

Glassy rheology: Combining microscopic theory and macroscopic fluid mechanics

Thomas Voigtmann

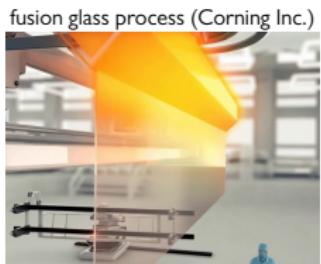
Theory of Soft Matter Group, DLR Cologne and University of Düsseldorf

Kyoto, October 2018

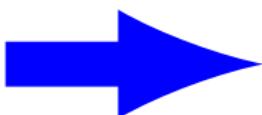
Process-Dependent Material Properties



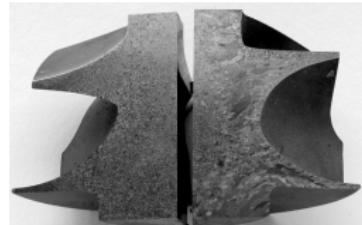
metallic melt (courtesy DLR Cologne)



fusion glass process (Corning Inc.)



*processing
solidification*

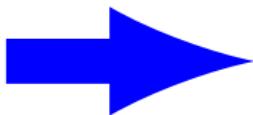


turbo charger gears
(courtesy ACCESS e.V. Aachen)

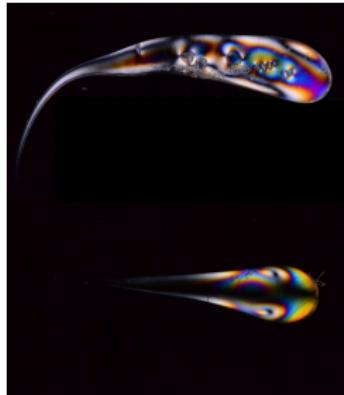


“materials design from the melt”

Residual Stresses: Prince Rupert's Drops



process



- **residual stresses** frozen in during production process
- **spatial stress patterns** determine material toughness
- other applications: spider silk, railway rails, ...

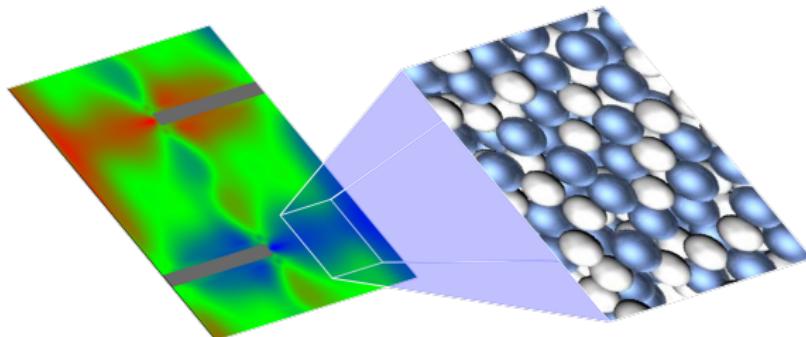


Residual Stresses: Prince Rupert's Drops



[video: Smarter Every Day, <http://www.youtube.com/user/destinws2>]

Multiscale Theory/Simulation

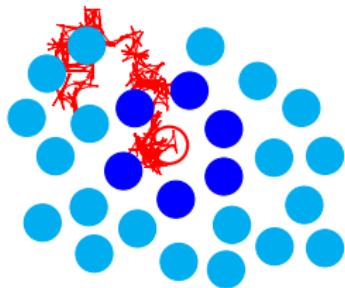


(basis for empirical) material laws \Leftarrow nonlinear-response theory

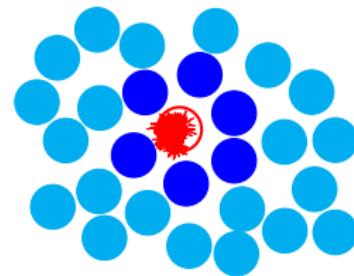
time-dependent, history-dependent material properties

... of soft matter, viscous melts, active materials etc.

Glasses: Liquid-Structured Solids



fluid: finite *viscosity*



glass: finite *elasticity*

slow dynamics ($\tau \rightarrow \infty$) \Rightarrow generic behavior

empirical: Maxwell model

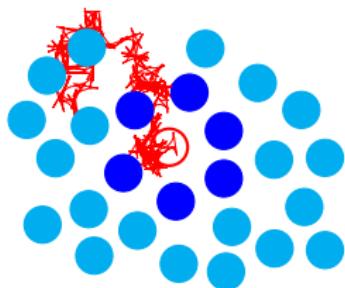
$$\sigma(t) = \int_{-\infty}^t \dot{\gamma}(t') G_\infty e^{-(t-t')/\tau} dt'$$



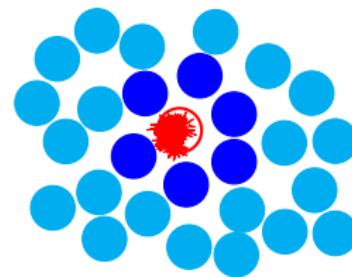
[U Queensland, Australia (1927–now); <http://smp.uq.edu.au/content/pitch-drop-experiment>]



Glasses: Liquid-Structured Solids



fluid: finite *viscosity*



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empirical: Maxwell model

$$\sigma(t) = \int_{-\infty}^t \dot{\gamma}(t') G_\infty e^{-(t-t')/\tau} dt'$$

$Pe = \dot{\gamma}\tau \gg 1$: nonlinear response phenomena



Outline

➤ Microscopic Dynamics

Mode-Coupling Theory (Rheology)

➤ Continuum Description

Hybrid Simulations

Empirical Models

Microscopic Dynamics

Mode-Coupling Theory (Rheology)

Nonlinear Response Theory

nonequilibrium phase-space density $\rho(\Gamma, t)$:

$$\partial_t \rho(\Gamma, t) = (\Omega_{\text{eq}}(\Gamma) + \delta\Omega(\Gamma, t)) \rho(\Gamma, t)$$

formal solution for **nonequilibrium averages**

$$\rho(t) = \rho_{\text{eq}} + \int_{-\infty}^t dt' \exp_+ \left[\int_{t'}^t \Omega(\tau) d\tau \right] \Omega(t') \rho_{\text{eq}}$$

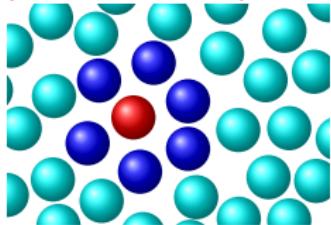
$$\langle f \rangle(t) = \langle f \rangle_{\text{eq}} + \int_{-\infty}^t dt' \left\langle \left[\frac{\delta\Omega(t') \rho_{\text{eq}}}{\rho_{\text{eq}}} \right] \exp_- \left[\int_{t'}^t \Omega^\dagger(\tau) d\tau \right] f \right\rangle_{\text{eq}}$$

for example: **stresses**

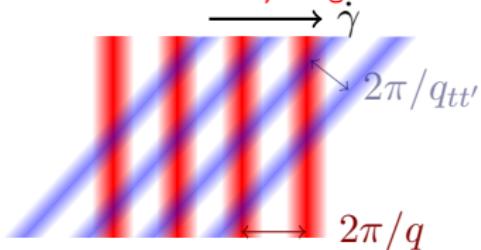
$$\boldsymbol{\sigma}(t) \sim \int_{-\infty}^t dt' \cdots \underbrace{[-\partial_{t'} \mathbf{B}(t, t')]}_{\text{deformation measure (Finger tensor)}} \cdots G(t, t', [\vec{\nabla} \vec{v}])$$

Mode Coupling Theory: Microscopic Approach

cage effect: $\tau \rightarrow \infty$
slow dynamics of density fluctuations



fluctuation advection: $\tau \sim 1/\dot{\gamma}$
shear destroys cages

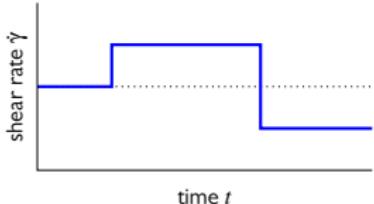


$$\sigma(t) \sim \int_{-\infty}^t dt' \dots \vec{\nabla} \vec{v}(t') \dots G(t, t', [\vec{\nabla} \vec{v}])$$

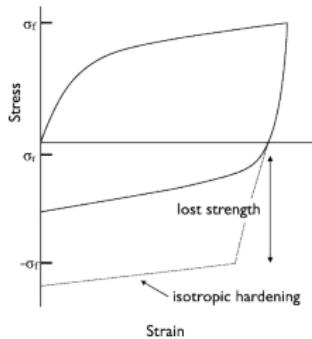
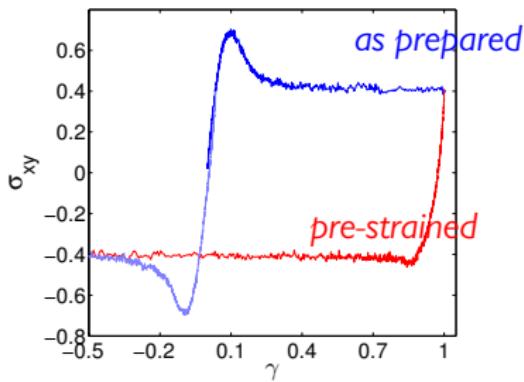
$$G(t, t') \stackrel{\text{MCT}}{=} \int d\vec{k} \dots \phi_{\vec{k}}^2(t, t')$$

$$\tau_0 \partial_t \phi_{\vec{k}}(t, t') + \phi_{\vec{k}}(t, t') + \int_{t'}^t m_{\vec{k}}([\phi], [\vec{\nabla} \vec{v}], t, t'', t') \partial_{t''} \phi_{\vec{q}}(t'', t') dt' = 0$$

Limits of Elasticity – Bauschinger Effect



measure shear stress $\sigma(t)$
under *deformation reversal*
⇒ history-dependent elastic modulus G_{eff}

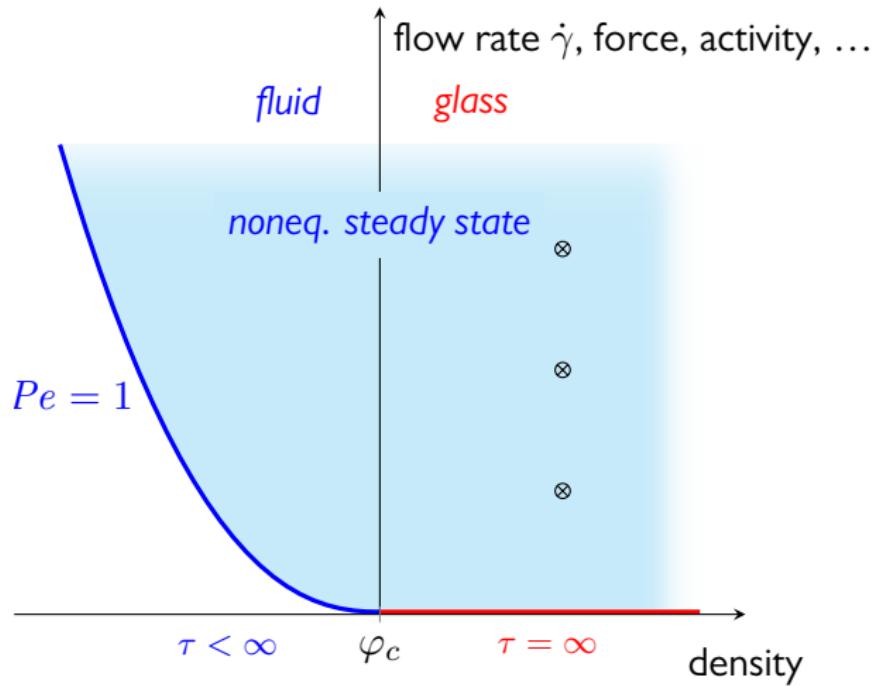


[Kassner, International Journal of Plasticity (2013)]

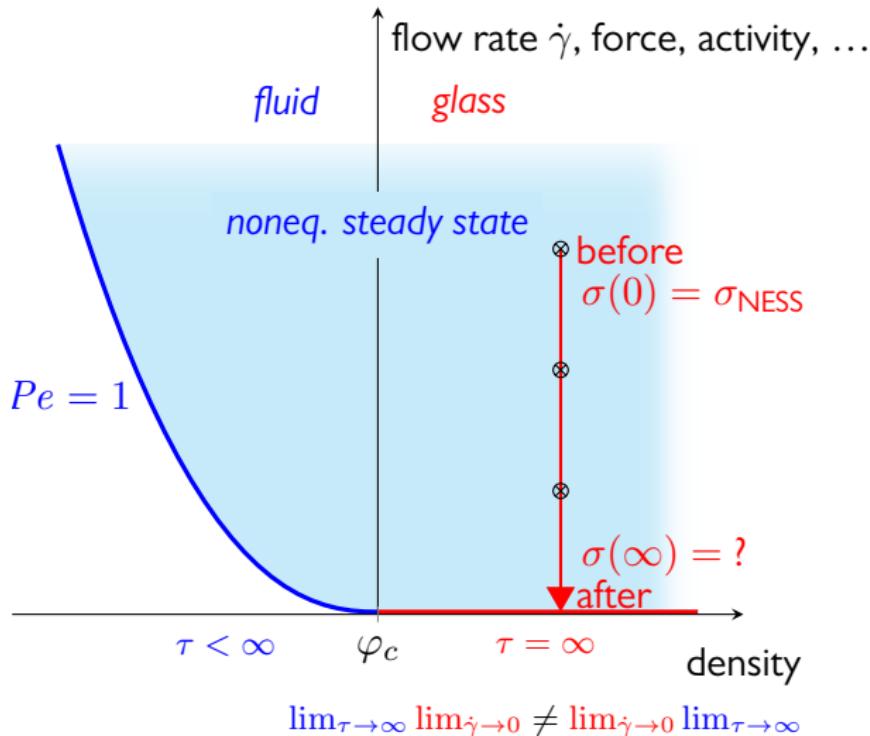
- microscopic explanation for empirical “Bauschinger effect”



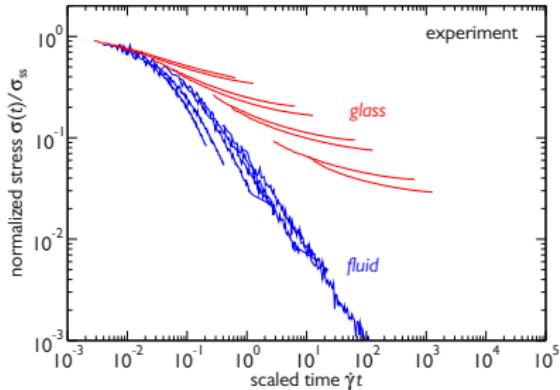
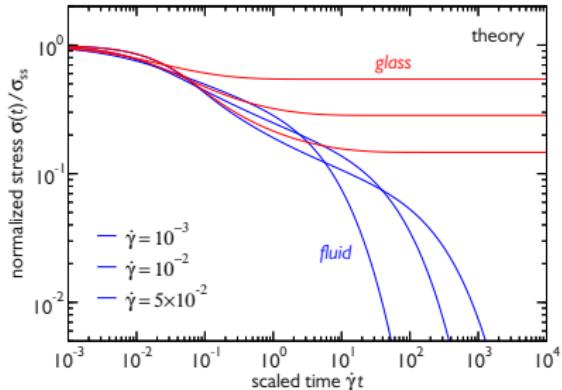
Stopping Flow



Stopping Flow



Residual Stresses: Microscopic Theory



- residual stress: true nonlinear-response effect

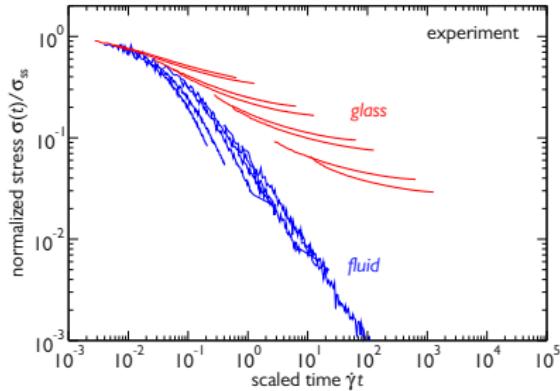
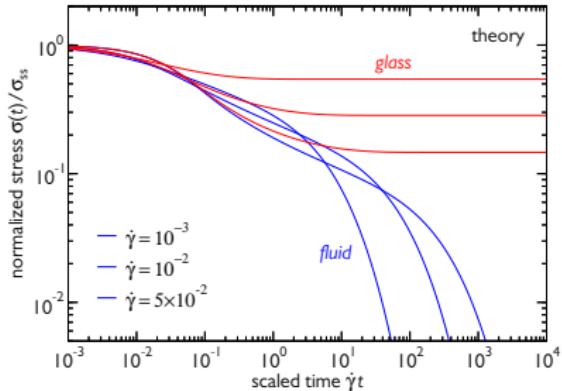
non-stationary flow:
$$\sigma(\dot{\gamma}, t) \sim \int^t \dot{\gamma}(t') G(t, t'; [\dot{\gamma}]) dt'$$

- theory: homogeneous shear, instantaneously stopped

[Ballauff et al., Phys Rev Lett **110**, 215701 (2013)]

[Physics (Focus article) **6**, 60 (2013)]

Residual Stresses: Microscopic Theory



- residual stress: true nonlinear-response effect

non-stationary flow:
$$\sigma(\dot{\gamma}, t) \sim \int^t \dot{\gamma}(t') G(t, t'; [\dot{\gamma}]) dt'$$

- theory: homogeneous shear, instantaneously stopped

this makes a huge difference!

Continuum Description

Continuum Description

Hybrid Simulations

Macroscopic Modeling

Navier Stokes equations

$$\underbrace{\rho \left[\partial_t \vec{v} + (\vec{v} \cdot \vec{\nabla}) \vec{v} \right]}_{\text{balance law of momentum}} = \underbrace{\rho \vec{f}^{\text{ext}} - \vec{\nabla} p}_{\text{friction}} + \vec{\nabla} \cdot \boldsymbol{\sigma}$$



need **constitutive equation** for $\boldsymbol{\sigma}$ (closure relation)

$$\boldsymbol{\sigma}(t) = \mathcal{F} [(\vec{\nabla} \vec{v})_{t' \leq t}, \dots]$$

historically,
“educated guesses”

The diagram shows two rectangular blocks. The left block is blue and has a vertical velocity profile. The right block is pink and has a horizontal displacement profile. Arrows indicate the direction of motion.

$$\dot{\gamma} = dv_x/dy$$

Newton (1687)
 $\sigma = \eta \dot{\gamma}$
resistentiam ...
proportionalem esse velocitati

$$\gamma = \Delta x/\Delta y$$

Hooke (1676)
 $\sigma = G_\infty \gamma$
ut tensio, sic vis



how to derive constitutive equations from *microscopic principles*?

Multi-Scale Computational Fluid Dynamics

Navier Stokes

$$\rho[\partial_t \vec{v} + (\vec{v} \cdot \vec{\nabla})\vec{v}] = \rho \vec{f} - \vec{\nabla} p + \vec{\nabla} \cdot \boldsymbol{\sigma}$$

constitutive equation

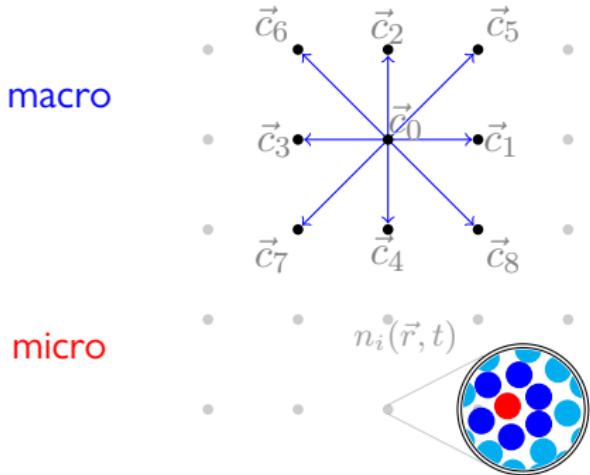
microscopic dynamics

$$\boldsymbol{\sigma}(t) = \int^t dt' [-\partial_{t'} \mathbf{B}(t, t')] G(t, t', [\mathbf{B}])$$

$$n_i(\vec{r} + \vec{c}_i \delta t, t + \delta t) = n_i(\vec{r}, t) - \frac{1}{\tau_{LB}} [n_i(\vec{r}, t) - n_i^{eq}(\vec{r}, t)] + \mathbf{F}_i$$

$$\text{physical fields } \rho = \sum_i n_i^{eq}, \vec{v} = \sum_i \vec{c}_i n_i^{eq}$$

$$\mathbf{F}_i = \frac{-a^{ci}}{2c_s^4 \tau_{LB}} \bar{\boldsymbol{\sigma}}^{\text{non-Newt}}[(\vec{\nabla} \vec{v})] : (\vec{c}_i \vec{c}_i - c_s^2 \mathbf{1})$$



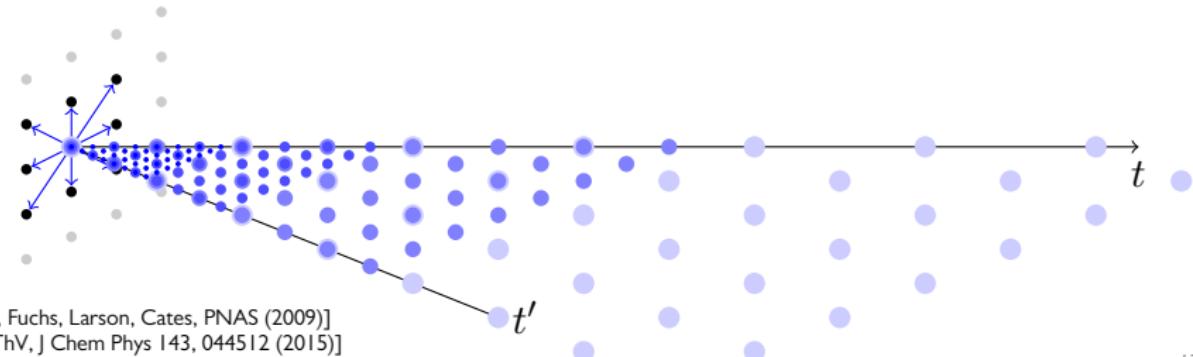
Integral Constitutive Equations

nasty task: need to solve Navier Stokes + integral equations

$$\boldsymbol{\sigma}(t) = \int_{t'}^t dt' [-\partial_{t'} \mathbf{B}_{tt'}] \phi^2(t, t', [\mathbf{B}])$$

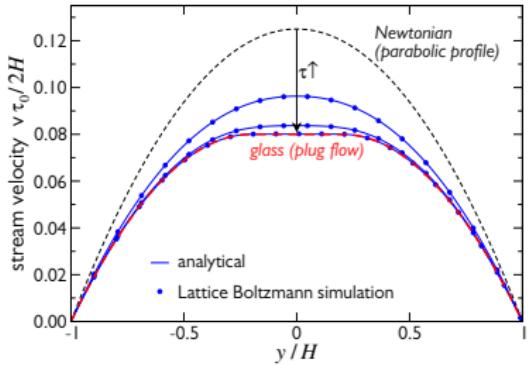
history effects \Rightarrow generalized Langevin equation

$$0 = \tau_0 \partial_t \phi(t, t') + \phi(t, t') + \int_{t'}^t dt'' m(t, t'', t') \partial_{t''} \phi(t'', t')$$
$$m(t, t'', t') = h(\mathbf{B}_{tt''}) h(\mathbf{B}_{tt'}) \mathcal{F}[\phi(t, t'')]$$



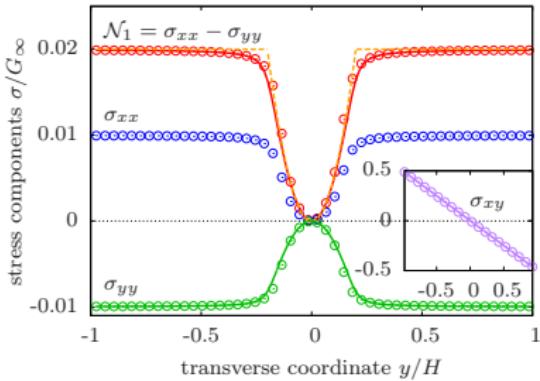
[Brader, ThV, Fuchs, Larson, Cates, PNAS (2009)]
[Papenfort, ThV, J Chem Phys 143, 044512 (2015)]

Plug Flow

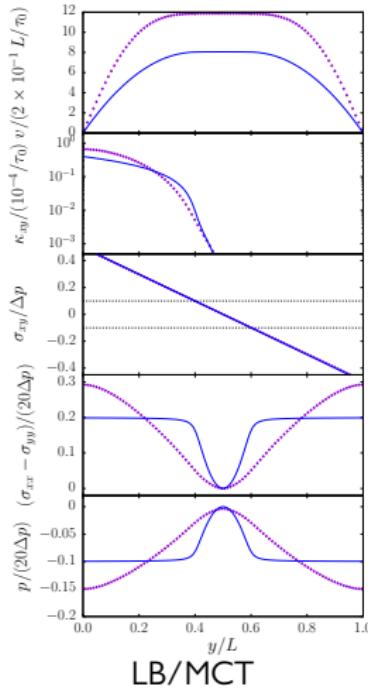


- yield stress \Rightarrow plug flow
- LB resolves analytical solution
- large normal stress coefficient

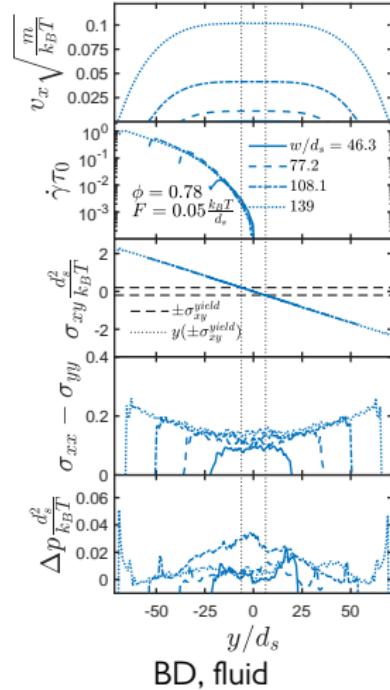
$$\mathcal{N}_1 = (\sigma_{xx} - \sigma_{yy})/\dot{\gamma}^2$$



Theory and Brownian Dynamics (BD) Simulations



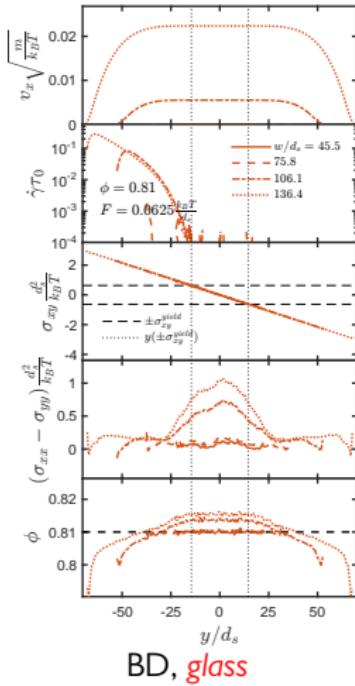
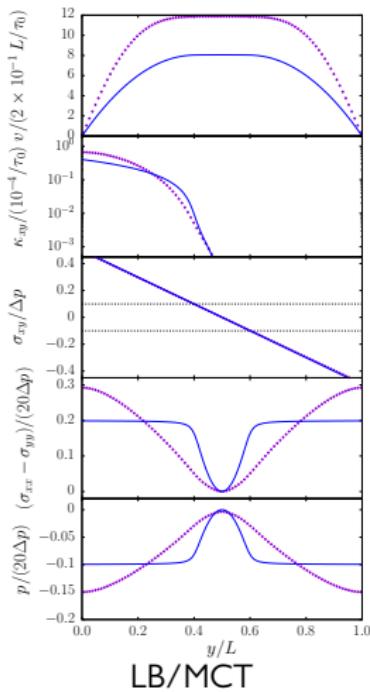
LB/MCT



BD, fluid

- glass: non-local rheology develops

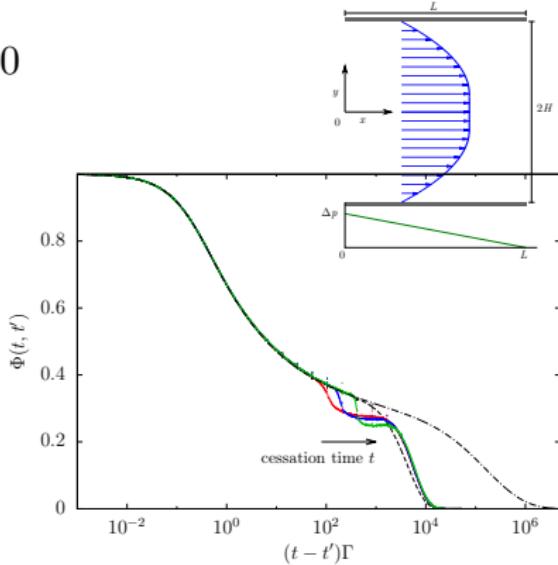
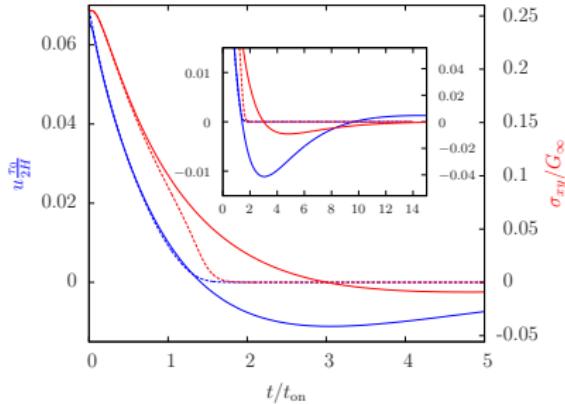
Theory and Brownian Dynamics (BD) Simulations



- glass: non-local rheology develops

Flow Cessation in a Channel

removal of pressure gradient at $t = 0$



- flow stops at *finite time*; stresses set fluid in motion again
 - competition of time scales:

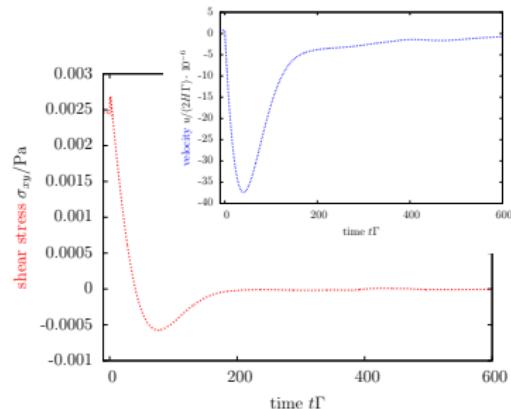
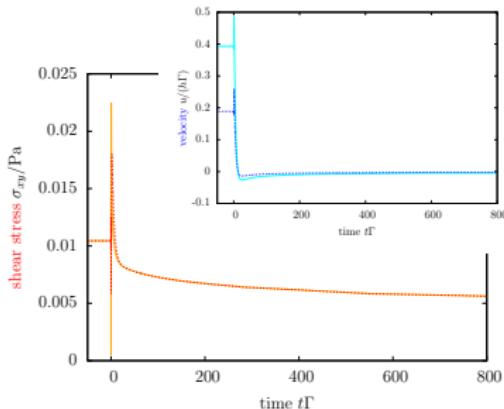
structural relaxation $\tau \propto \eta$

\Leftrightarrow fluid mechanics $\tau \propto \eta^{-1}$

microscopic

macroscopic

Residual Stresses: The Role of Geometry

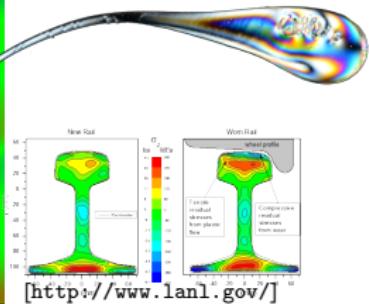
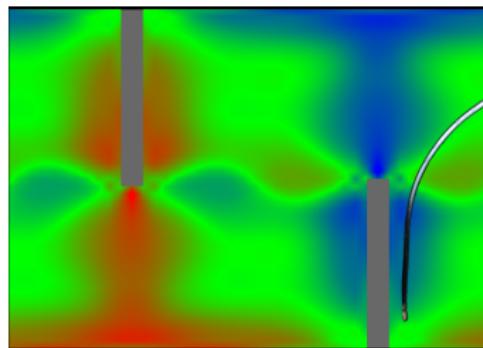
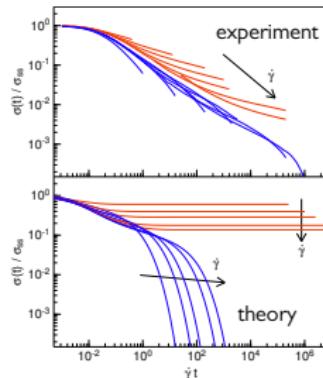


- channel geometry prevents residual stresses

$$0 = \vec{\nabla} \cdot \boldsymbol{\sigma}$$

- unless translational invariance is broken!

Processing Dependence of Materials: Residual Stresses



[<http://www.lanl.gov/>]

residual stresses: fingerprint of previous flow

$$\tau \rightarrow \infty$$

coupling of microscopic and
macroscopic time scales

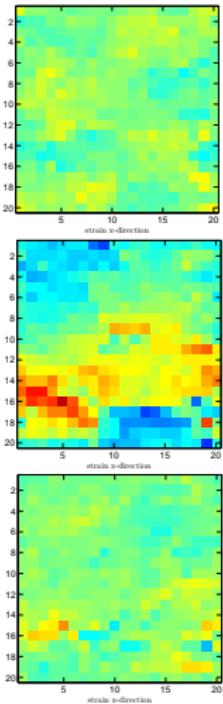
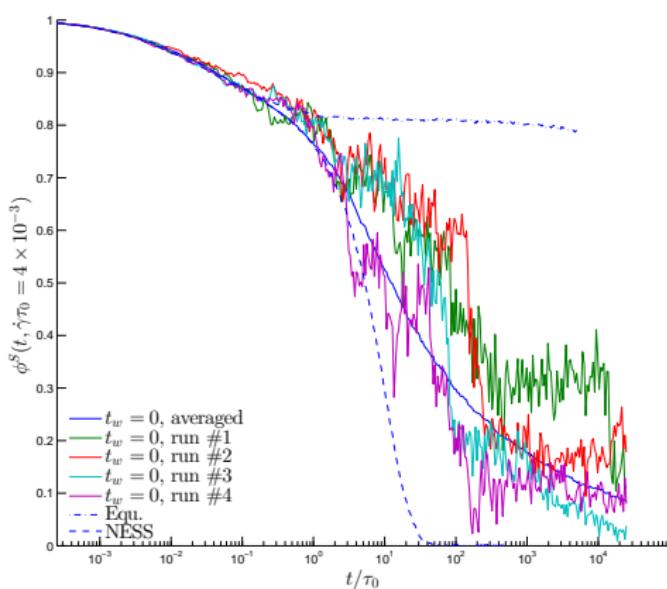
$$\vec{\nabla} \cdot \boldsymbol{\sigma} = 0$$

hydrodynamic boundaries change
microscopic dynamics

Continuum Description

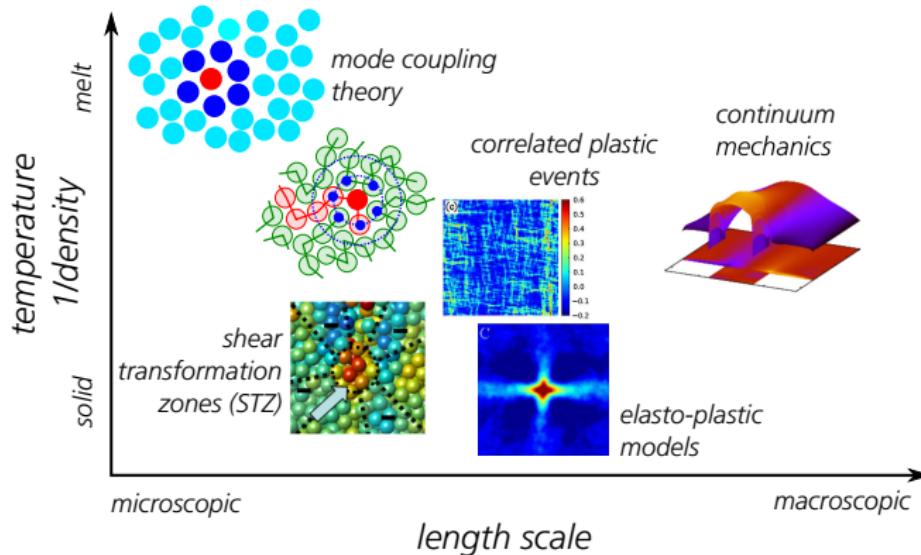
Empirical Models

Cessation Dynamics: Avalanches



- structural relaxation: *avalanches*
- sudden stress drops

Approaches to Glassy Rheology

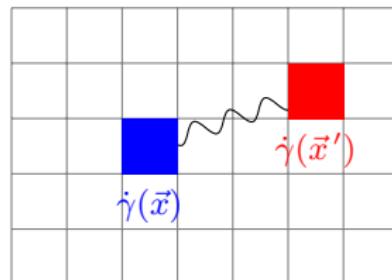


Spatial Cooperativity: Fluidity Model

$$\overset{\nabla}{\sigma}(t) + f(t)\sigma(t) = G_\infty \mathbf{D}(t)$$

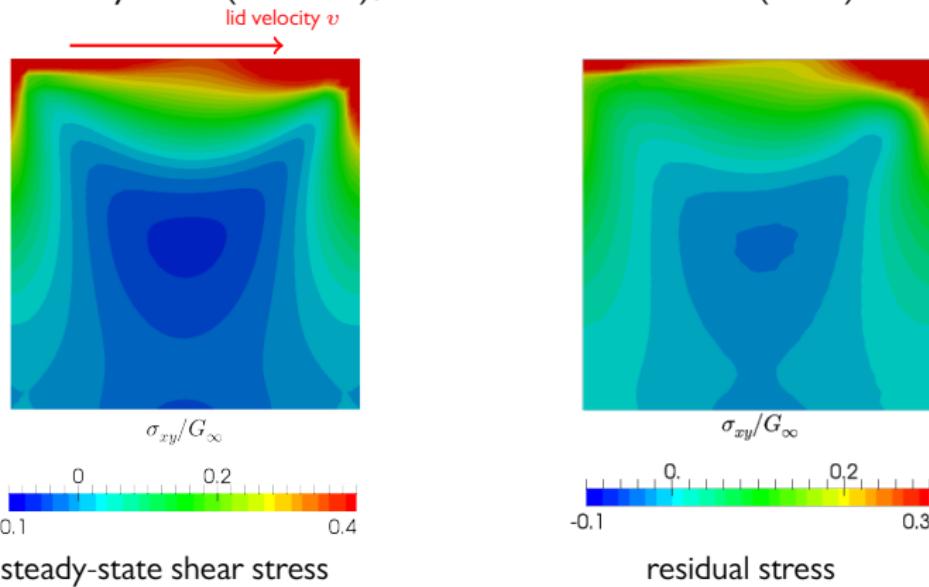
$$\tau_f \frac{D}{Dt} f(\vec{x}, t) + f(\vec{x}, t) = \left(\frac{1}{\tau} + \frac{\dot{\gamma}(\vec{x}, t)}{\gamma_c} \right) + \xi^2 \nabla^2 f(\vec{x}, t)$$

- drop integral equation – for computational ease
- ad-hoc spatial diffusion term – equivalent not yet in MCT
- ξ : spatial cooperativity length



Fluidity Model: Cessation

lid-driven cavity flow (low- Re), finite-volume method (FVM)



- fluidity diffusion breaks symmetry of low- Re residual stresses

Summary

Summary

- **history-dependent nonlinear response**

- material state *not uniquely fixed by thermodynamic control variables*

Siebenbürger, Ballauff, ThV, PRL **108**, 255701 (2012);
Ballauff et al., Phys. Rev. Lett. **110**, 215701 (2013)

- **statistical-physics foundations of material laws**

- *coupling between micro- & macroscopic time scales*
 - *multi-scale simulation* using microscopic theory

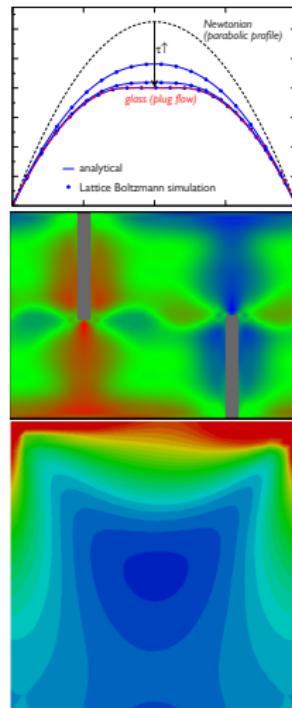
Papenkort and ThV, J. Chem. Phys. **143**, 204502 (2015)

Cárdenas et al., Eur. Phys. J. ST **226**, 3039 (2017)

- **effects of non-local rheology**

- empirical *glassy fluidity model*

Cárdenas and ThV, to be published (2018)



Thank you

H. Cárdenas, L. Elizondo, M. Gnann,
C. Harrer, R. Keßler, A. Liliuashvili,
J. Ónody, H.-L. Peng, S. Papenkort,
J. Reichert, M. Priya, Y.-C. Wang
A. Meyer, M. Fuchs, P. Born

