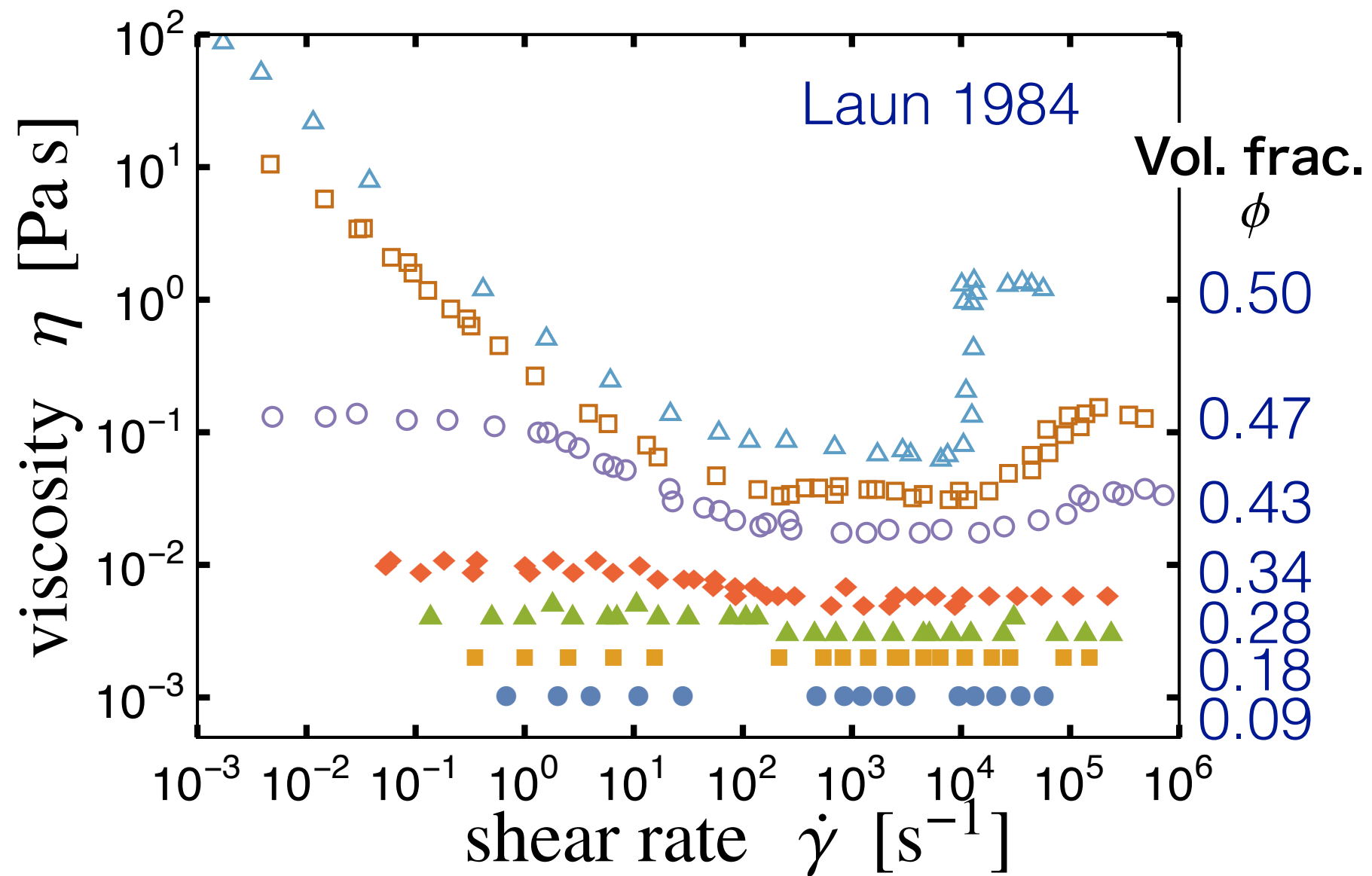


Microstructure determines the rheology!



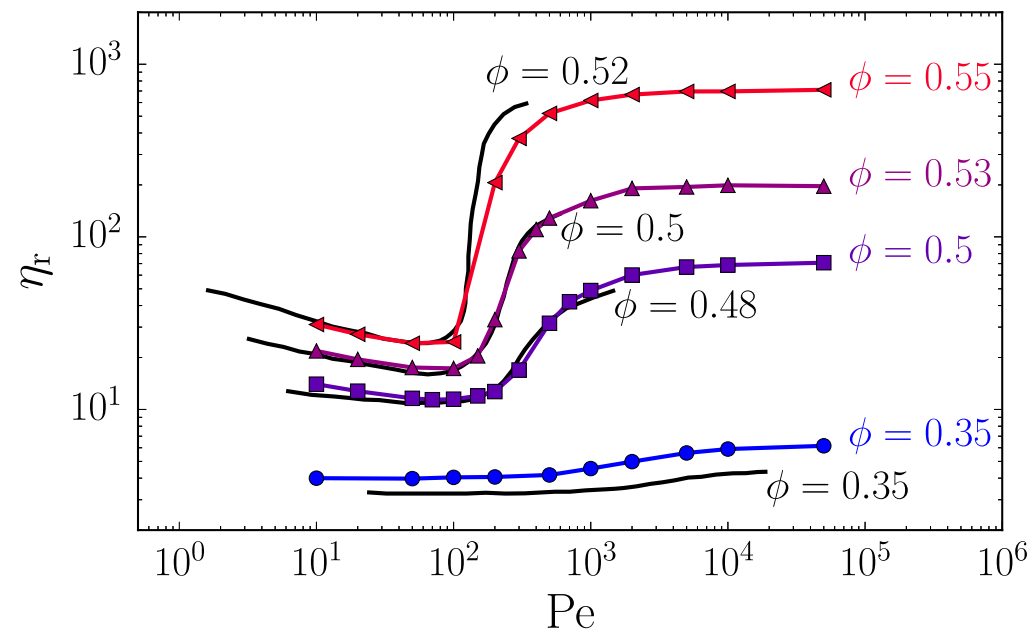
Non-Newtonian behavior in steady-shear rheology

$$\eta(\dot{\gamma})$$



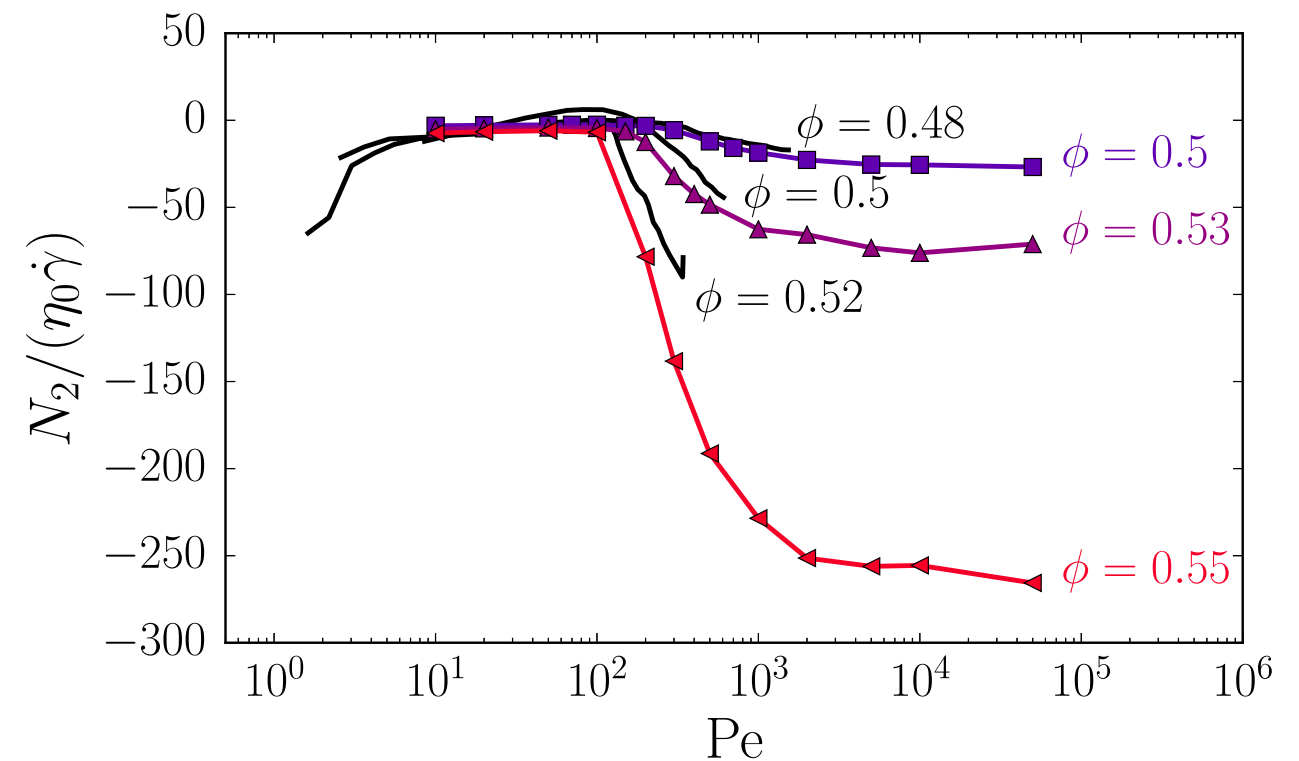
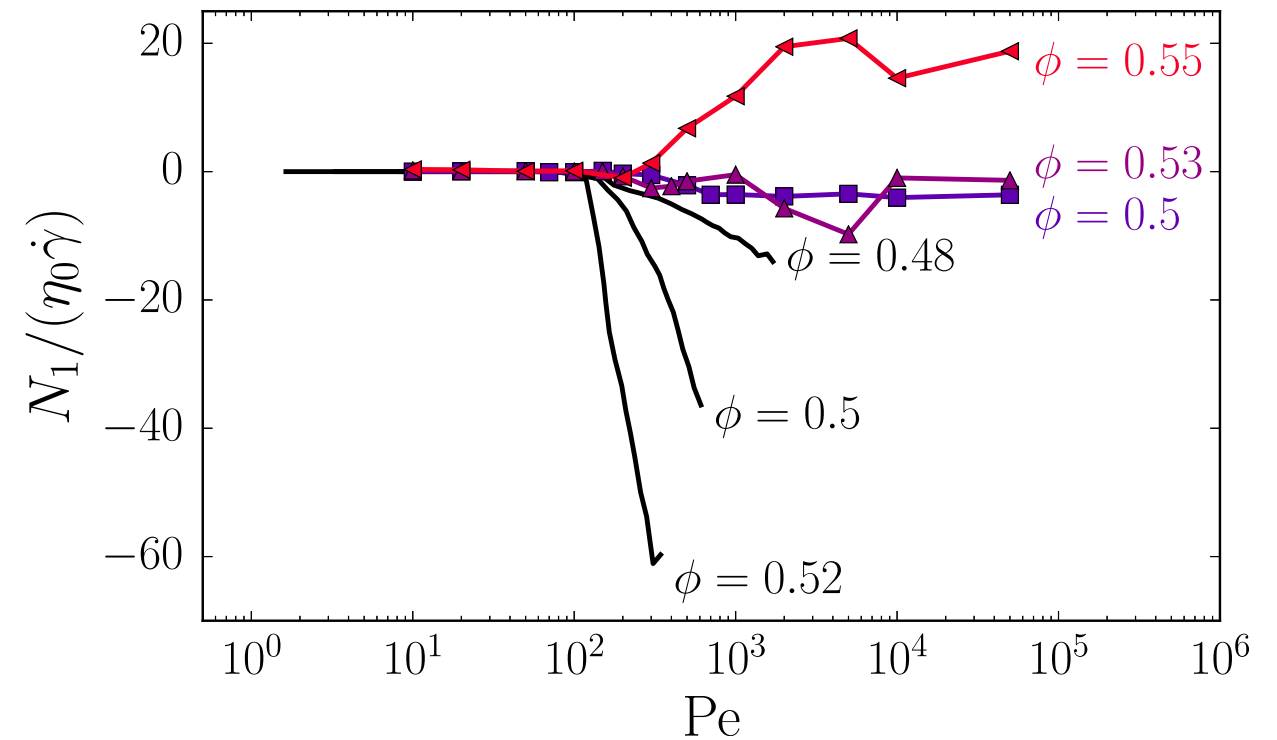
We could reproduce two of the three.

Mari, Seto, Morris, Denn PNAS (2015)



Experimental data
black-solid lines

Cwalina and Wagner, JOR (2014)



liquid

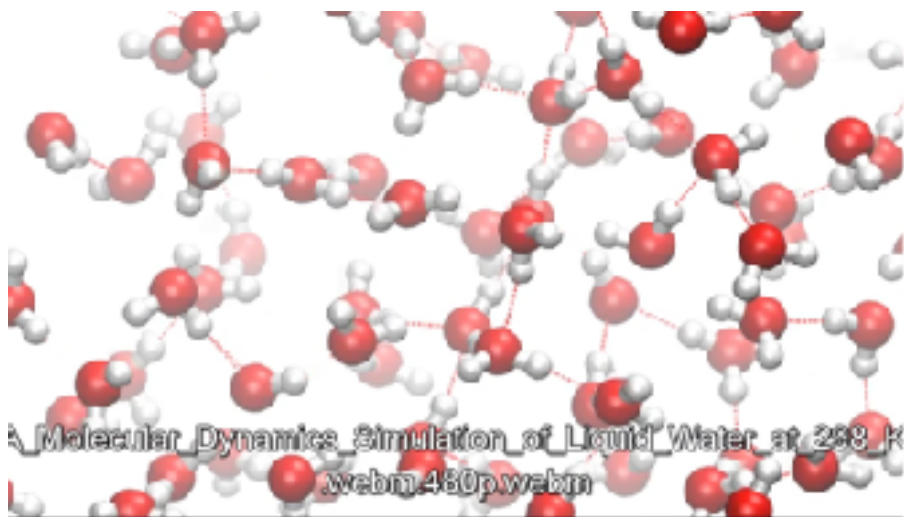
Newtonian fluid

$$\sigma = -p\mathbf{I} + 2\eta\mathbf{D}$$

time scale $1/\dot{\gamma}$

↑ macro
↓ micro

Molecular dynamics



$$\frac{\text{mean free path}}{\text{velocity}} \sim 10^{-11} \text{ s}$$

Colloidal suspension

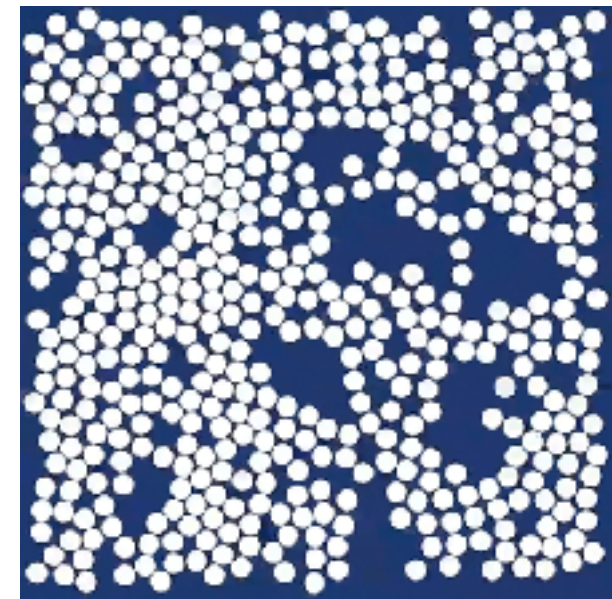
Non-Newtonian fluid

?

time scale $1/\dot{\gamma}$

↑ macro
↓ micro

Colloidal dynamics



$$\frac{\text{radius}^2}{\text{diffusion constant}} \sim 1 \text{ s}$$

Stokesian Dynamics

Brady & Bossis 1985

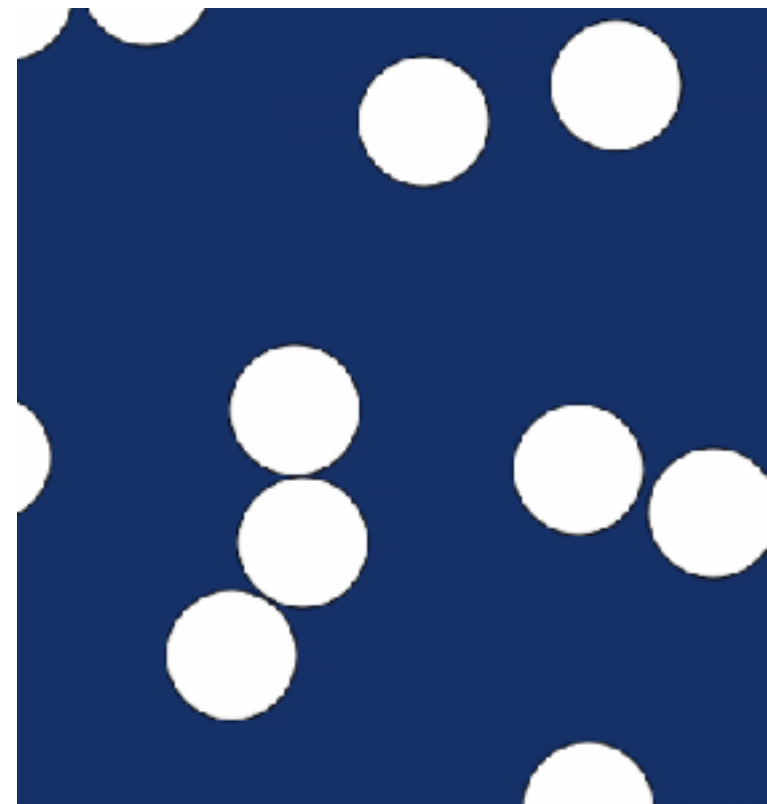
$6N$ -dimensional overdamped Langevin eq. with hydrodynamic interaction

$$\mathbf{F}_B + \mathbf{F}_H = \mathbf{0}$$

Hydrodynamic force $\mathbf{F}_H = -\mathbf{R} \cdot (\mathbf{U} - \mathbf{u}) + \mathbf{R}' : \mathbf{D}$

Brownian force $\langle \mathbf{F}_B \rangle = 0$, $\langle \mathbf{F}_B(t_1) \mathbf{F}_B(t_2) \rangle = 2k_B T \mathbf{R} \delta(t_1 - t_2)$

$$\mathbf{u}(\mathbf{r}) = \nabla \mathbf{u} \cdot \mathbf{r} = \mathbf{D} \cdot \mathbf{r} + (\boldsymbol{\omega}/2) \times \mathbf{r}$$



Brownian $\gg$ Flow $\rightarrow$ equilibrium

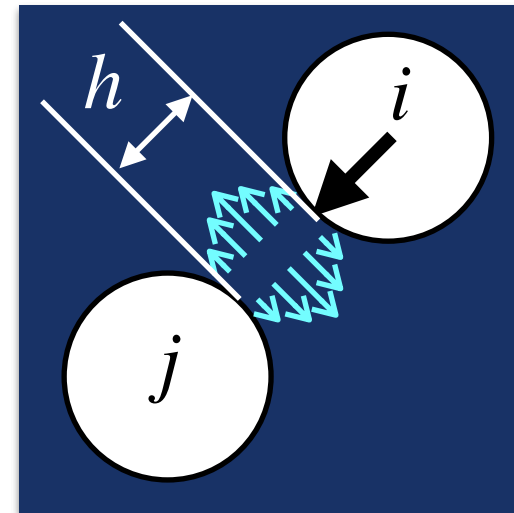
Brownian $\ll$ Flow $\rightarrow$ non-equilibrium

“Divergence-free” Stokesian Dynamics

lubrication force

$$\mathbf{F} \sim -\frac{1}{h}(\mathbf{U}^i - \mathbf{U}^j) \cdot \mathbf{n}\mathbf{n}$$

$$\frac{1}{h} \rightarrow \frac{1}{h + \delta}$$



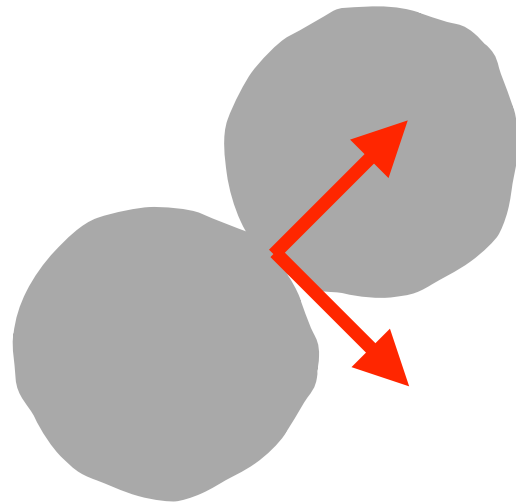
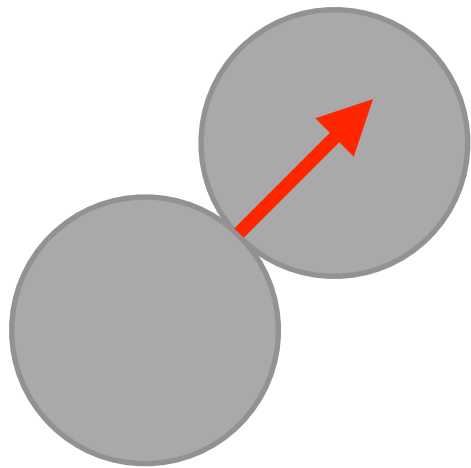
One important consequence

→ Particle contacts are no longer forbidden...

We *must* include a contact force model

$$\mathbf{F}_H + \mathbf{F}_B + \mathbf{F}_C = \mathbf{0}$$

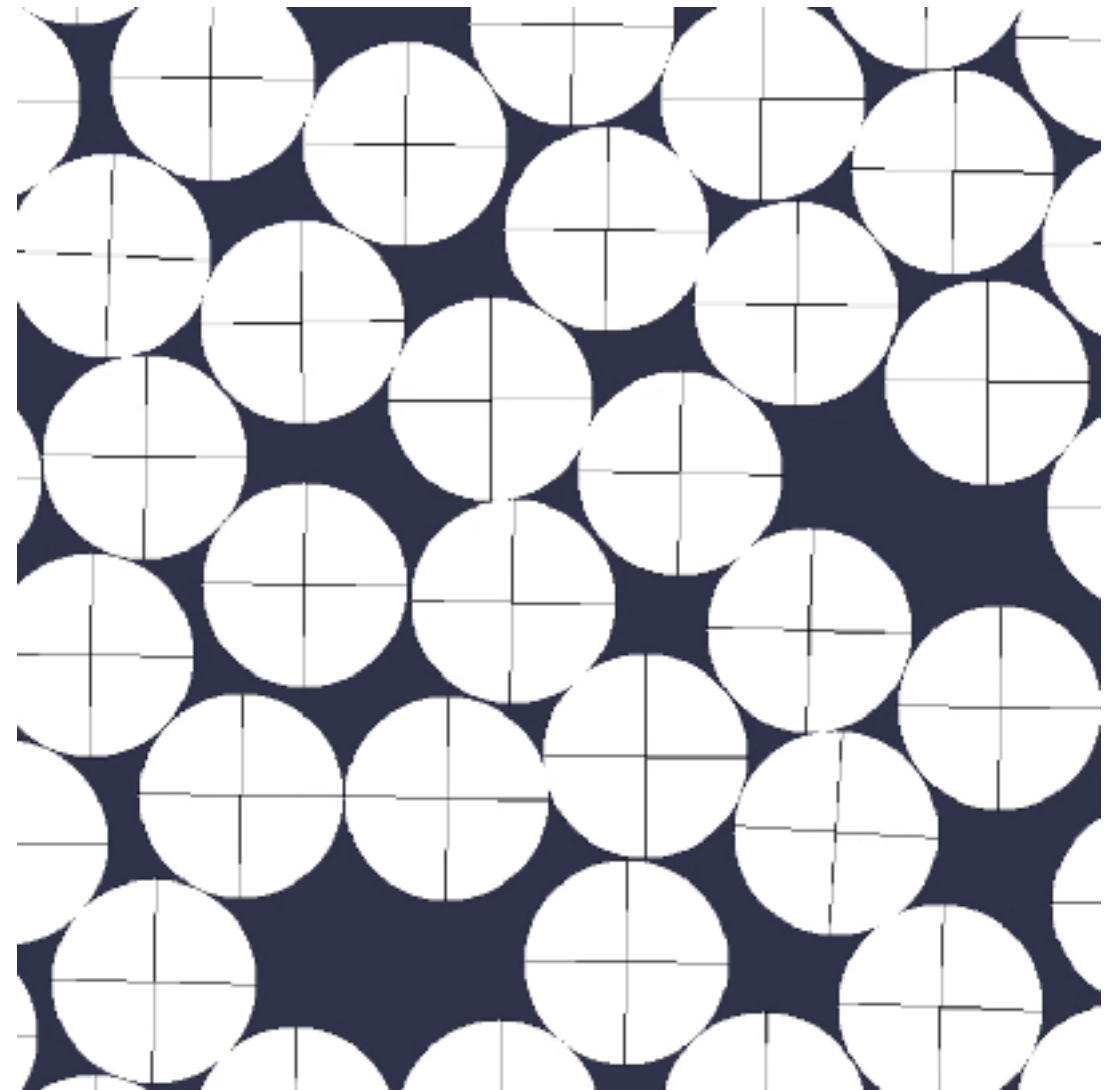
$$\mathbf{F}_H = -\mathbf{R} \cdot (\mathbf{U} - \mathbf{u}) + \mathbf{R}' : \mathbf{D}$$



$$|\mathbf{F}_C^{tan}| < \mu |\mathbf{F}_C^{nor}|$$

$$(\mathbf{F}_C^{ij})^{nor} = k_n(r_{ij} - 2a)\mathbf{n}^{ij}$$

$$(\mathbf{F}_C^{ij})^{tan} = -k_t \boldsymbol{\xi}^{ij}$$



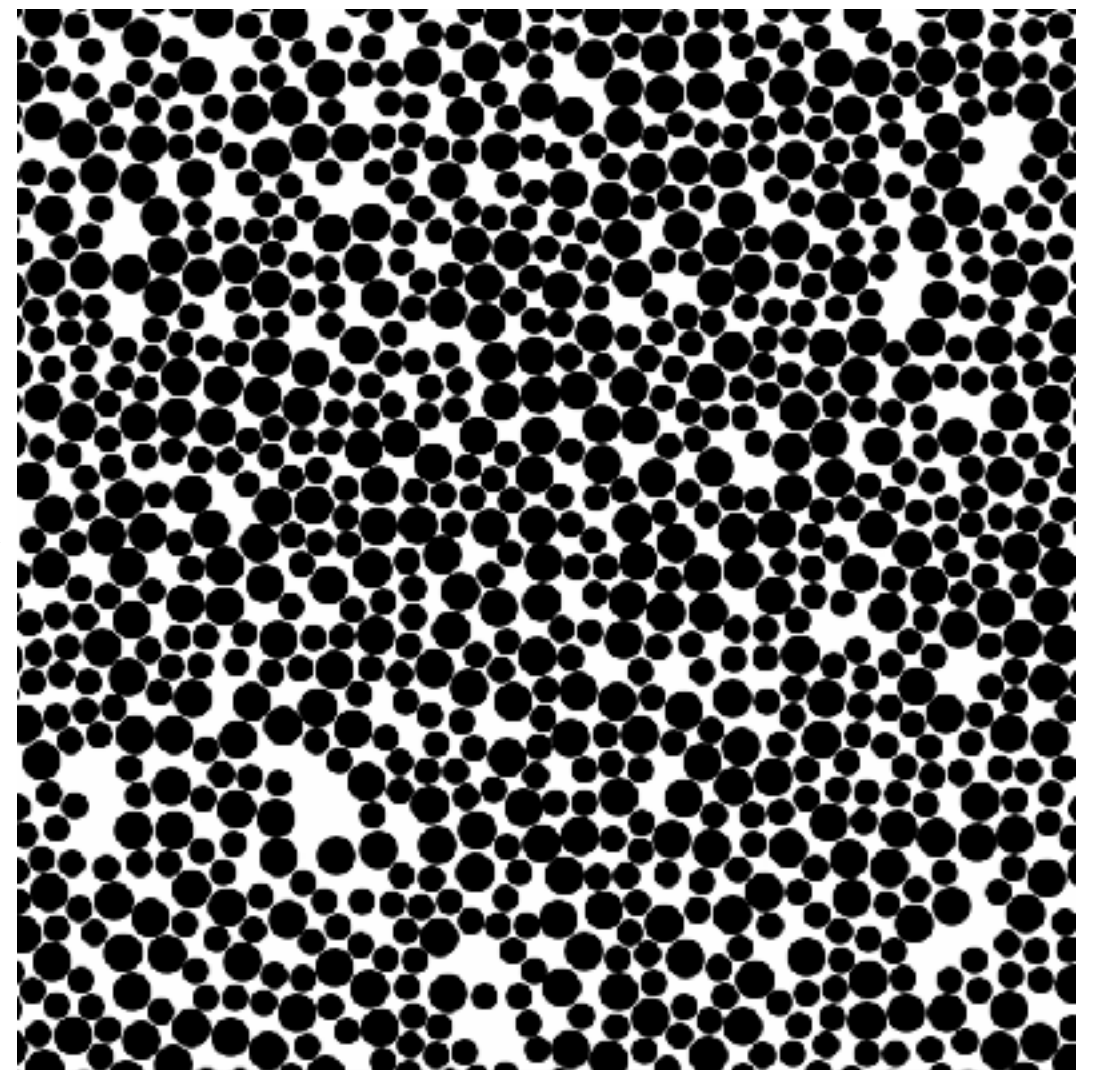
We can simulate the non-equilibrium limit
(thanks to these two modifications)

$$Pe \rightarrow \infty \longrightarrow F_H + \cancel{F_B} + F_C = 0$$

cf. Brady 1995: Perturbation theory for the small Pe regime
(Shear distorts isotropic microstructures)

$$F_H + F_C = 0$$

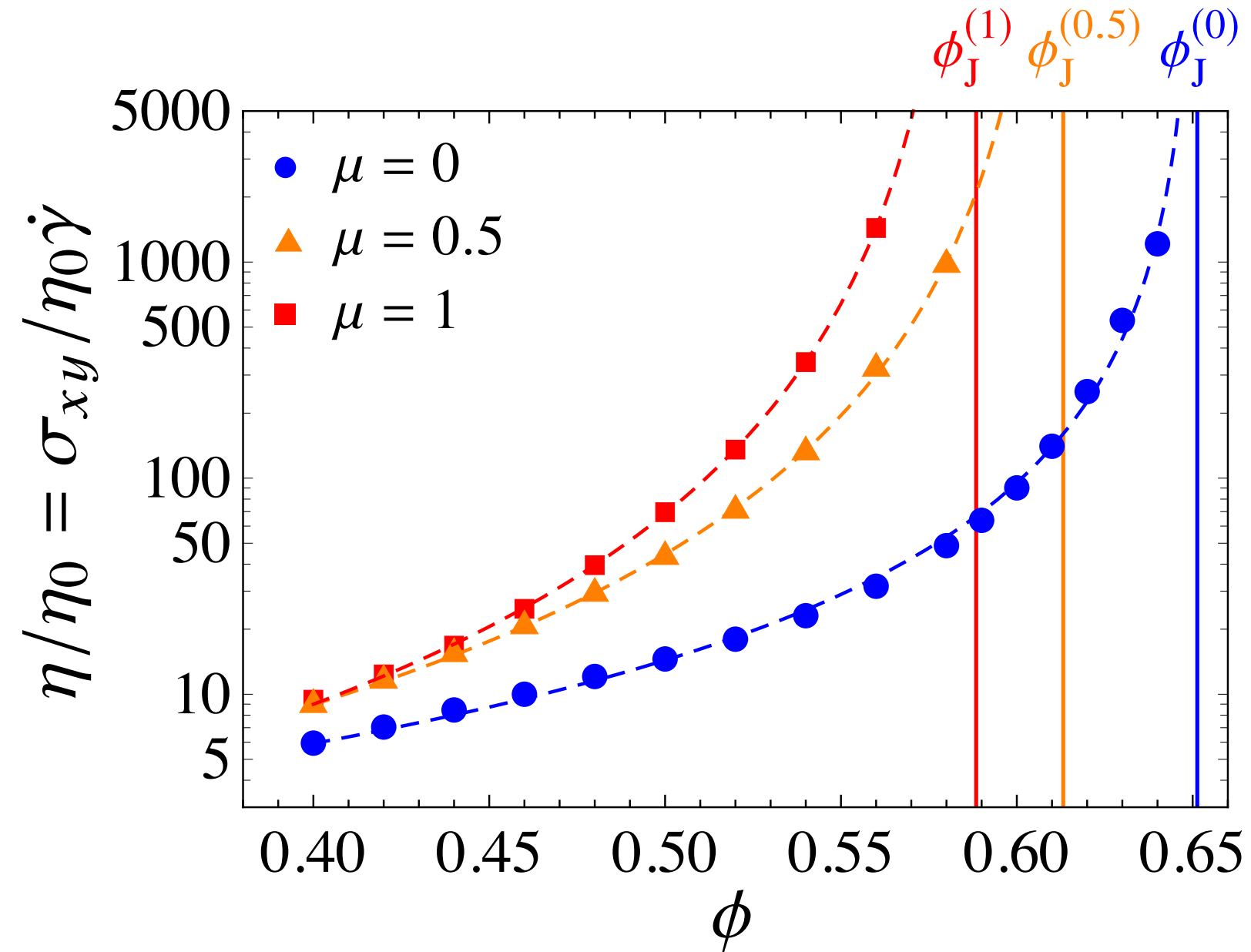
$$F_H = -R \cdot (U - u) + R' : D$$



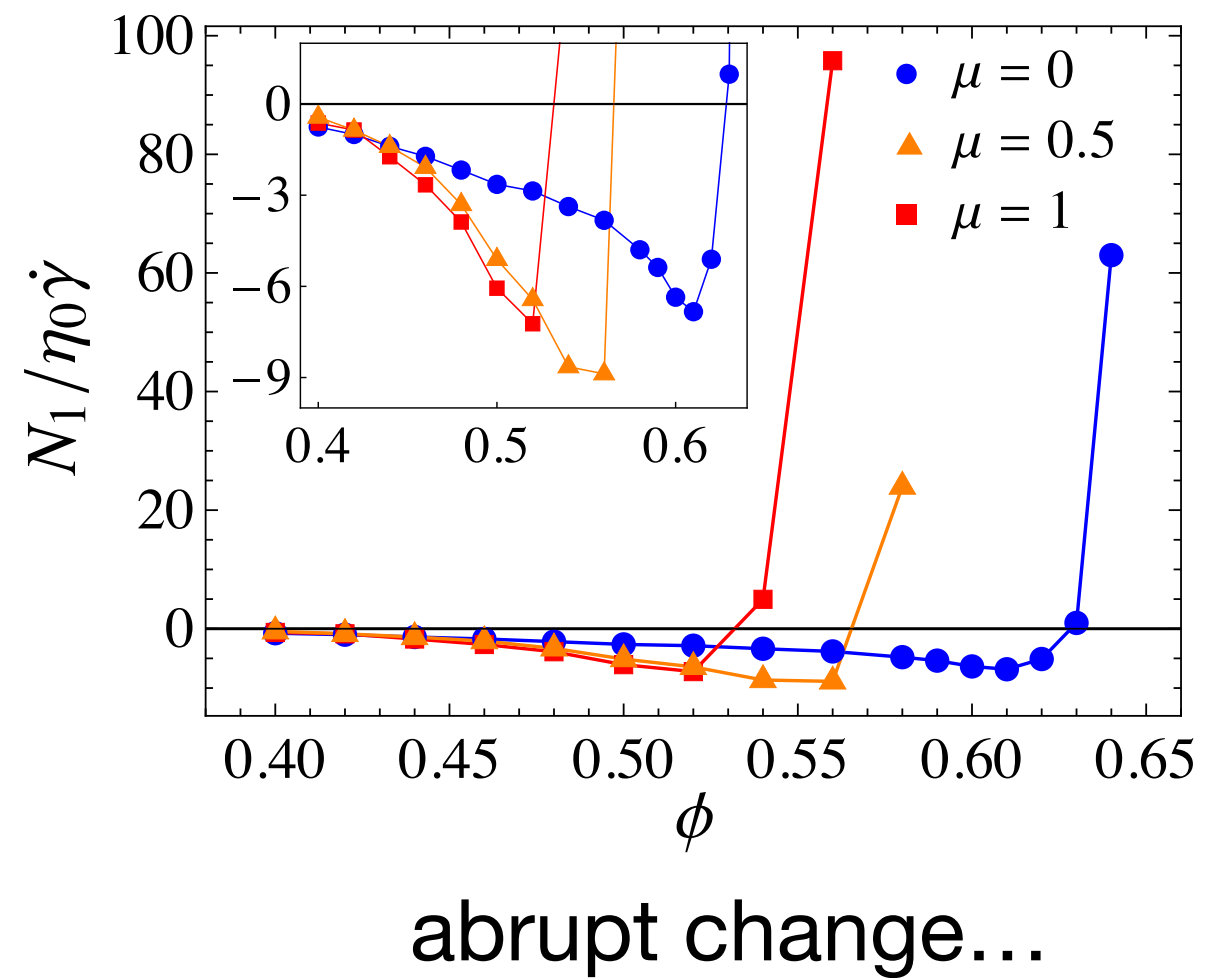
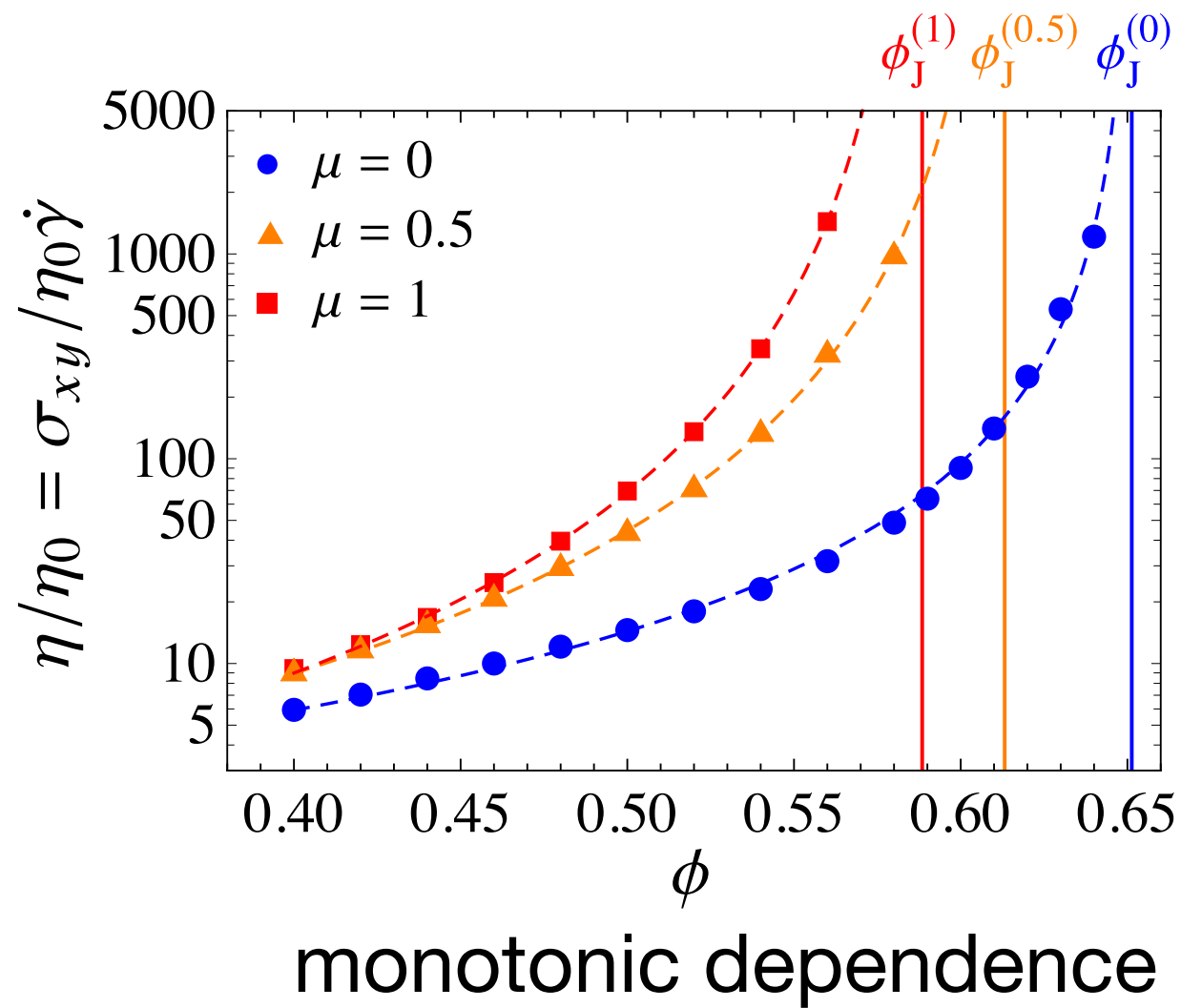
(2D demo)

Monotonic increase of viscosity

$$\eta(\phi)/\eta_0 = c(\phi_J - \phi)^{-\lambda}$$



Non-monotonic ϕ dependence of N_1



Steady shear rheology

$$\sigma_{xy} = \eta \dot{\gamma}$$

$$N_1 = \sigma_{xx} - \sigma_{yy}$$

$$N_2 = \sigma_{yy} - \sigma_{zz}$$

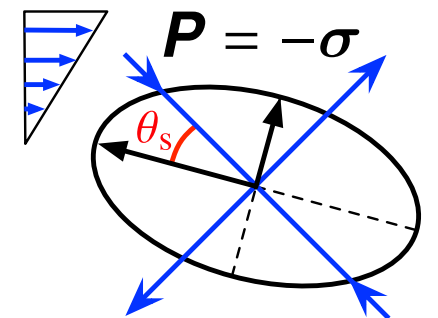
$$p = -\frac{1}{3} \text{Tr } \sigma$$

$$\longleftrightarrow \sigma = \begin{pmatrix} -p + \frac{2}{3}N_1 + \frac{1}{3}N_2 & \sigma_{xy} & 0 \\ \sigma_{xy} & -p - \frac{1}{3}N_1 + \frac{1}{3}N_2 & 0 \\ 0 & 0 & -p - \frac{1}{3}N_1 - \frac{2}{3}N_2 \end{pmatrix}$$

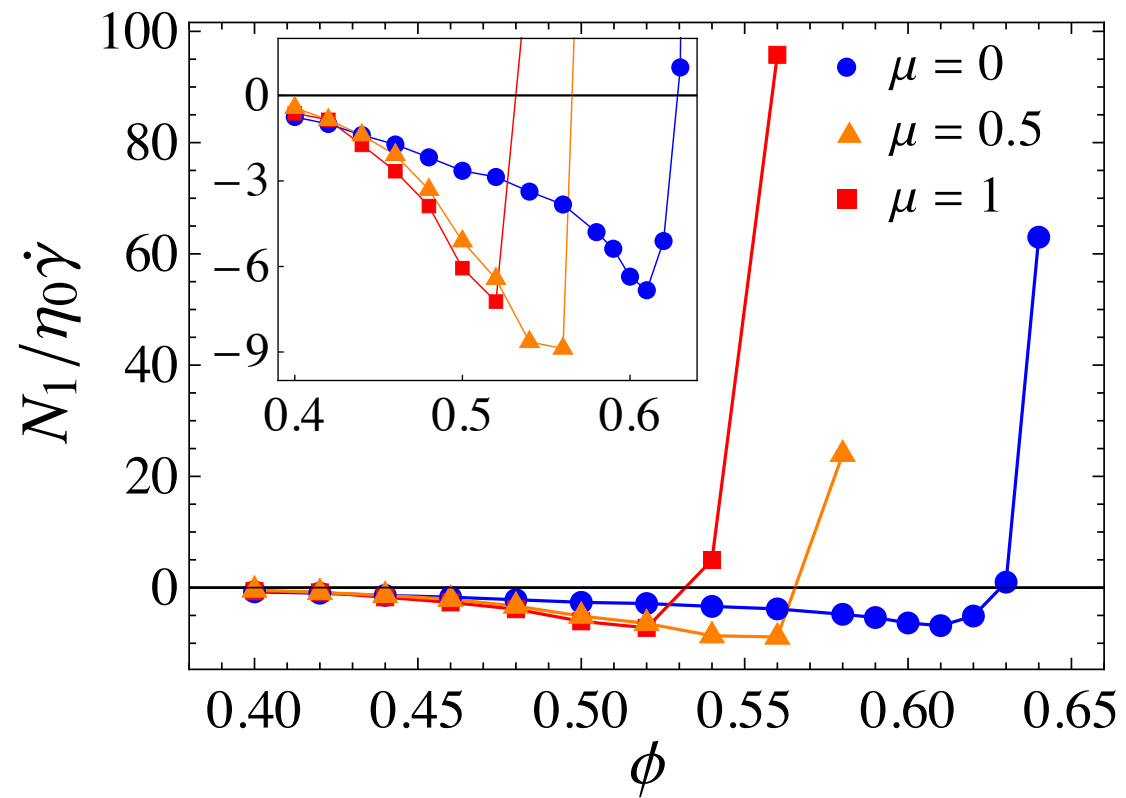
$$N_0 \equiv \sigma_{zz} - \frac{\sigma_{xx} + \sigma_{yy}}{2} = -N_2 - 0.5N_1$$

$$\text{Eigenvalues} \left\{ \begin{array}{l} P_1 = p \left(1 + \frac{N_0}{3p} \right) + \frac{\sigma_{xy}}{2} \sqrt{4 + (N_1/\sigma_{xy})^2} \\ P_2 = p \left(1 + \frac{N_0}{3p} \right) - \frac{\sigma_{xy}}{2} \sqrt{4 + (N_1/\sigma_{xy})^2} \\ P_3 = p \left(1 - 2\frac{N_0}{3p} \right) \end{array} \right.$$

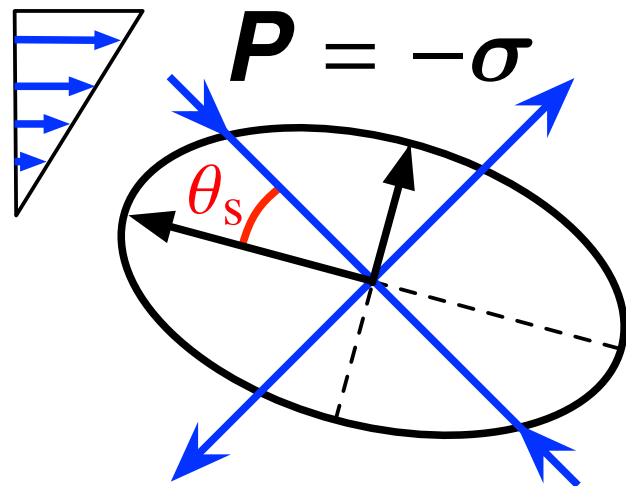
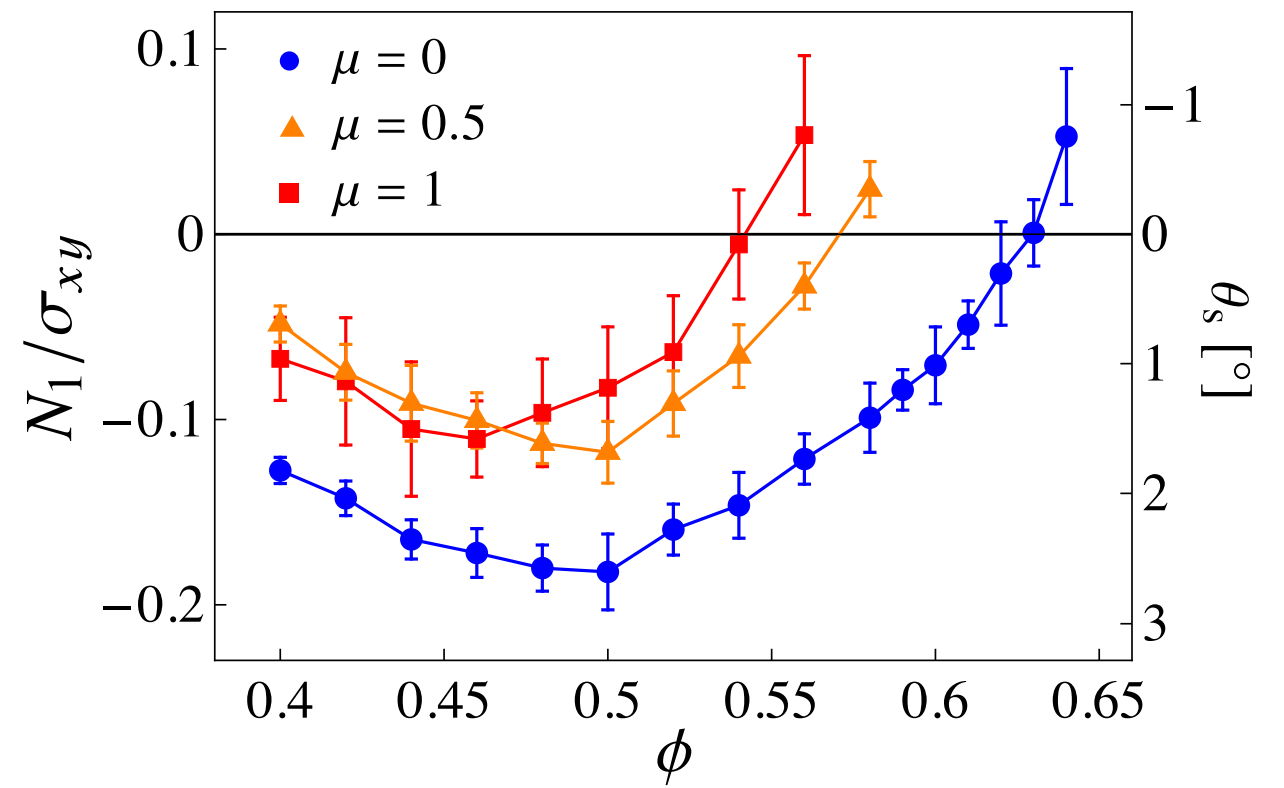
$$\text{Eigenvectors} \left\{ \begin{array}{l} \hat{n}_1 = \begin{pmatrix} \cos(\theta_s + 3\pi/4) \\ \sin(\theta_s + 3\pi/4) \\ 0 \end{pmatrix}, \quad \hat{n}_2 = \begin{pmatrix} \cos(\theta_s + \pi/4) \\ \sin(\theta_s + \pi/4) \\ 0 \end{pmatrix}, \quad \hat{n}_3 = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \\ \theta_s \equiv \tan^{-1} \left(\frac{-N_1/\sigma_{xy}}{2 + \sqrt{4 + (N_1/\sigma_{xy})^2}} \right) \approx -\frac{N_1}{4\sigma_{xy}} \end{array} \right.$$



abrupt change



rather smooth sign change

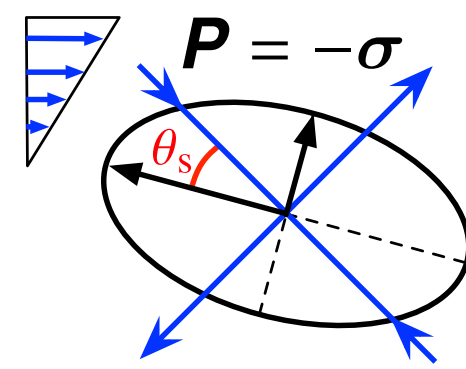


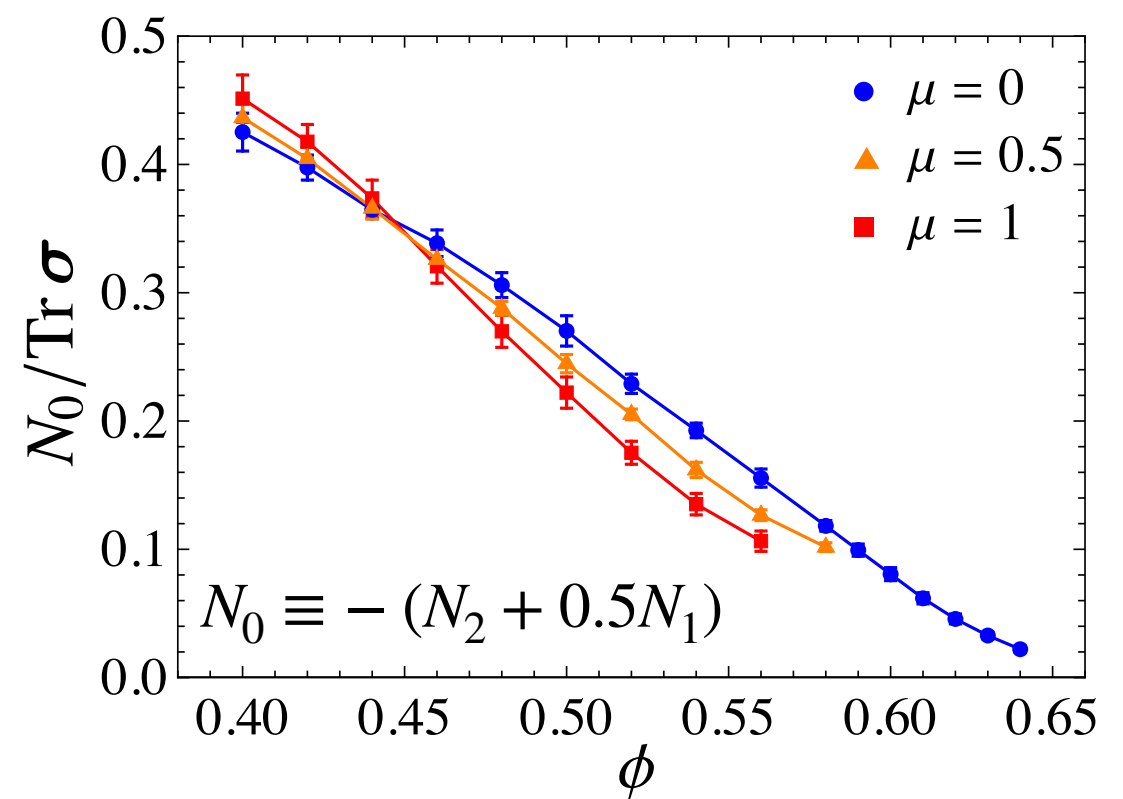
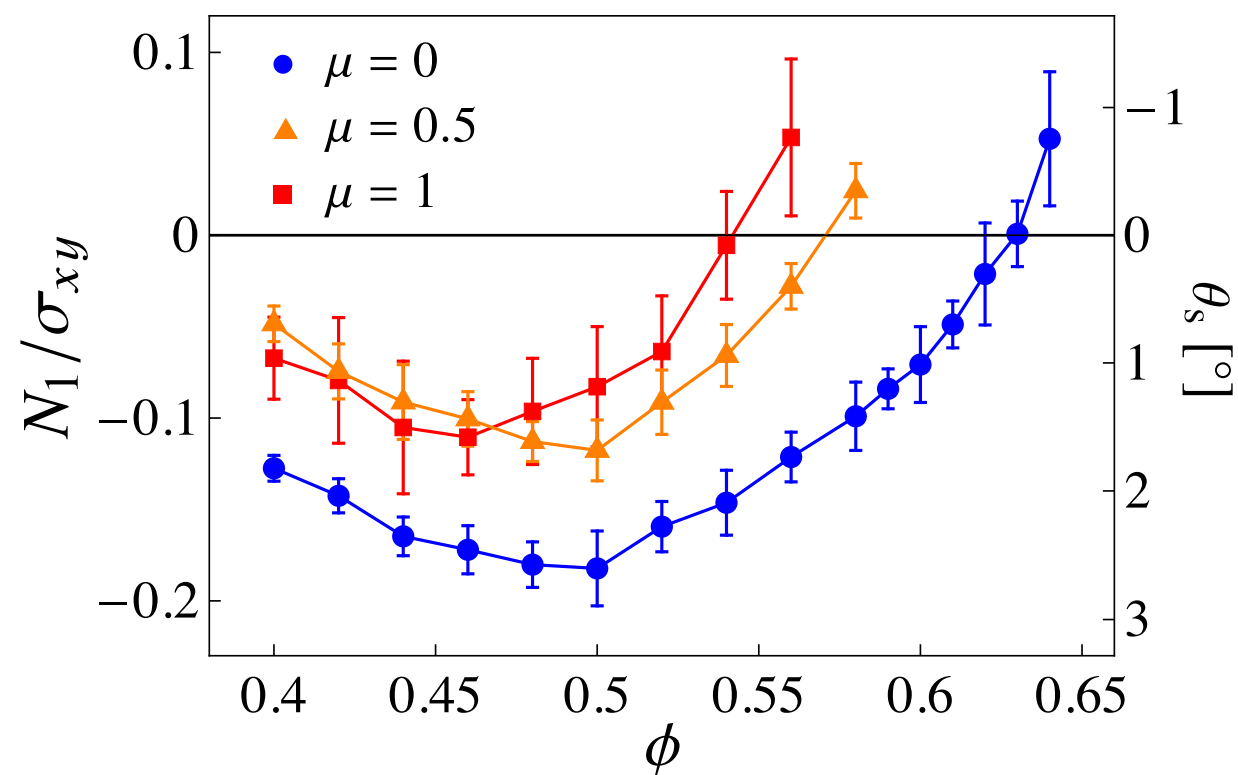
$$\theta_s \equiv \tan^{-1} \left(\frac{-N_1/\sigma_{xy}}{2 + \sqrt{4 + (N_1/\sigma_{xy})^2}} \right) \approx -\frac{N_1}{4\sigma_{xy}}$$

$$N_0 \equiv \sigma_{zz} - \frac{\sigma_{xx} + \sigma_{yy}}{2} = -N_2 - 0.5N_1$$

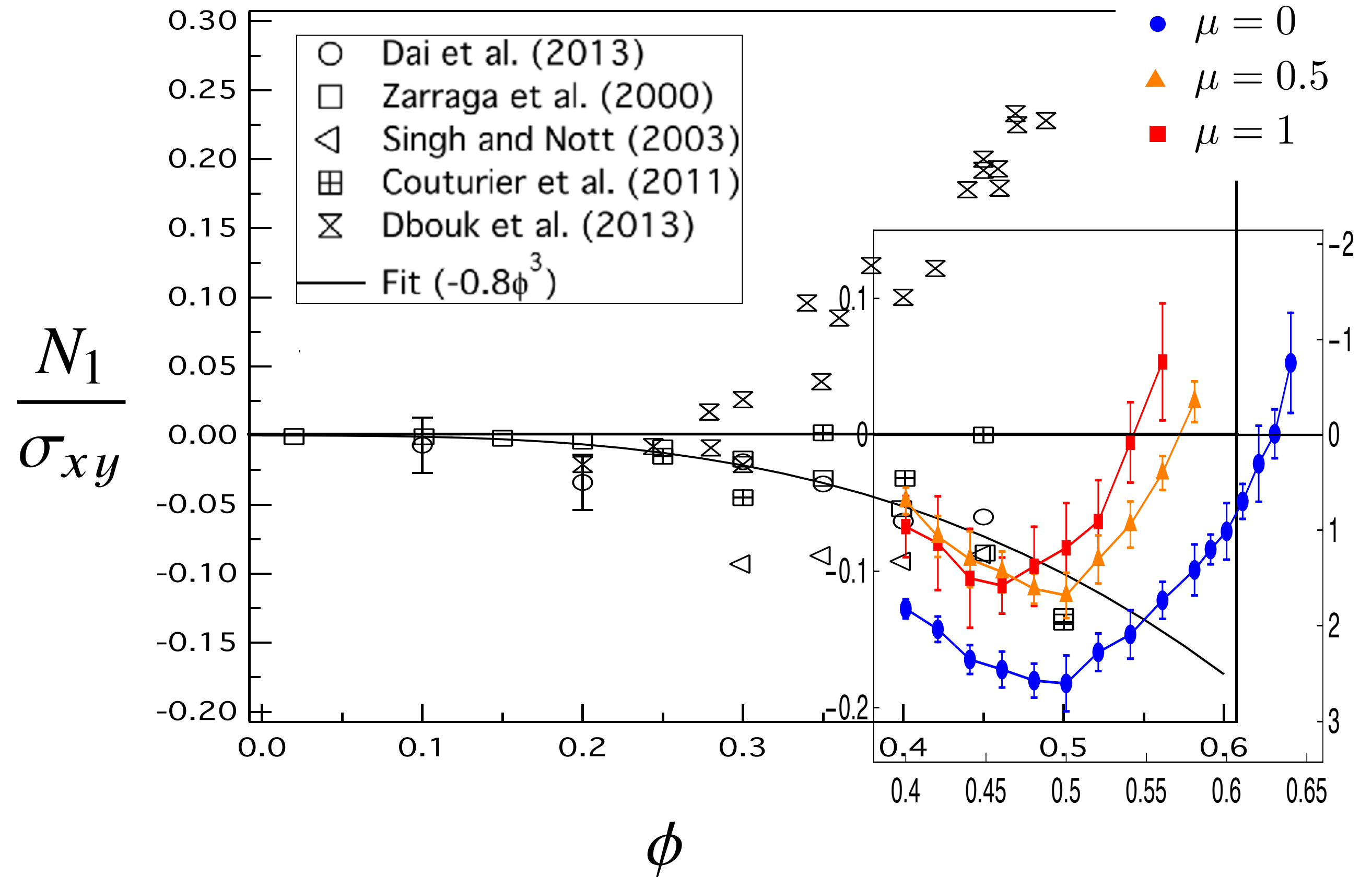
Eigenvalues

$$\left\{ \begin{array}{l} P_1 = p \left(1 + \frac{N_0}{3p} \right) + \frac{\sigma_{xy}}{2} \sqrt{4 + (N_1/\sigma_{xy})^2} \\ P_2 = p \left(1 + \frac{N_0}{3p} \right) - \frac{\sigma_{xy}}{2} \sqrt{4 + (N_1/\sigma_{xy})^2} \\ P_3 = p \left(1 - 2\frac{N_0}{3p} \right) \end{array} \right.$$

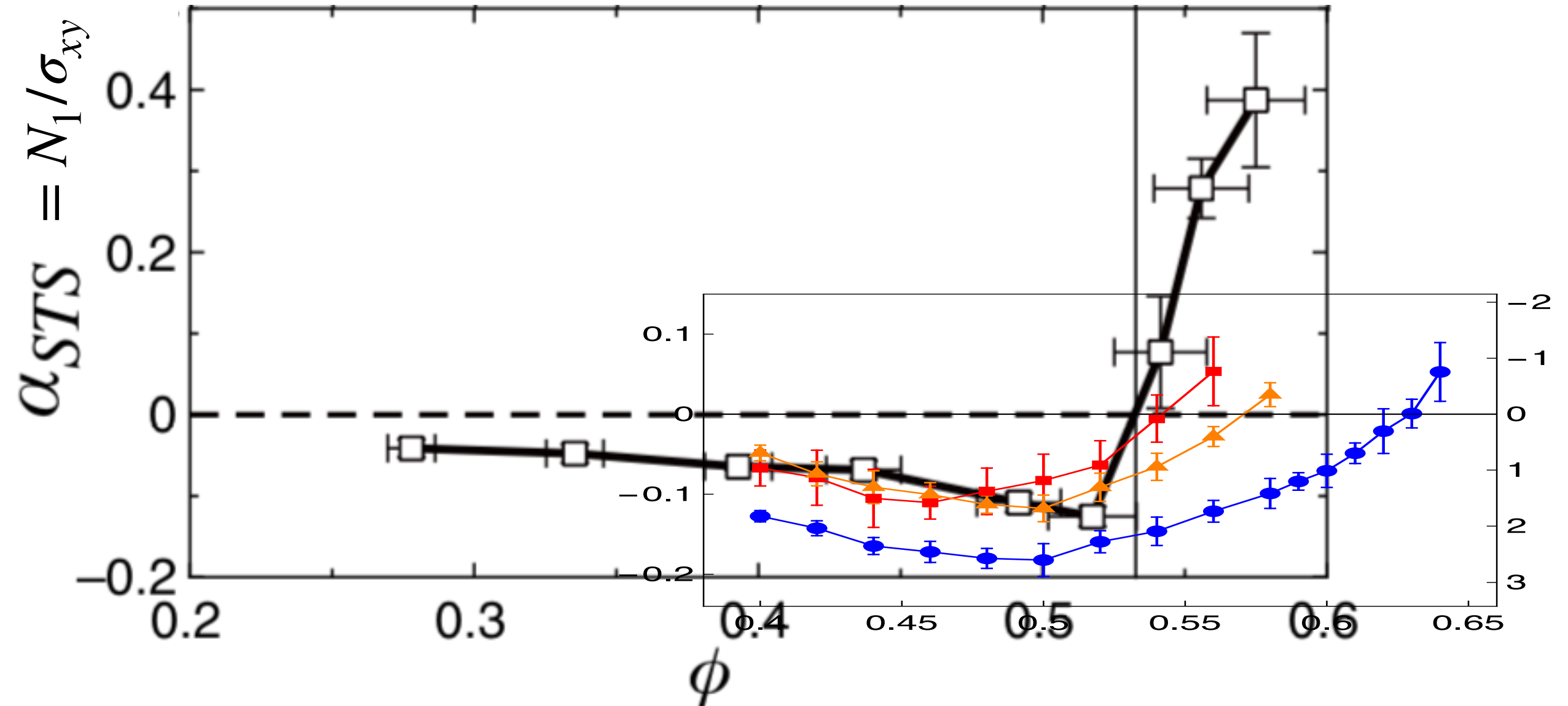
$$\theta_s \equiv \tan^{-1} \left(\frac{-N_1/\sigma_{xy}}{2 + \sqrt{4 + (N_1/\sigma_{xy})^2}} \right) \approx -\frac{N_1}{4\sigma_{xy}}$$




Experimental data



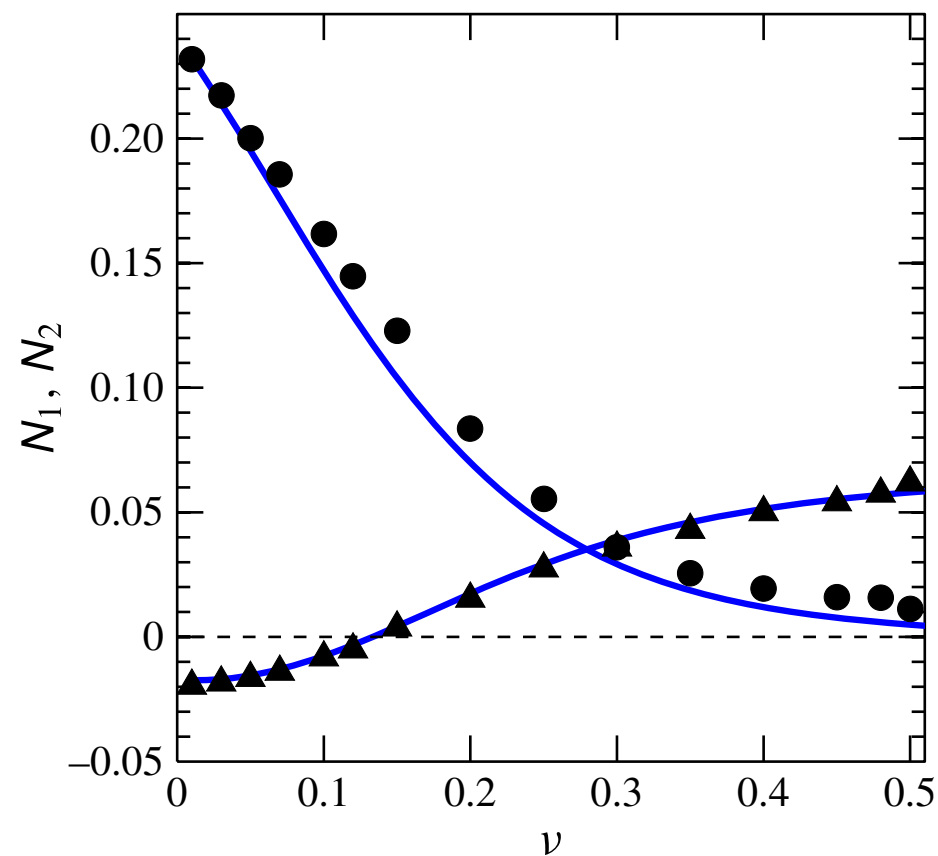
Experimental data



Royer, Blair, and Hudson
Phys. Rev. Lett., 116:188301, 2016.

Simulation of collisional granular systems

Alam and Luding (2005)



$$\tilde{N}_2 \equiv (P_{yy} - P_{zz})/p$$

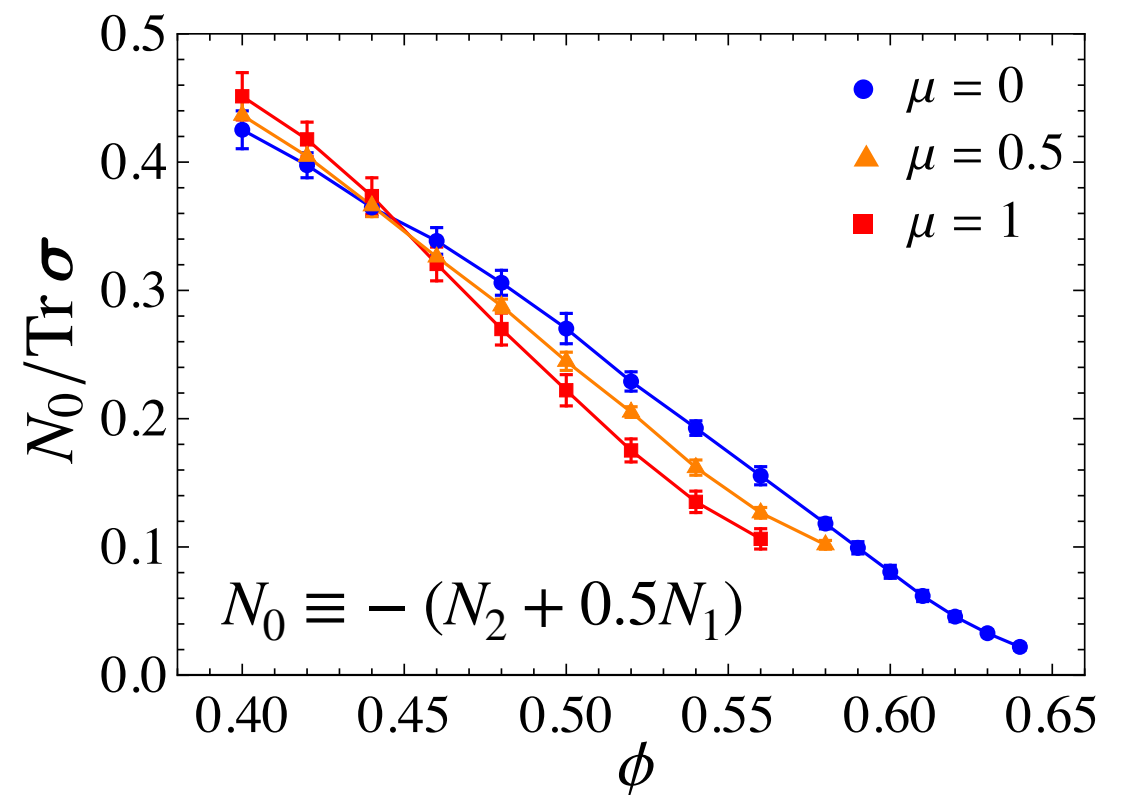
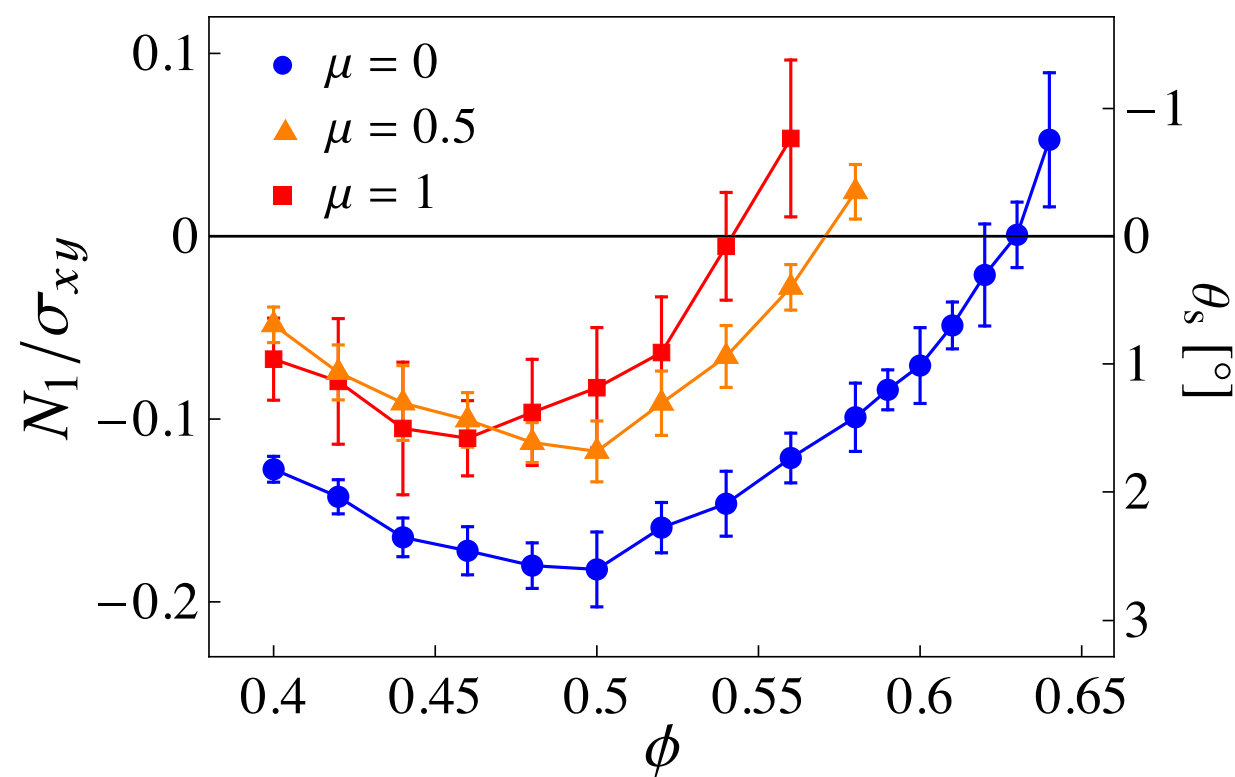
$$\tilde{N}_1 \equiv (P_{xx} - P_{yy})/p$$

**note: opposite signs
in the definitions of NSD.**



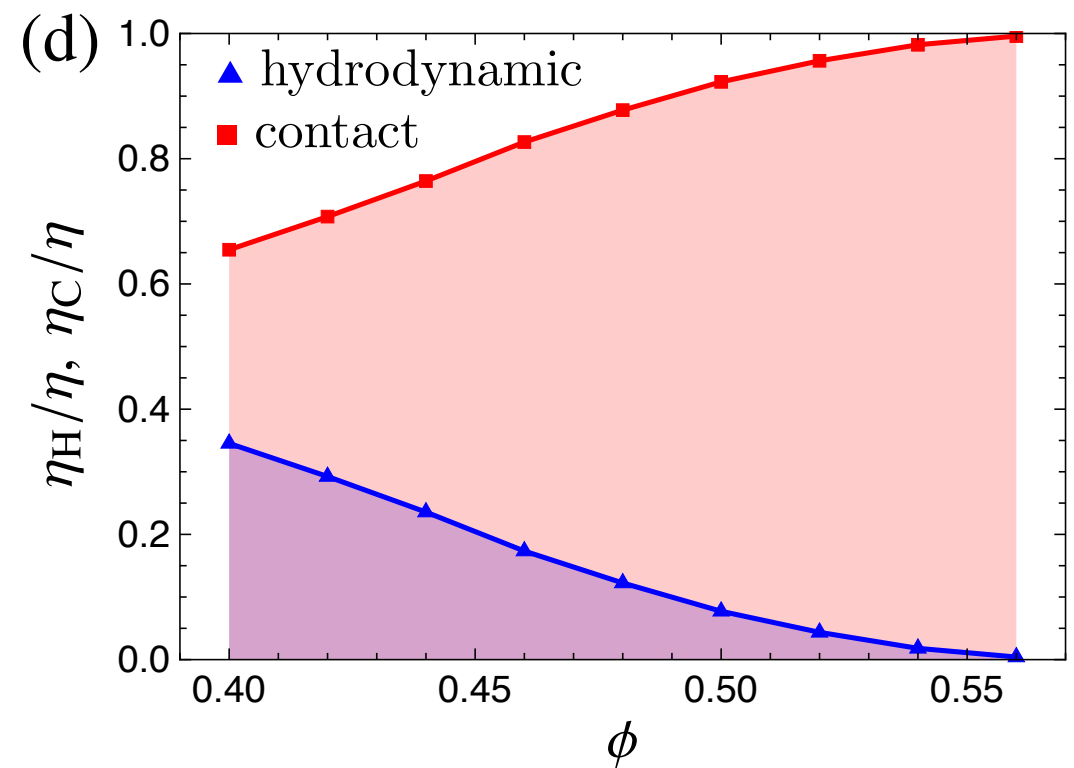
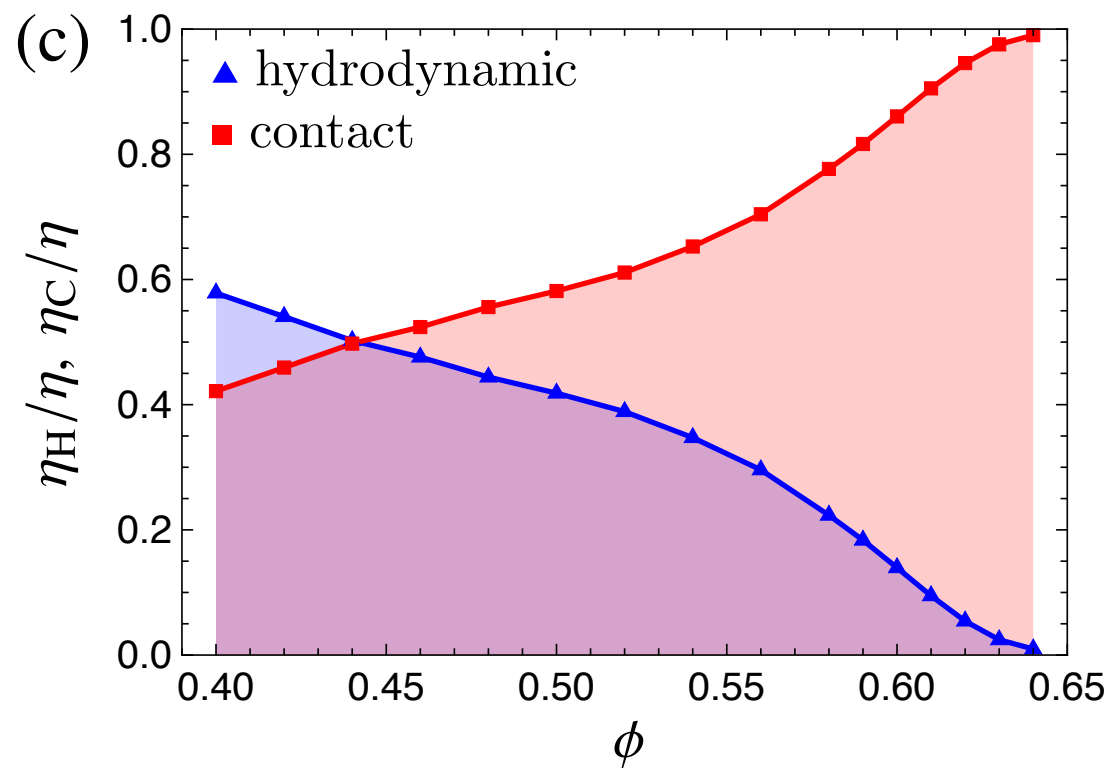
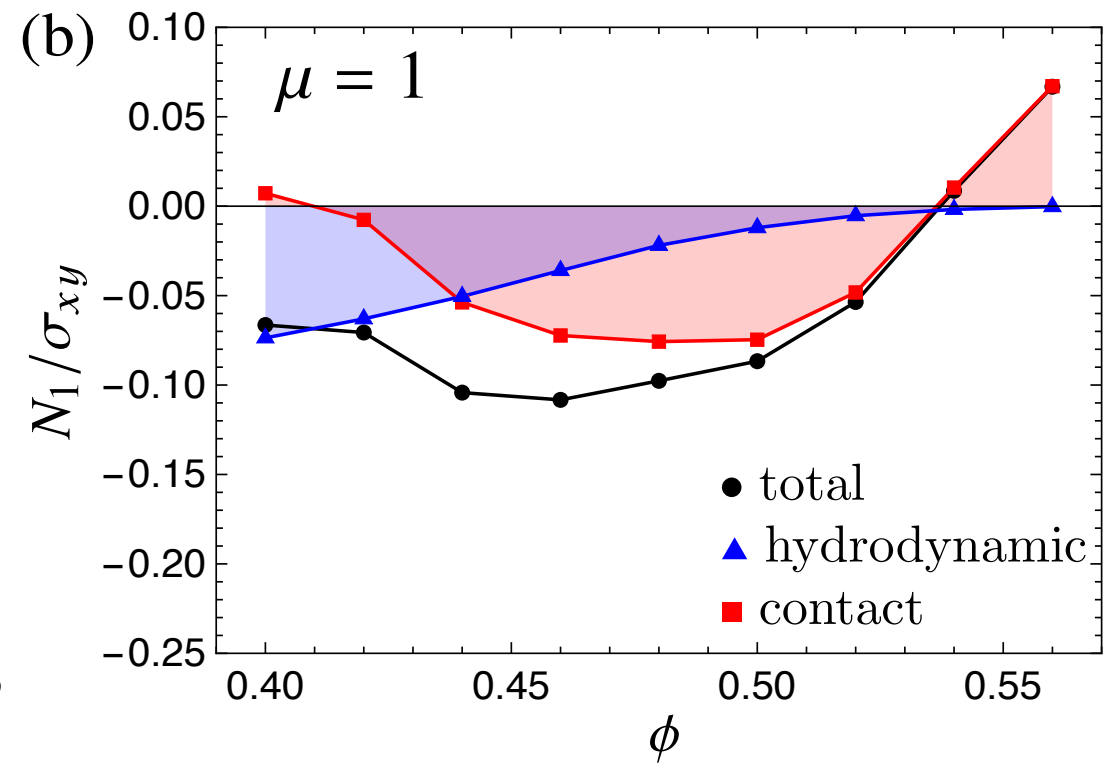
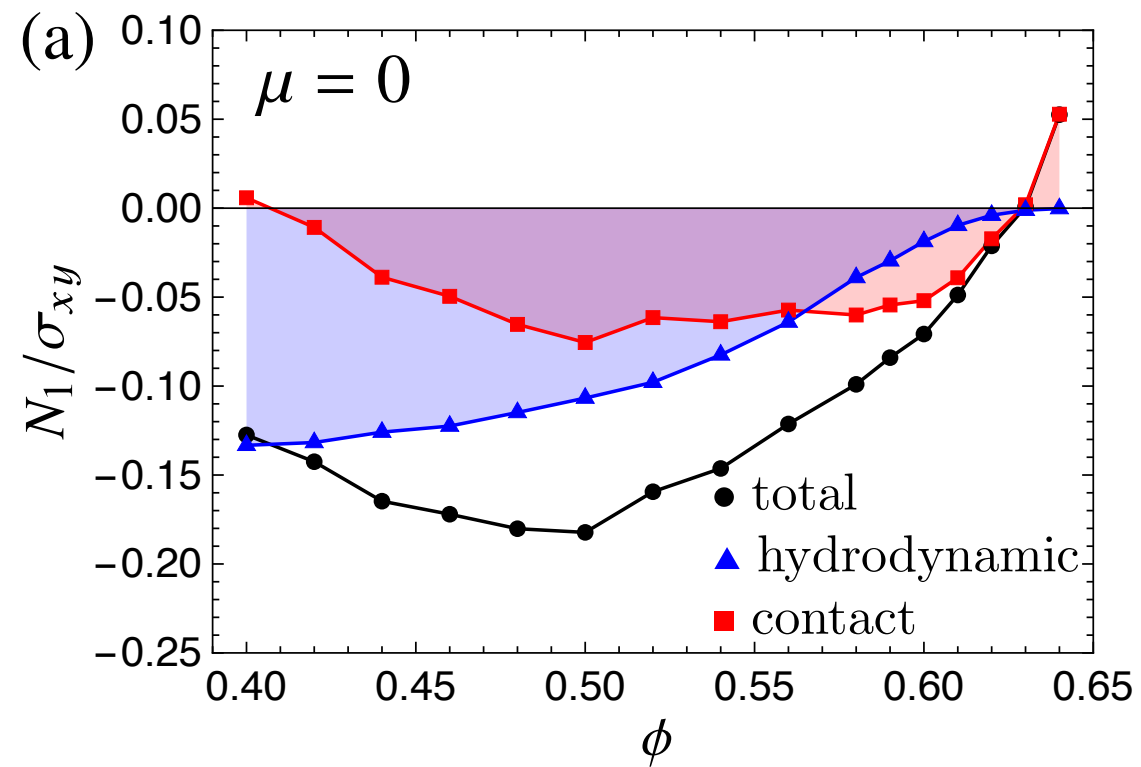
$$N_1 \equiv \sigma_{xx} - \sigma_{yy}$$

$$N_2 \equiv \sigma_{yy} - \sigma_{zz}$$



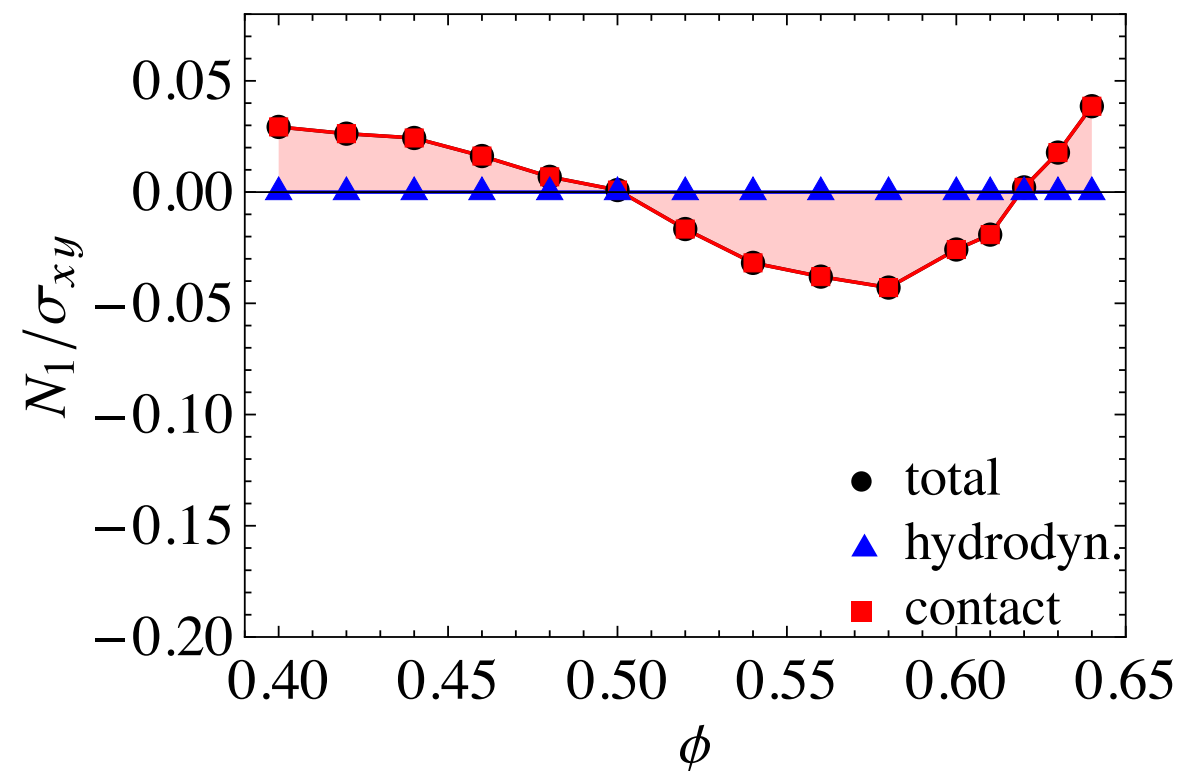
$$N_0 \equiv -(N_2 + 0.5N_1)$$

Hydrodynamic interaction vs. Contact force



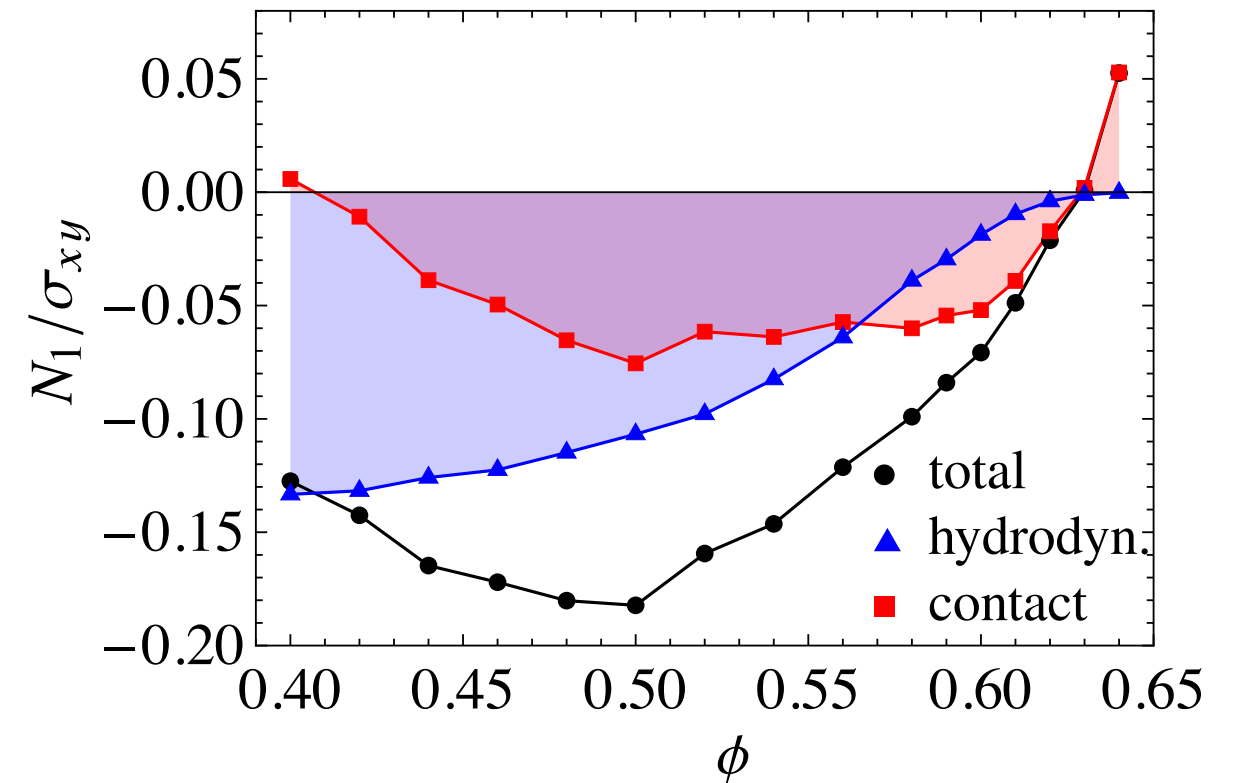
Without

hydrodynamics interaction
(frictionless)



With

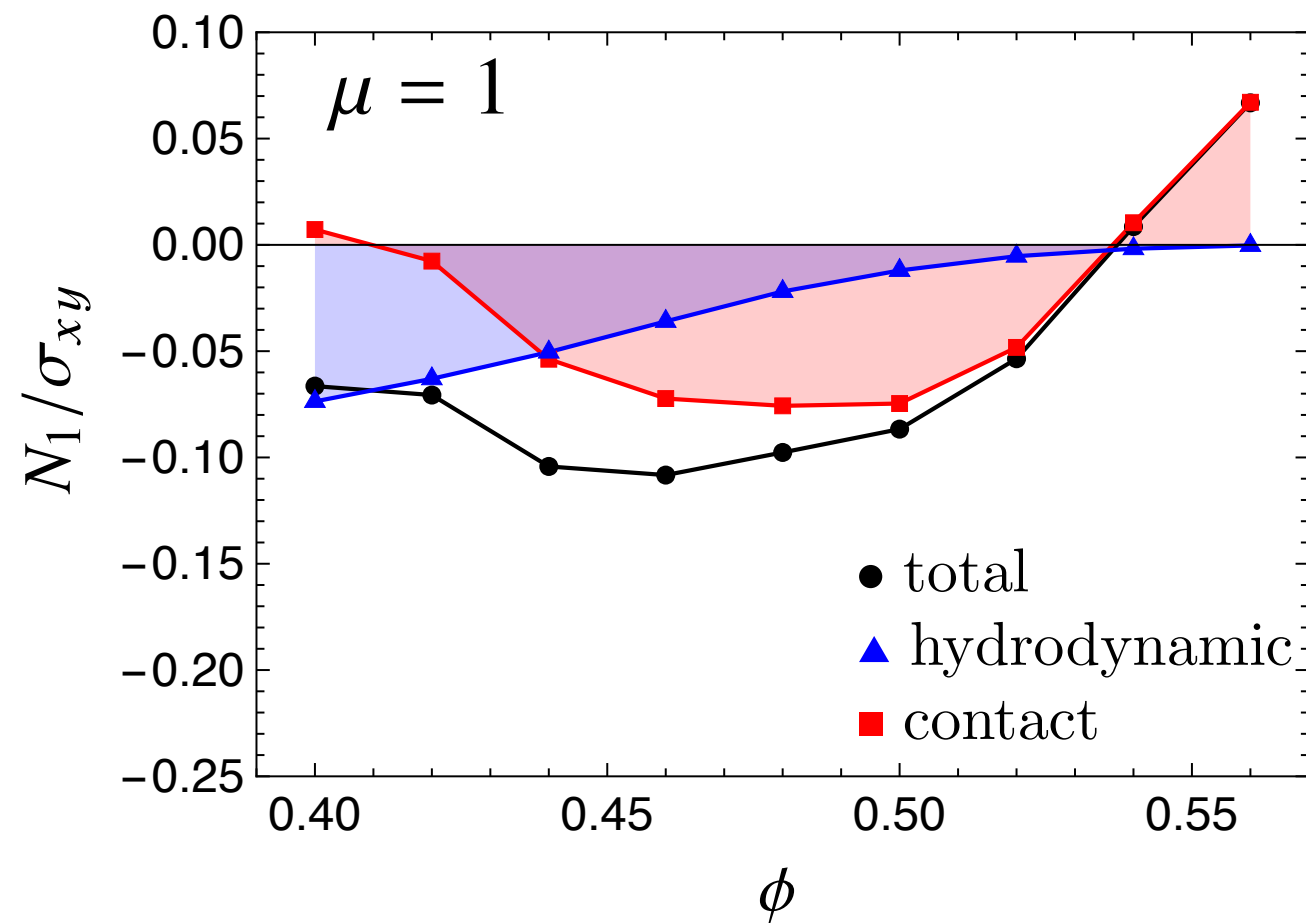
hydrodynamics interaction
(frictionless)



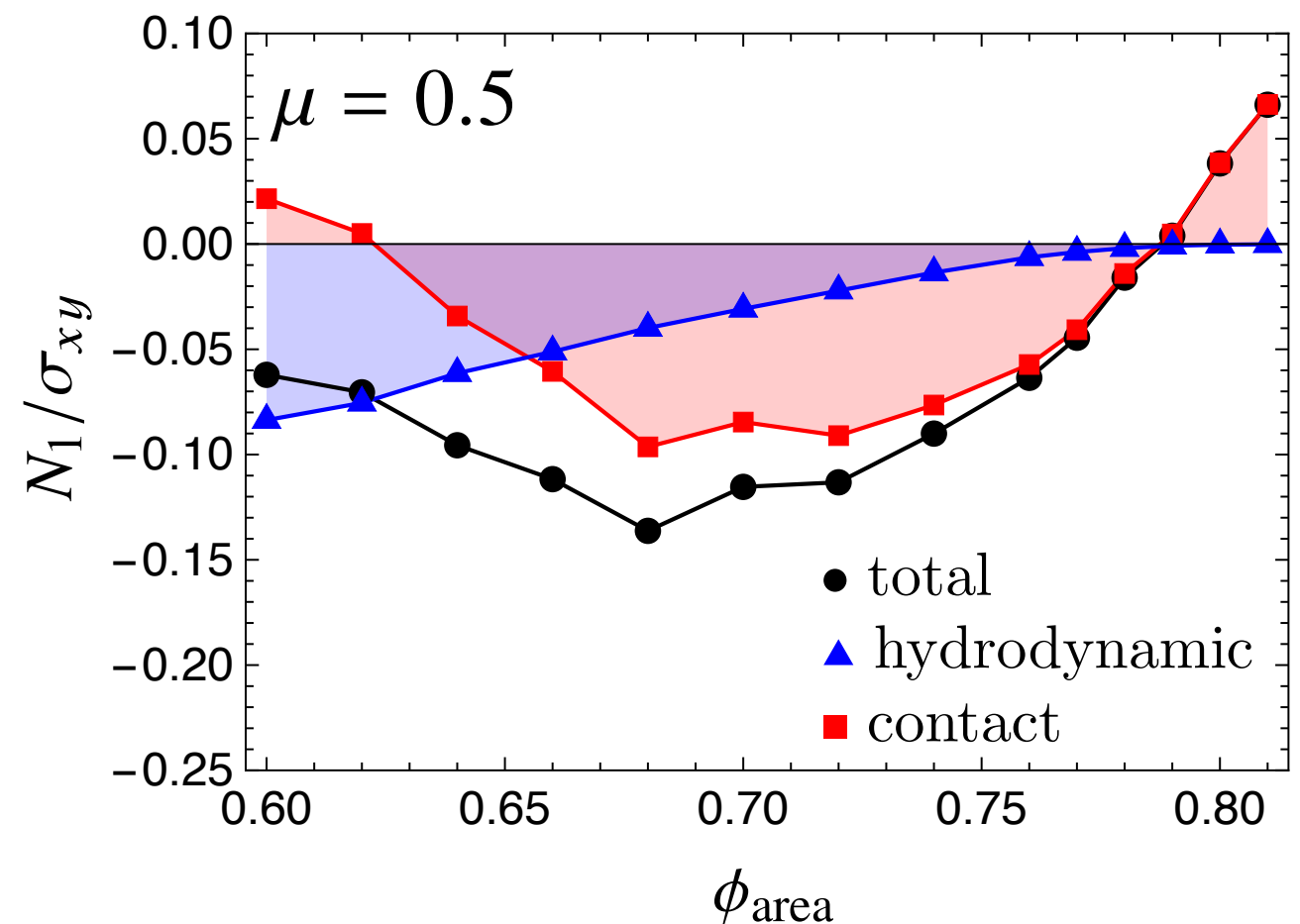
→ Hydrodynamic interaction may be essential for the microstructure giving the negative N_1 .

Monolayer simulation gives similar results

3D simulation



2D (monolayer) simulation



2D (monolayer) simulations
are easier for visualization and data analysis.

Approximation of N_1 using only normal forces

$$\bar{F}_{ij} \equiv -\mathbf{F}^{(ij)} \cdot \mathbf{n}^{(ij)}$$

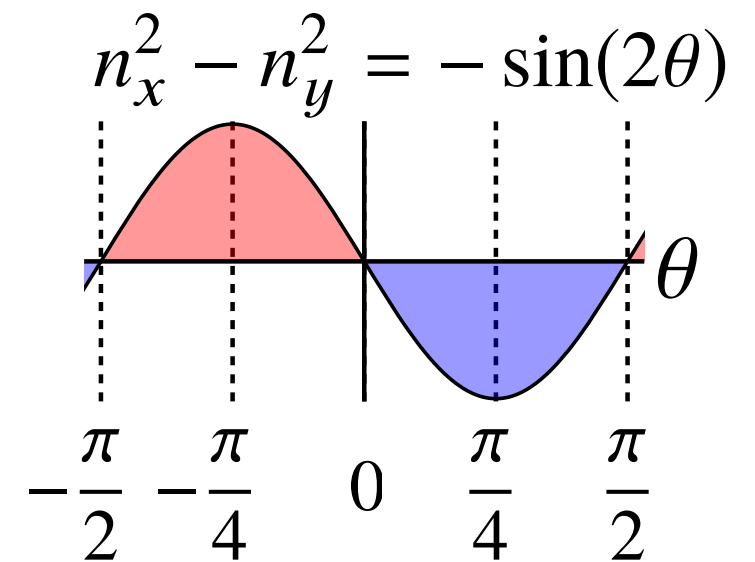
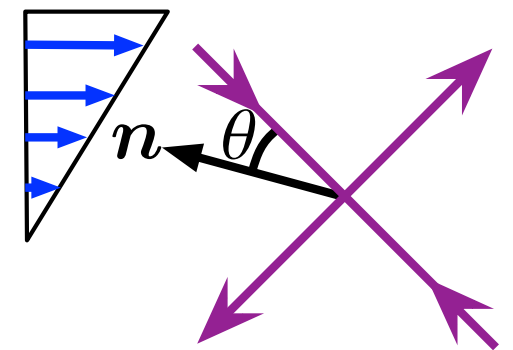
$$\bar{\mathbf{F}}^{(ij)} = \bar{F}_{ij} \mathbf{n}^{(ij)}$$

Stress tensor using only normal forces

$$\tilde{\sigma} \equiv -p\mathbf{I} + 2\eta_0\mathbf{D} + V^{-1} \sum (\mathbf{r}^j - \mathbf{r}^i) \bar{\mathbf{F}}^{(ij)}$$

First normal stress difference using only normal forces

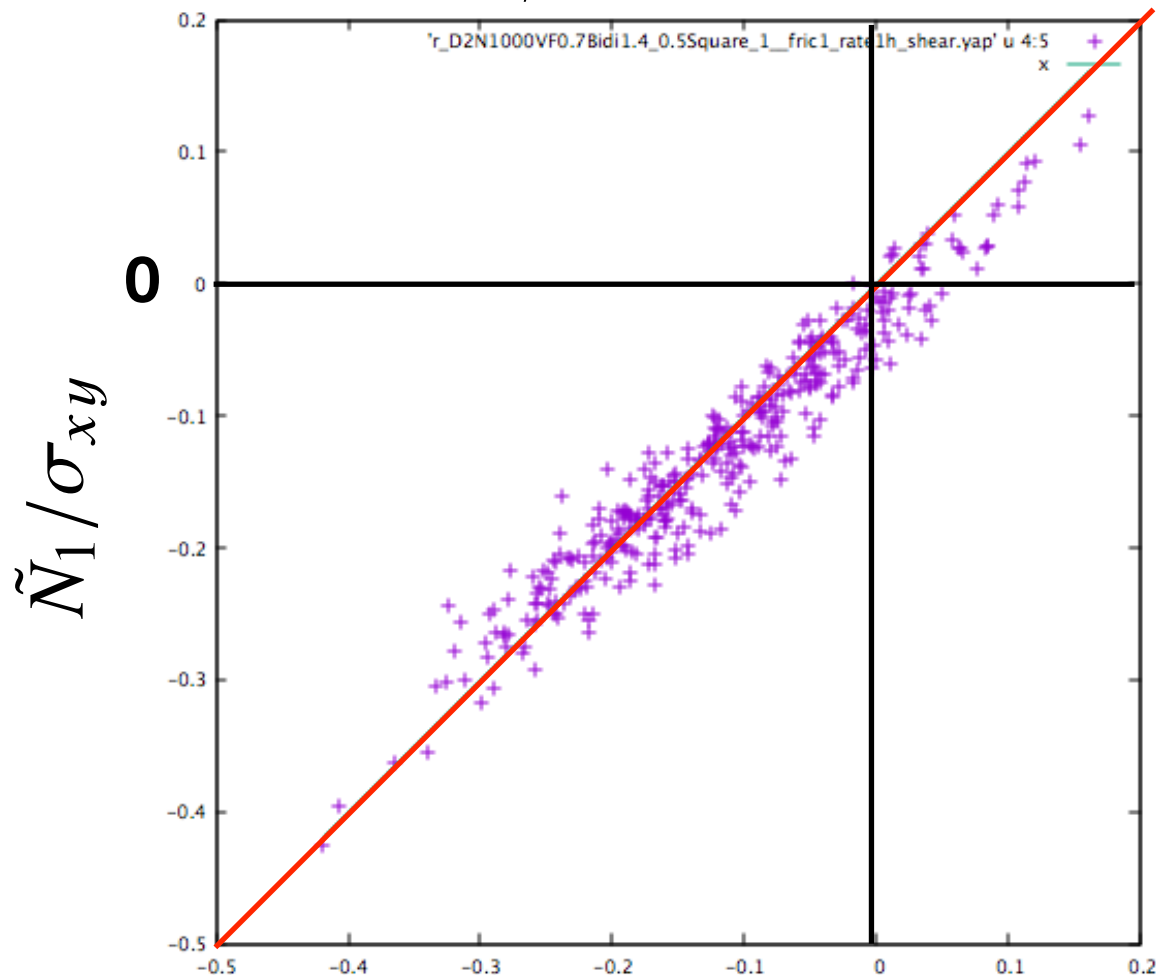
$$\begin{aligned} \tilde{N}_1 &\equiv \tilde{\sigma}_{xx} - \tilde{\sigma}_{yy} \\ &= V^{-1} \sum_{i>j} r_{ij} \bar{F}_{ij} \left[\left(n_x^{(ij)} \right)^2 - \left(n_y^{(ij)} \right)^2 \right] \\ &= V^{-1} \sum_{i>j} \left(-r_{ij} \bar{F}_{ij} \sin 2\theta_{ij} \right) \\ &= \sum_{i>j} \tilde{N}_1^{ij} \end{aligned}$$



The approximated N_1 works

$$\phi_{\text{area}} = 0.7$$

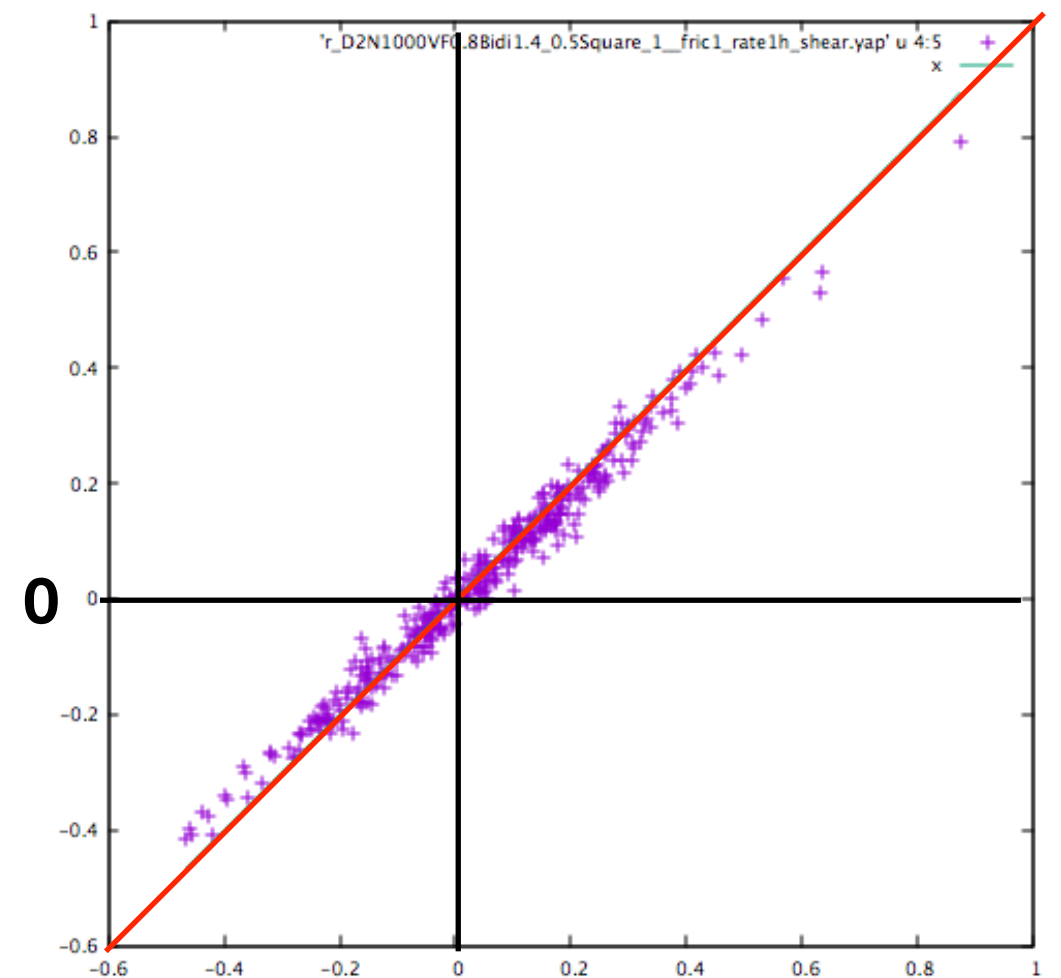
(using only normal forces)



N_1/σ_{xy}
(using all forces)

(using only normal forces)

$$\phi_{\text{area}} = 0.8$$

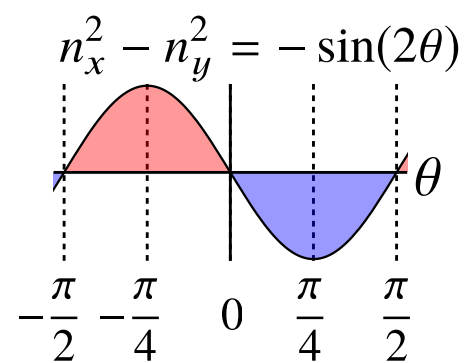
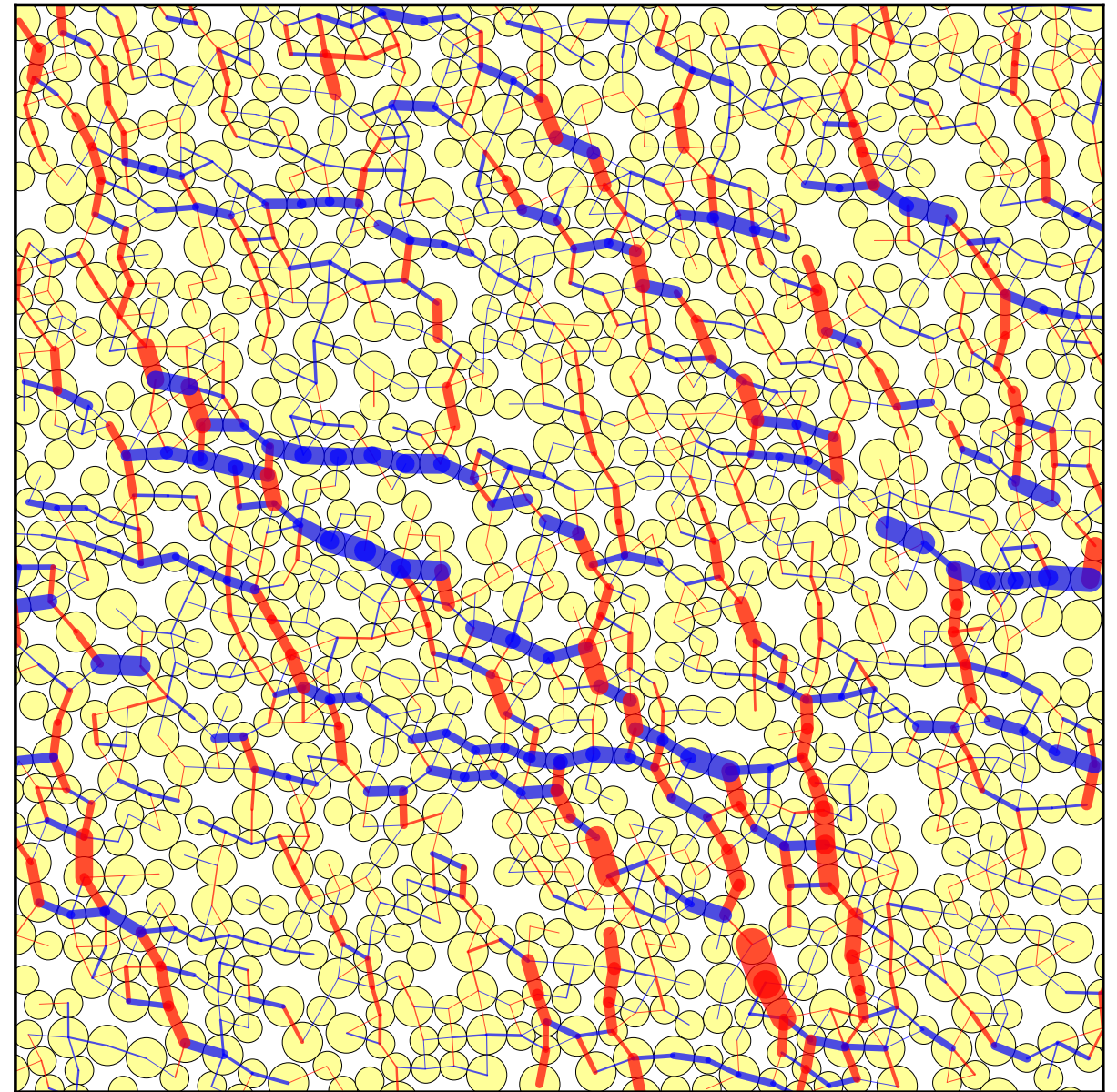
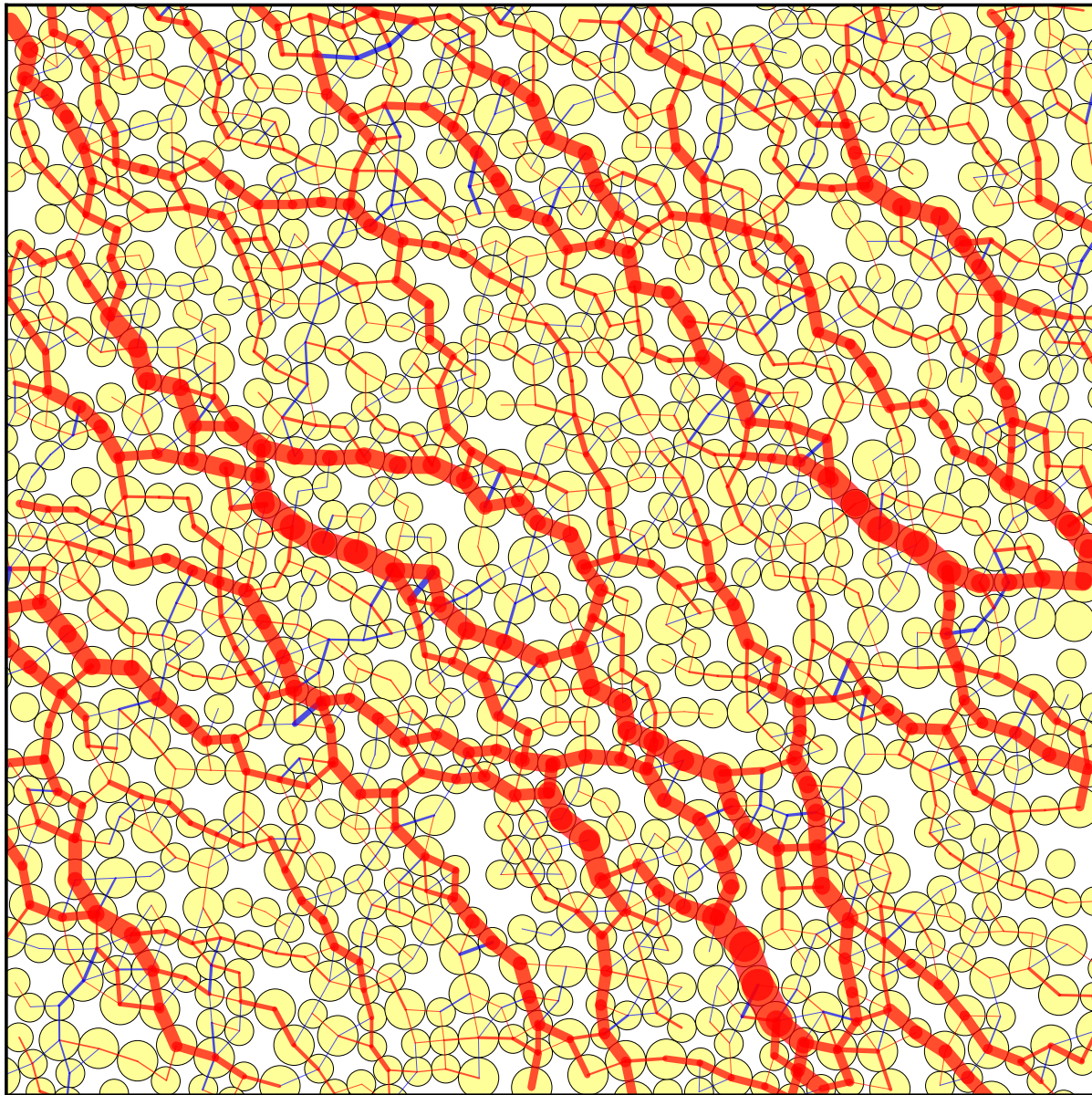


N_1/σ_{xy}
(using all forces)

$$\phi_{\text{area}} = 0.7$$

$$\bar{F}_{ij} \equiv -\mathbf{F}^{(ij)} \cdot \mathbf{n}^{(ij)}$$

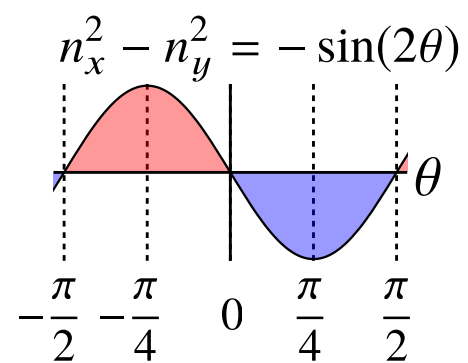
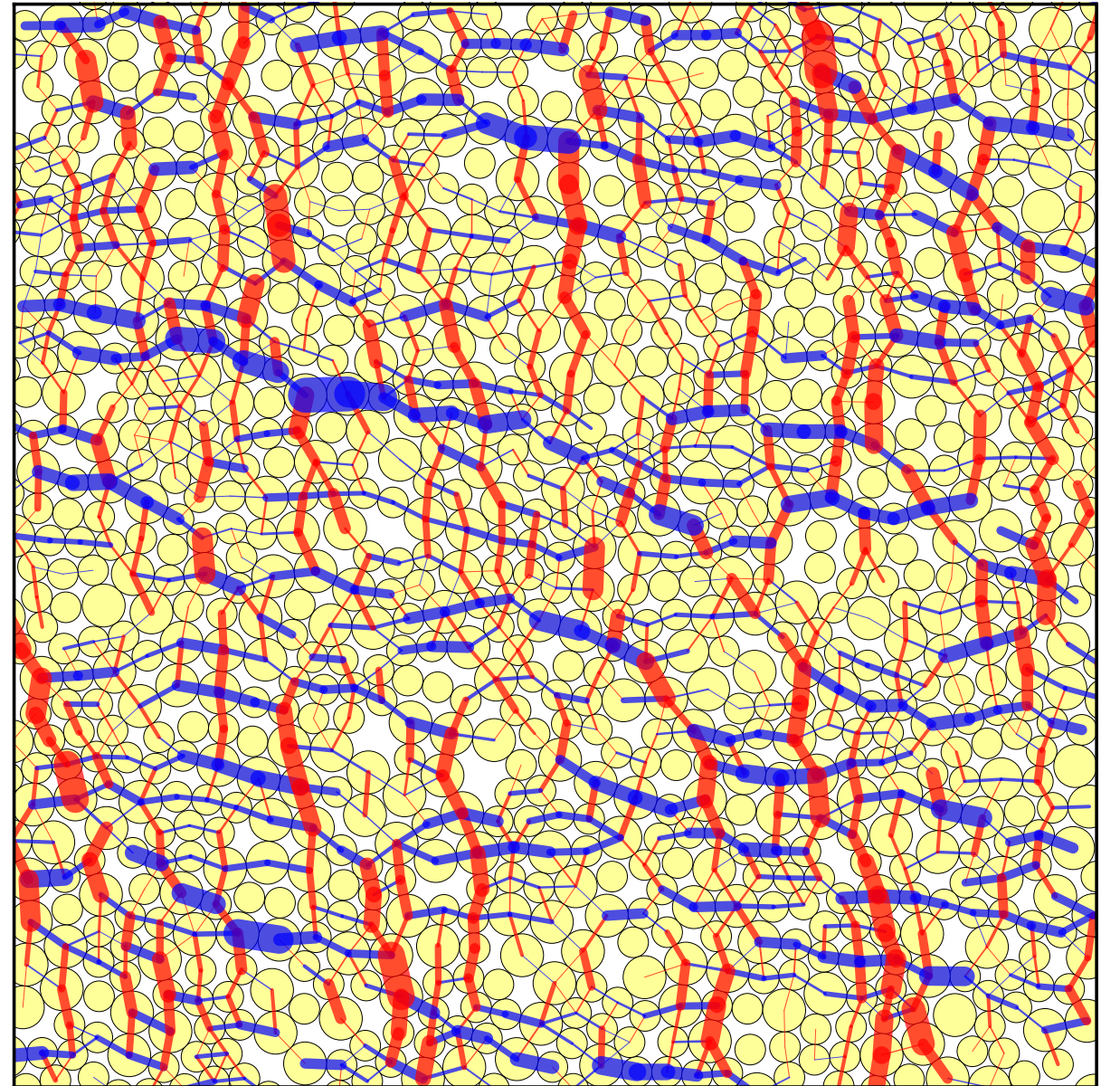
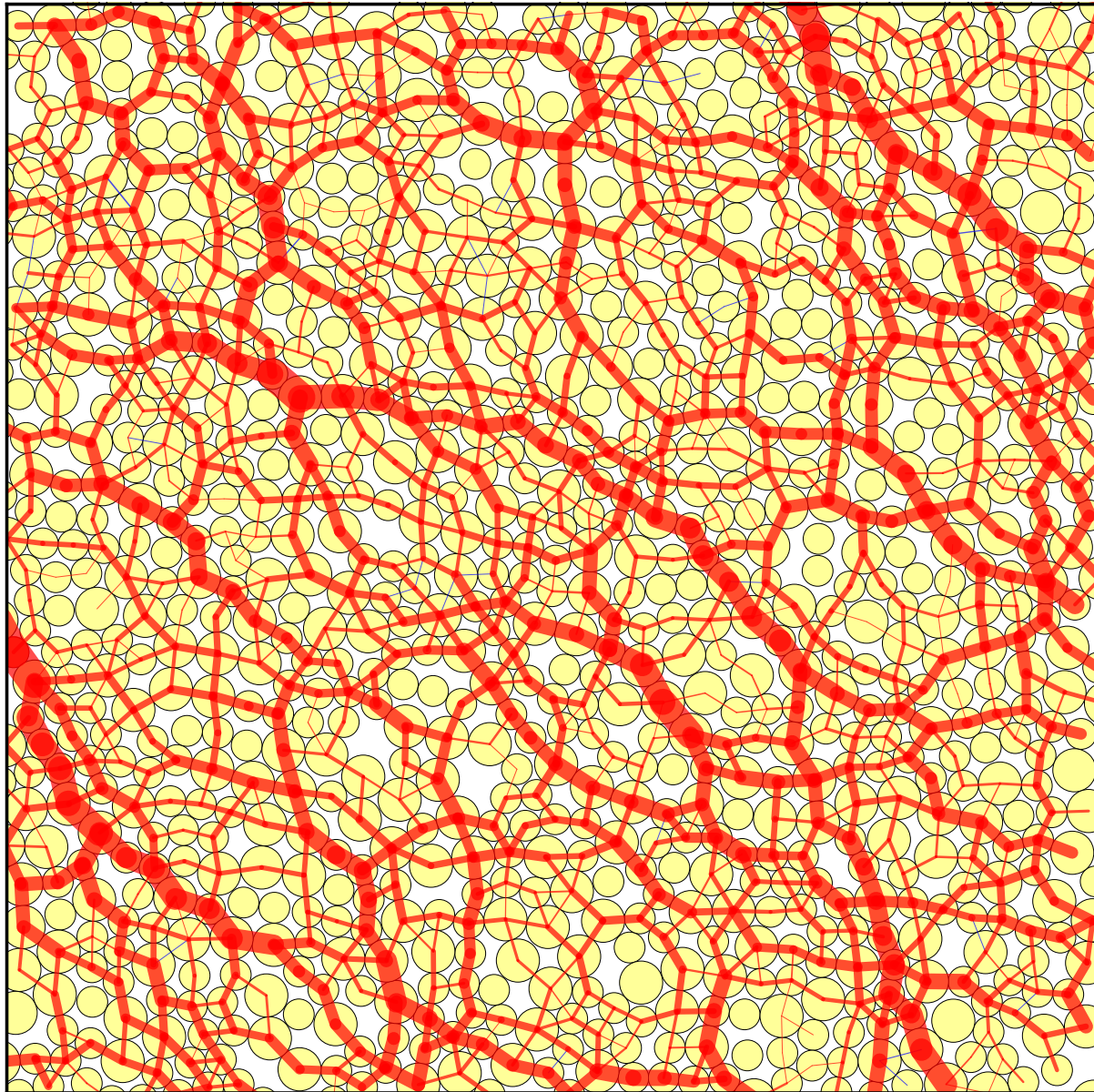
$$\tilde{N}_1^{ij} \equiv r_{ij} \bar{F}_{ij} \sin(2\theta_{ij})/V$$



$$\phi_{\text{area}} = 0.8$$

$$\bar{F}_{ij} \equiv -\mathbf{F}^{(ij)} \cdot \mathbf{n}^{(ij)}$$

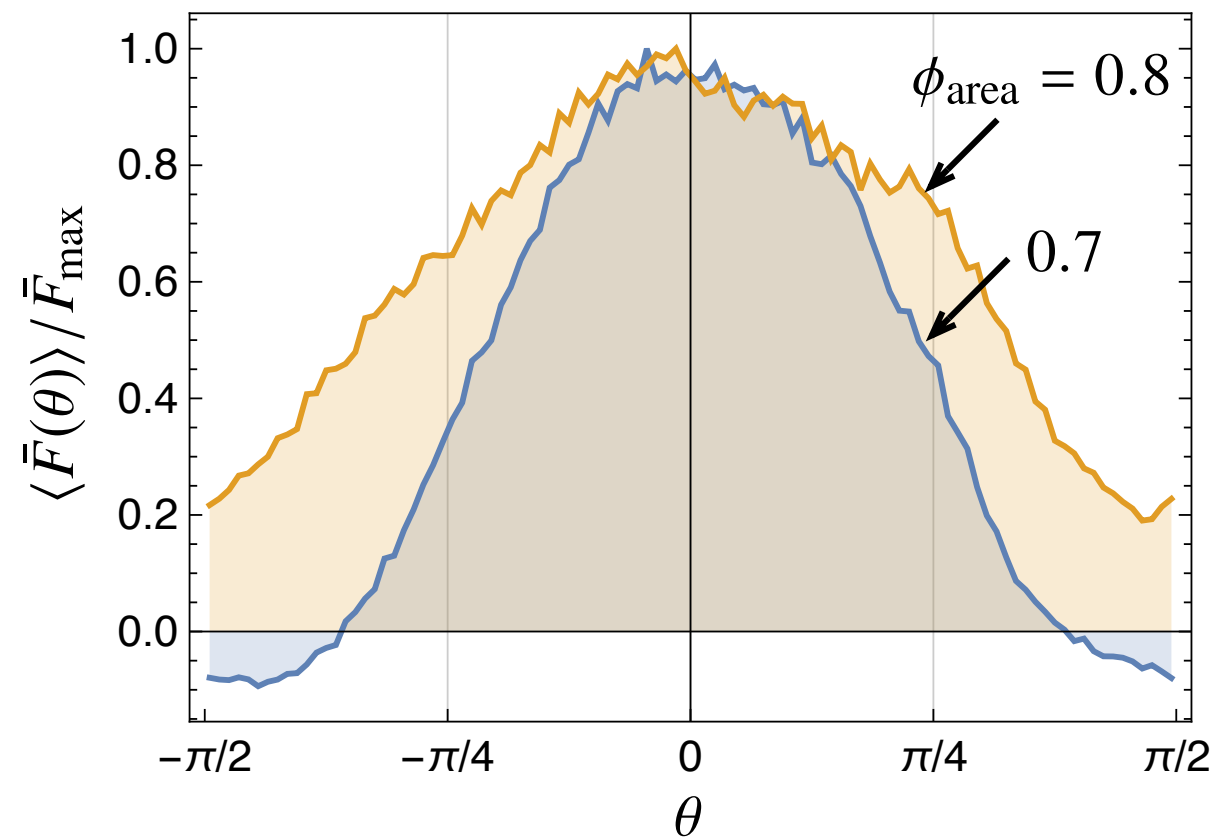
$$\tilde{N}_1^{ij} \equiv r_{ij} \bar{F}_{ij} \sin(2\theta_{ij}) / V$$



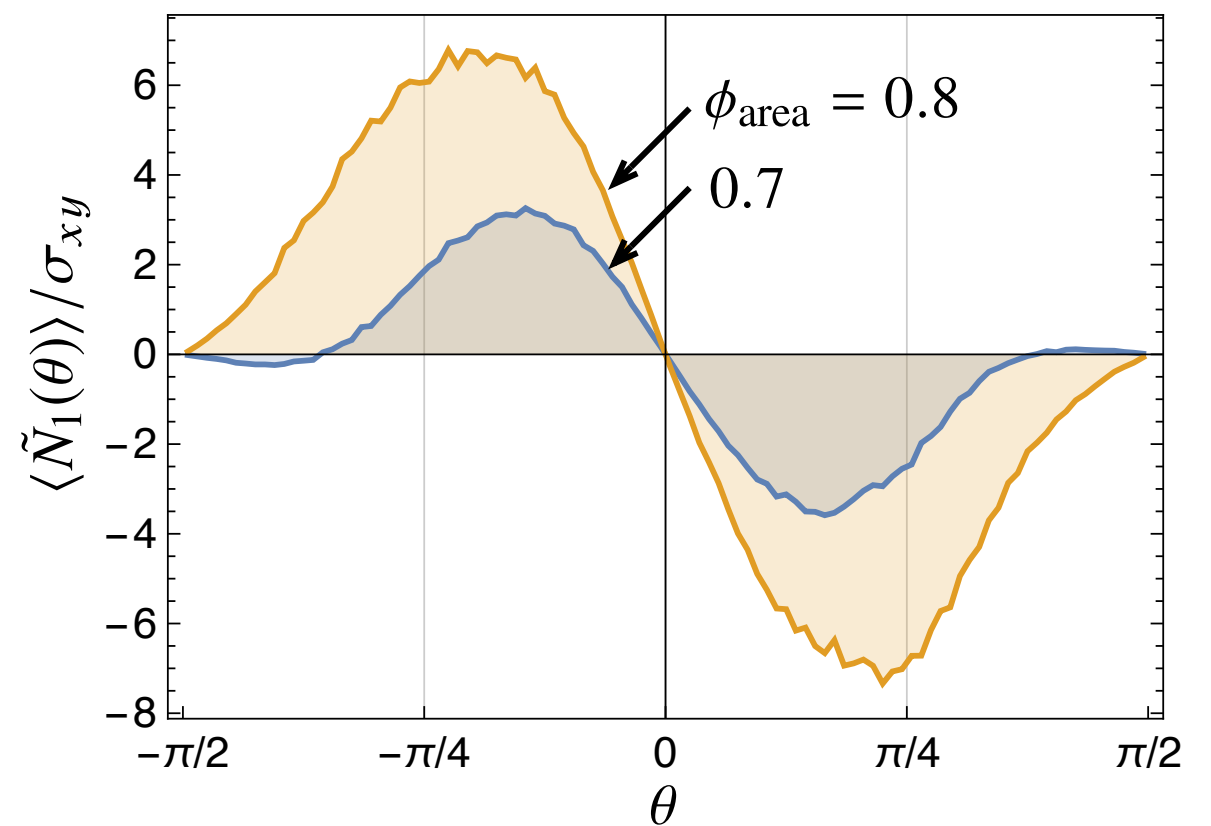
Angular distribution

normal force

$$\bar{F}_{ij} \equiv -\mathbf{F}^{(ij)} \cdot \mathbf{n}^{(ij)}$$

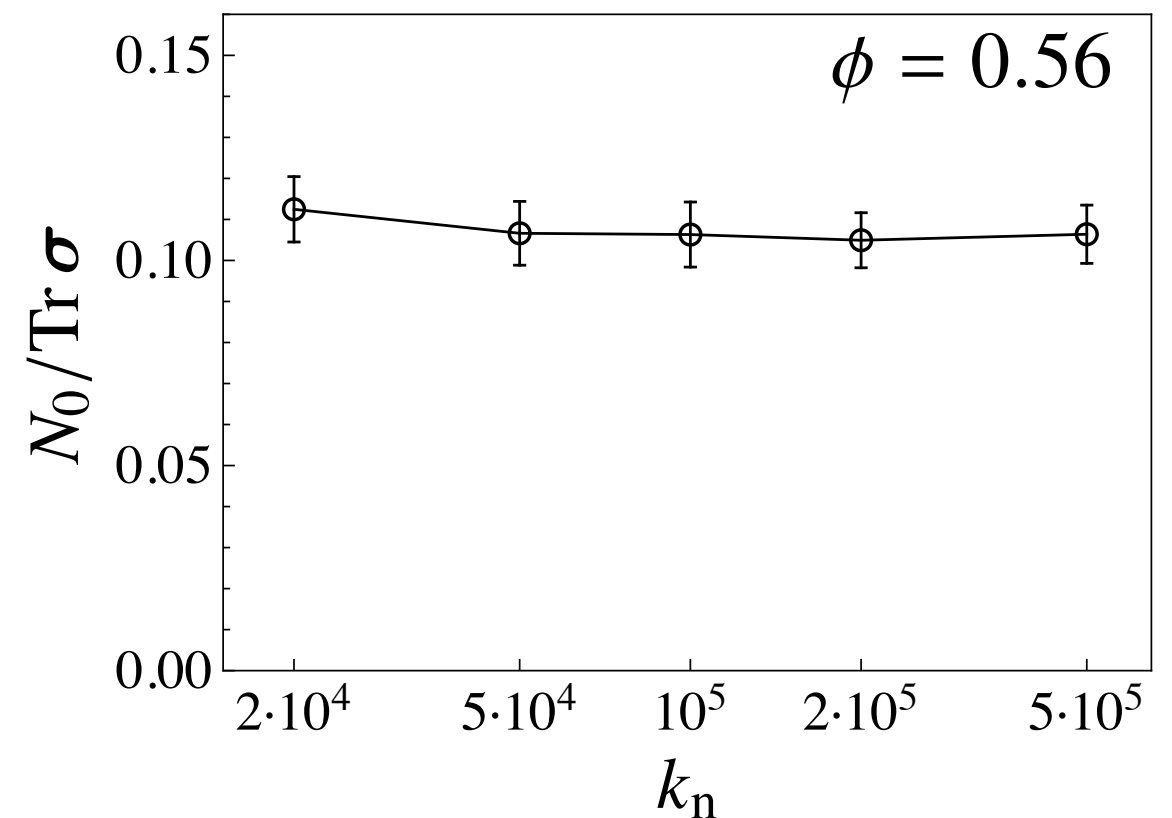
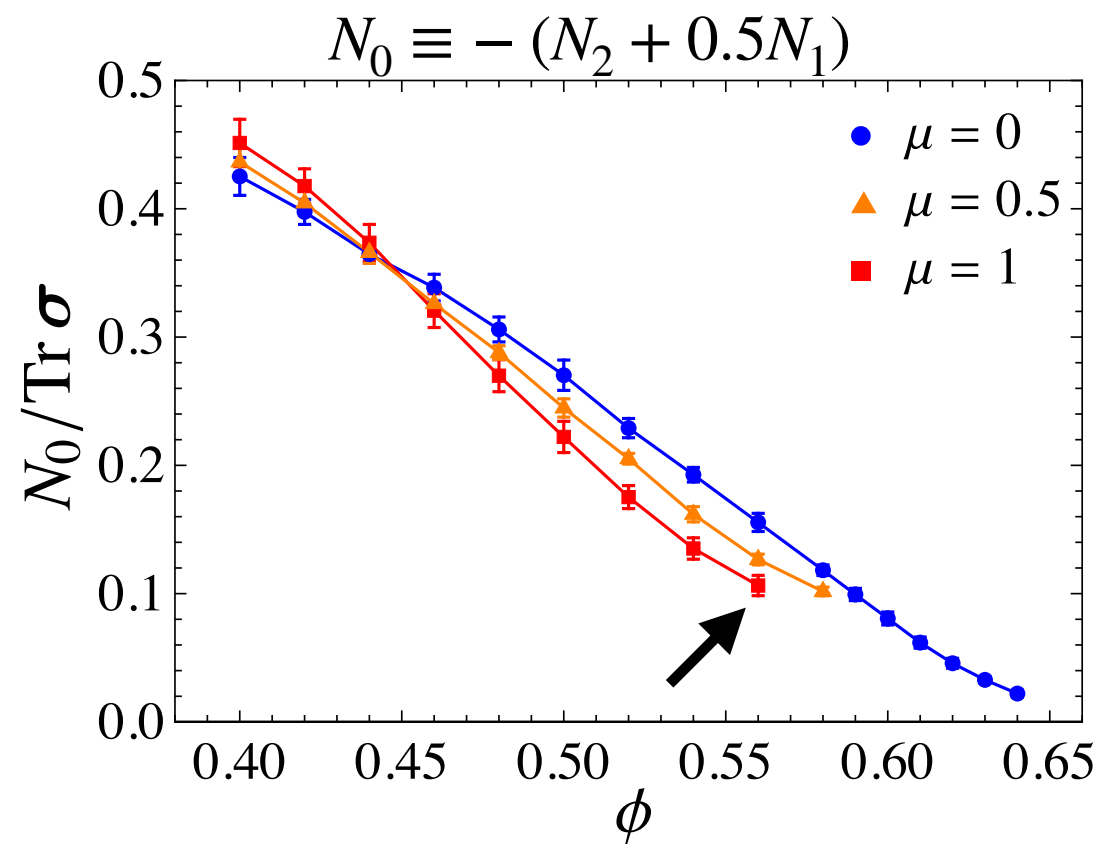
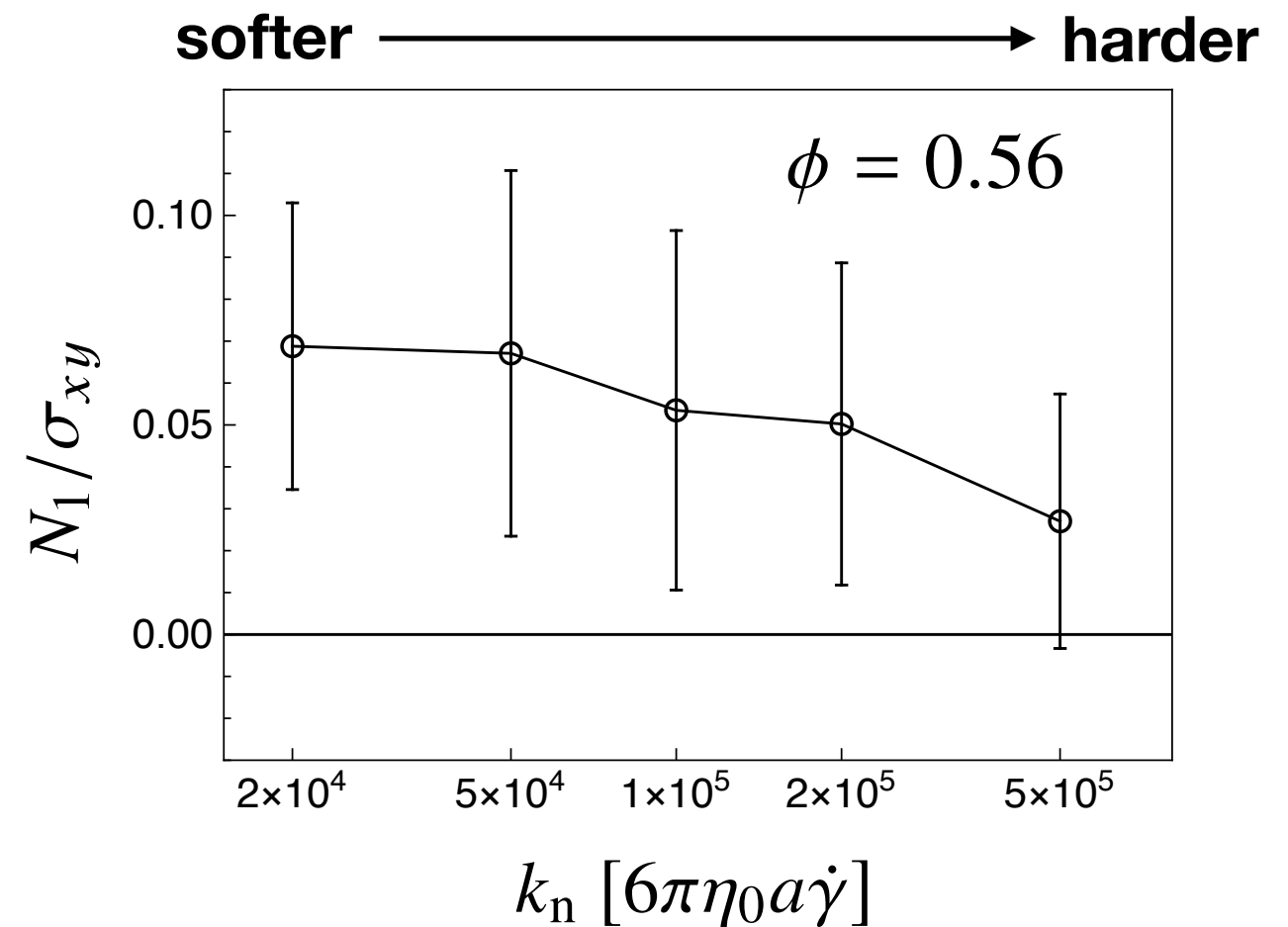
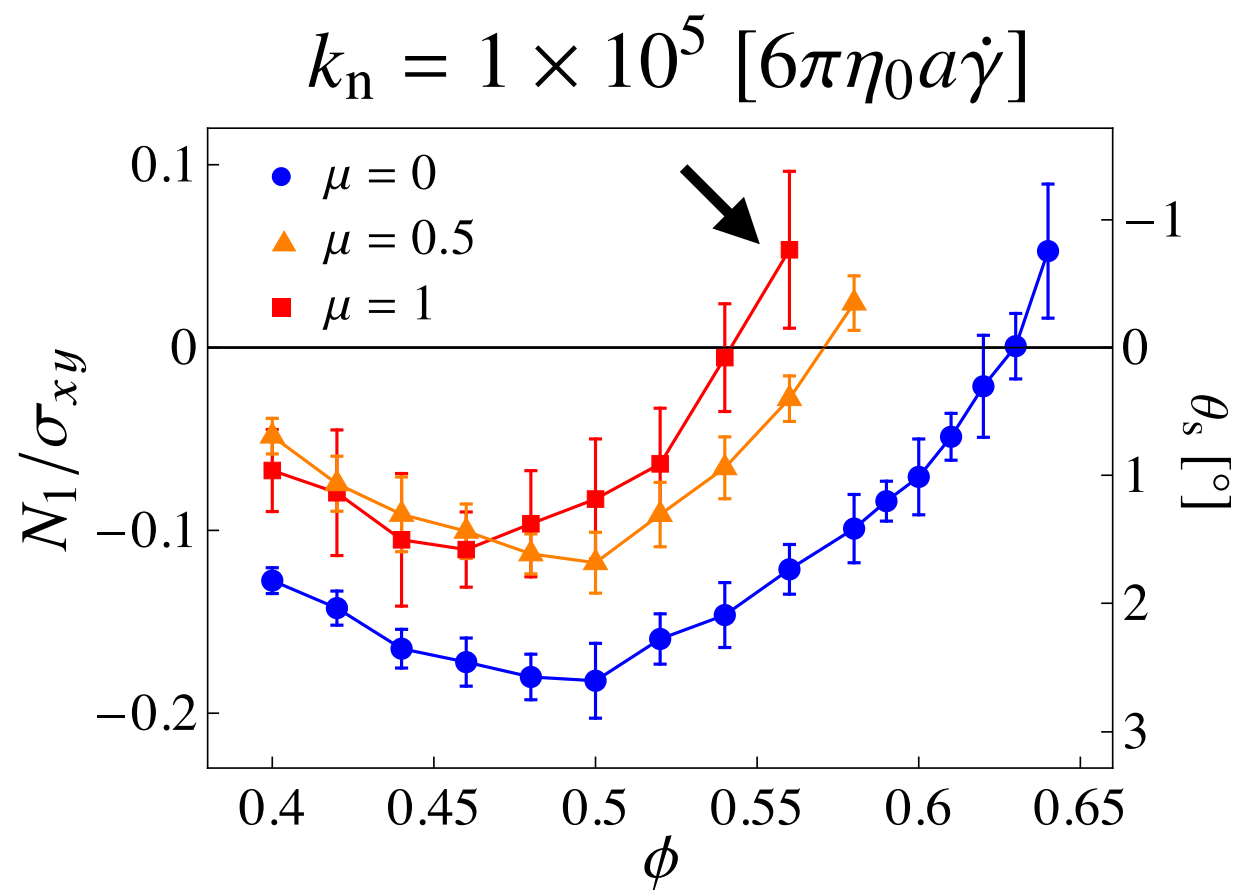


$$\tilde{N}_1^{ij} / \sigma_{xy}$$



$$N_1 \approx \frac{1}{\pi} \int_{-\pi/2}^{\pi/2} \langle \tilde{N}_1(\theta) \rangle d\theta$$

Anisotropies exist at jamming points of hard spheres?



Summary

Smallness of the reorientation angle.
(Observed finite N_1 due to high shear stress)

Large N_1 fluctuation around zero
due to competition between **positive** and **negative** contributions

Positive N_1 in simulation is due to softness of particles.

