

# 準静的剪断下における摩擦のある アモルファス固体のヤコビアン行列による解析

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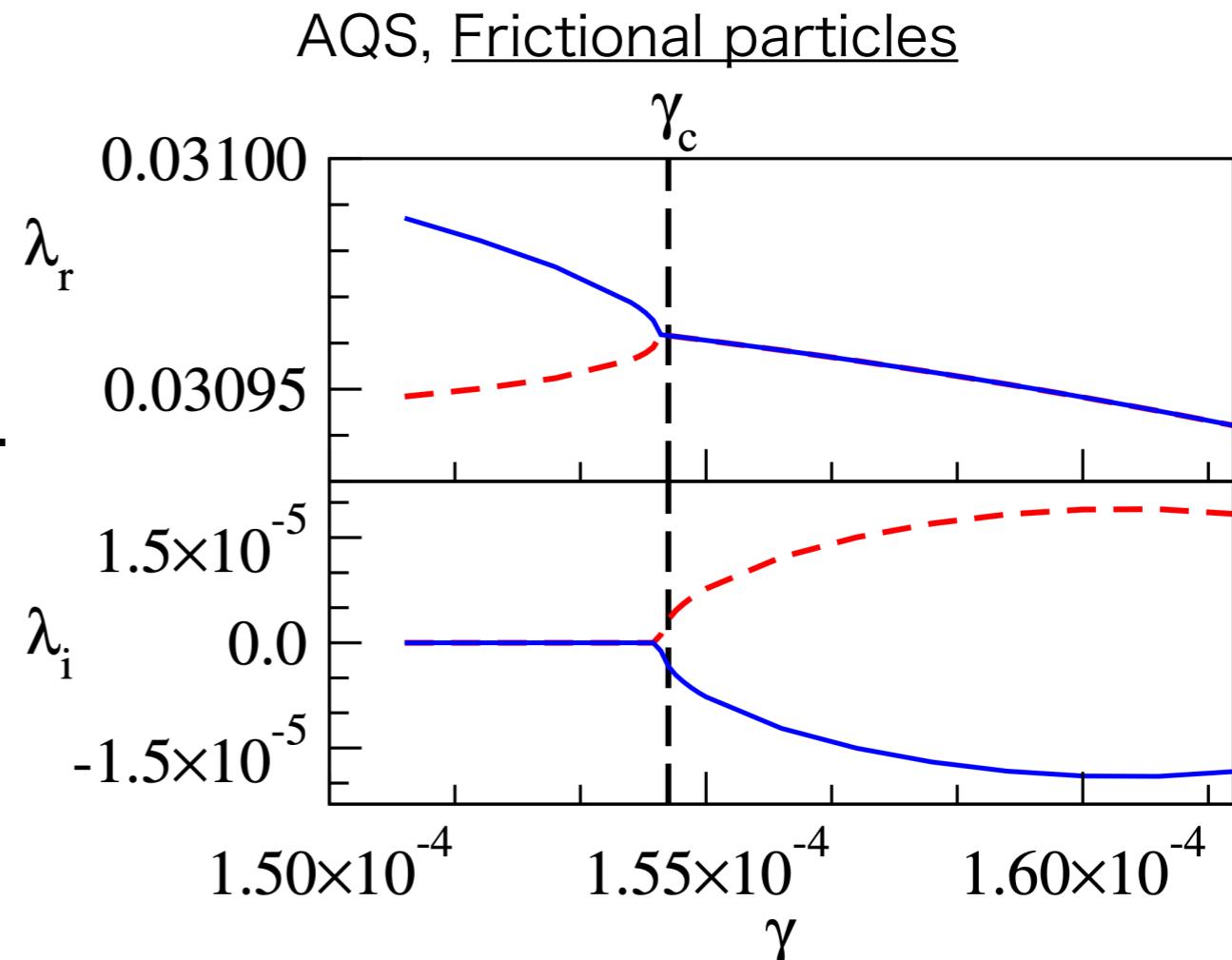
# Introduction

## Definition of Jacobian $J_{ij}^{\alpha\beta}$

$J_{ij}^{\alpha\beta} = -\frac{\partial \tilde{F}_i^\alpha}{\partial q_j^\beta}$ ,  $\tilde{F}_i^\alpha$ :  $\alpha$  component of generalized force acting on  $i$ -th particle  $\vec{\tilde{F}}_i = (F_i^x, F_i^y, T_i)^T$ ,  
 $q_i^\alpha$ :  $\alpha$  component of generalized  $i$ -th particle coordinate  $q_i := (r_i^x, r_i^y, \theta_i)$ ,  
 $T_i$ : Torque of  $i$  th particle,  
 $\theta_i$ : Rotational degree of  $i$  th particle.

Jacobian is an asymmetric matrix.

- >It has complex eigenvalue  $\lambda = \lambda_r + i\lambda_i$ .
- >Imaginary parts contribute to oscillatory instability\*.



\*J. Chattoraj et al., Phys. Rev. Lett. **123**, 098003 (2019).

# Introduction

	Frictionless materials	Frictional materials
Tool for stability analysis (dynamical matrix)	Hessian: $H_{ij}^{\alpha\beta} = \frac{\partial^2 U}{\partial q_j^\alpha \partial q_j^\beta}$	Jacobian: $J_{ij}^{\alpha\beta} = -\frac{\partial \tilde{F}_i^\alpha}{\partial q_j^\beta}$
Oscillatory instability	✗	○
Shear rigidity $G$ formula with dynamical matrix	○	?
$G$ can be obtained from $H_{ij}^{\alpha\beta}$ , Hessian's eigenvalues & Hessian's eigenvectors*.		

\*A. Lemaître & C. Maloney, J. Stat. Phys. 123, 2 (2006).

## Question?

Can we predict  $G$  by Jacobian?

## Purpose

To obtain the prediction of  $G$  in the limit  $\gamma \rightarrow 0$

# Our numerical protocol

## Preparation of initial configuration

1. Preparing the frictionless configuration at density  $\phi$  with energy minimization by FIRE\*
2. Incorporating the tangential forces
3. Relaxation by drag force  $-\eta \vec{v}_i$  until  $|F_i^\alpha| < F_{\text{Th}}$

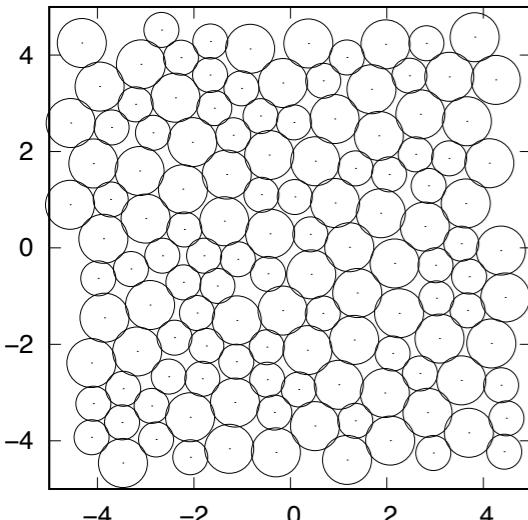
\*E. Bitzek et al., Phys. Rev. Lett., 97, 170201 (2006).



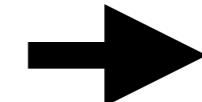
## Athermal quasistatic shear protocol

- I. Applying affine shear deformation  $\Delta\gamma$  to the system with Lees-Edwards periodic boundary condition
- II. Relaxation by drag force  $-\eta \vec{v}_i$  until  $|F_i^\alpha| < F_{\text{Th}}$

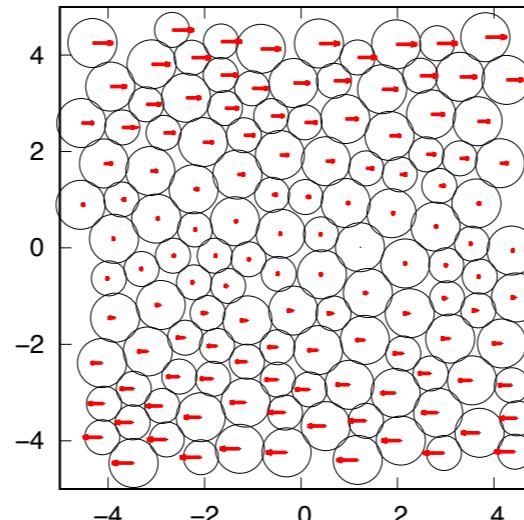
Initial configuration



Step strain  $\Delta\gamma$



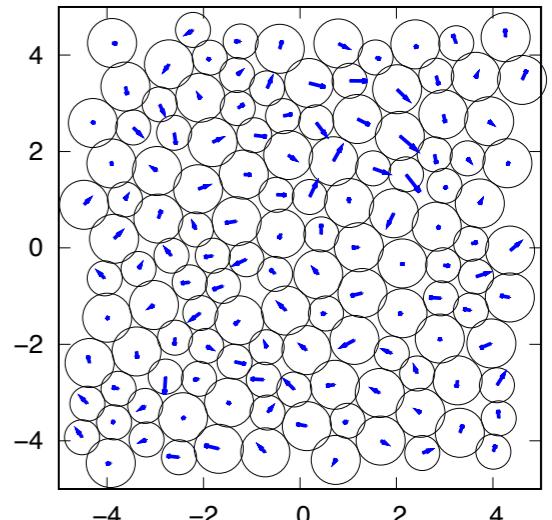
I. Affine deformation



Relaxation  
by  $-\eta \vec{v}_i$



II. Non affine displacement

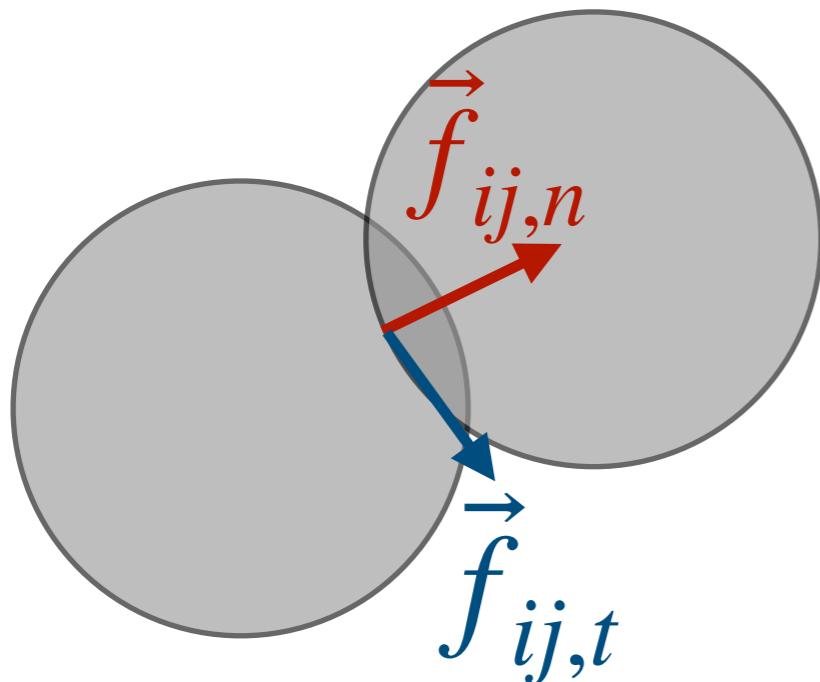


# Numerical methods

## Equation of motion

$$m_i \frac{d^2 \vec{x}_i}{dt^2} = \vec{F}_i^c - \eta \frac{d \vec{x}_i}{dt},$$

$$I_i \frac{d^2 \theta_i}{dt^2} = T_i^c - \eta \frac{d \theta_i}{dt}$$



$\vec{F}_i^c$  : Contact force of  $i$  particle

$T_i^c$  : Torque of  $i$  particle

$\theta_i$  : rotational degree of  $i$  particle

$$\vec{F}_i^c = \sum_j \left( \vec{f}_{ij,n} + \vec{f}_{ij,t} \right) \Theta(a_i + a_j - r_{ij}),$$

$$\vec{f}_{ij,n} = k_n \xi_{ij,n}^{3/2} \vec{n}_{ij},$$

$$\vec{f}_{ij,t} = -k_t \xi_{ij,n}^{1/2} \vec{\xi}_{ij,t}$$

\*nonslip model

Our simulated system

2 dimensional binary disks ( $N = 128$ ),

Step strain:  $\Delta\gamma = 10^{-10}$ ,

Threshold value of mechanical equilibrium condition:  $F_{\text{Th}}/(k_n d_0) = 10^{-14}$ ,

Density  $0.80 \leq \phi \leq 0.90$ ,

Tangential ratio  $0.0 \leq k_t/k_n \leq 10.0$ .

# Expression of $G$ by $J$

We obtain shear modulus  $G$  by  $J$ :

$$G(0) = \frac{1}{2L^2} \sum_{i,j(i \neq j)} \left[ \underbrace{y_{ij}^2(0) J_{N,ij}^{xx}(0)}_{\text{Affine shear modulus}} + \underbrace{\sum_{\kappa=x,y} y_{ij}(0) J_{ij}^{\kappa x}(0) \frac{du_{ij}^{\kappa}(0)}{d\gamma} + y_{ij}(0) J_{ij}^{\ell x}(0) \left( \frac{du_i^{\ell}(0)}{d\gamma} + \frac{du_j^{\ell}(0)}{d\gamma} \right)}_{\text{Non affine shear modulus}} \right] \dots \quad (1)$$

Affine shear modulus Non affine shear modulus

with  $J_{ij}^{\alpha\beta} = -\frac{\partial f_{ij}^{\beta}}{\partial q_i^{\alpha}}$ ,  $J_{N,ij}^{\alpha\beta} = -\frac{\partial f_{N,ij}^{\beta}}{\partial q_i^{\alpha}}$ ,  $u_{ij}^{\alpha} := u_i^{\alpha} - u_j^{\alpha}$ ,  $u_i^{\alpha}(0) = q_i^{\alpha}(\Delta\gamma) - q_i^{\alpha}(0) - \Delta\gamma\delta_{\alpha x}$ : non affine displacement.

## Calculation methods of $G$

### Cauchy's expression

$$G = \frac{d\sigma_{xy}}{d\gamma}, \quad \sigma_{xy} = -\frac{1}{L^2} \sum_i \sum_{j>i} f_{ij}^x y_{ij},$$

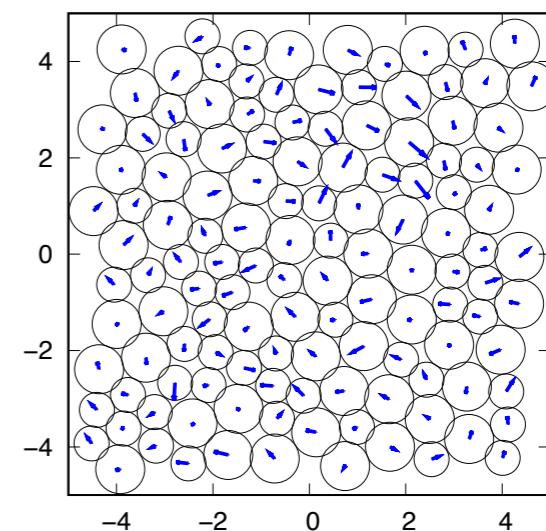
$f_{ij}^x$  :  $x$  component of forces from  $j$  to  $i$  particle,

$y_{ij}$  :  $y$  component of displacements from  $j$  to  $i$  particle.

It needs  $f_{ij}^x(0)$ ,  $y_{ij}(0)$ ,  $f_{ij}^x(\Delta\gamma)$ ,  $y_{ij}(\Delta\gamma)$ .

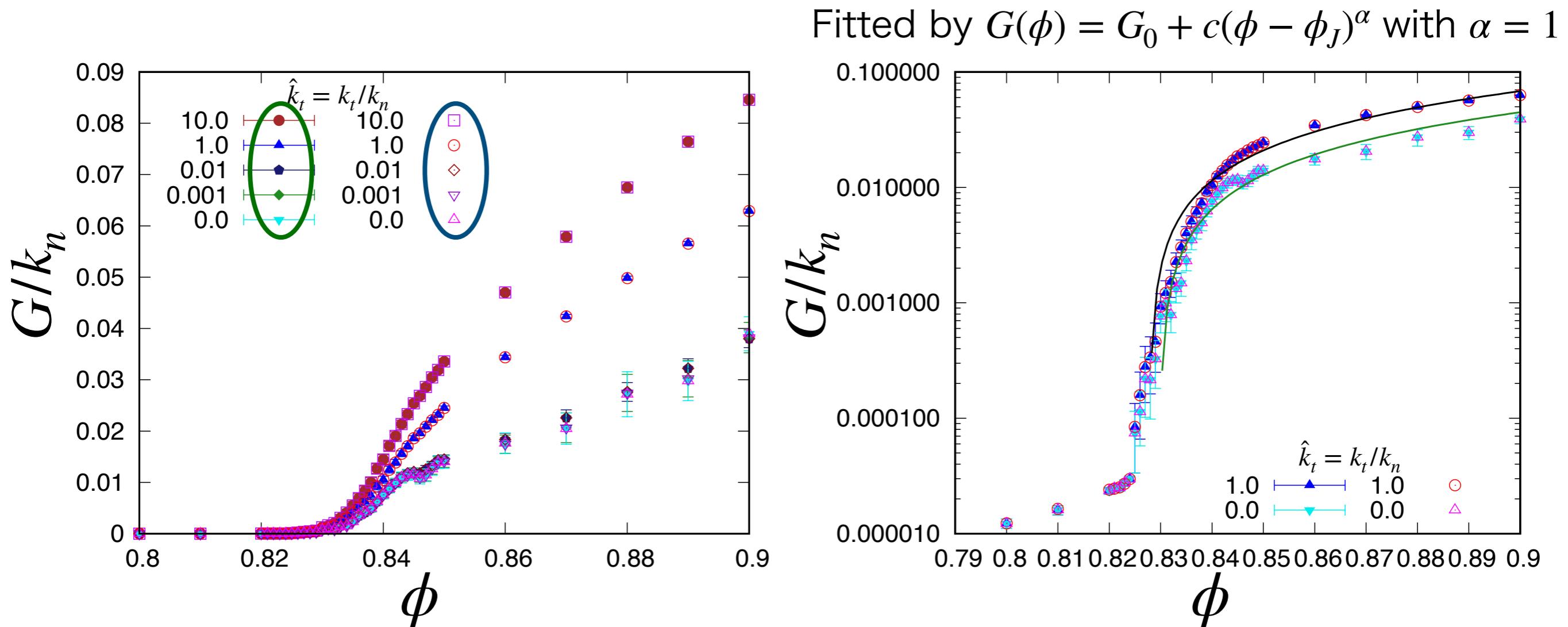
### Jacobian's expression

Eq. (1) needs  $J_{ij}^{\alpha\beta}(0)$ ,  $y_{ij}(0)$ ,  $u_i^{\alpha}(0)$



Non affine displacement:  $u_i^{\alpha}(0)$

# $\phi$ -dependence

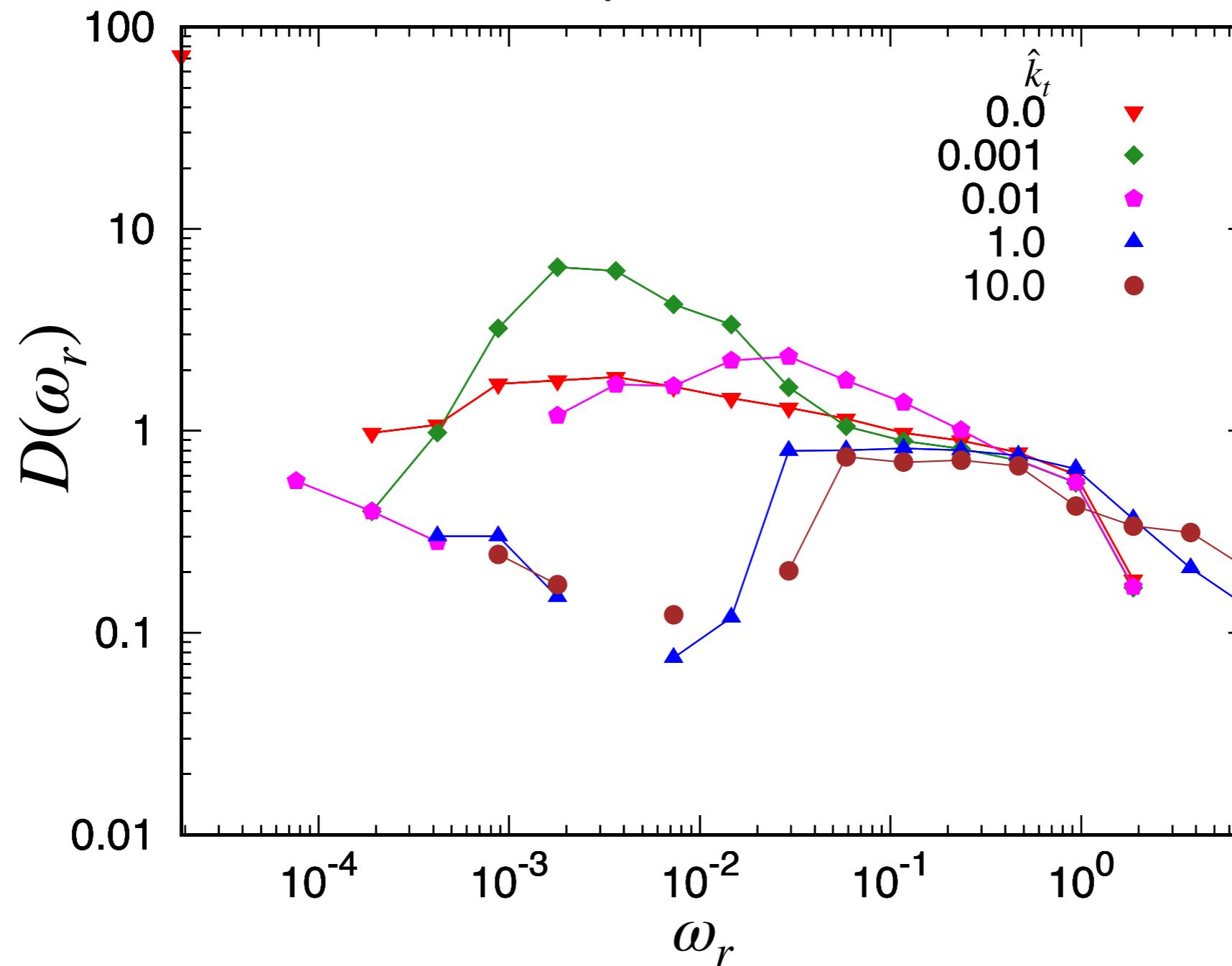


Jacobian's expression reproduces  $\phi$  dependence.  
 $G(\phi)$  has a linear dependence of  $\phi - \phi_J^*$ .

\*C. S. O'Hern et al., Phys. Rev. Lett., 88, 7 (2002),  
E. Somfai et al., Phys. Rev. E, 75, 020301(R) (2007).

# Density of State

$$\phi = 0.87$$



An isolated band at low frequency\* appears for  $\hat{k}_t \geq 0.01$ .

\*C. F. Schreck et al., Phys. Rev. E, 85, 061305 (2012).

# Summary

Frictional amorphous solids under quasi-static shear are analyzed using the Jacobian.

## Shear modulus $G$ in the limit $\gamma \rightarrow 0$

- Jacobain's representation can reproduce  $G$ .

## Density of state $D(\omega_r)$ in the limit $\gamma \rightarrow 0$

- An isolated band at low frequency appears for  $\hat{k}_t \geq 0.01$ .

## Future work

- Expanding non affine displacements  $u_i^\alpha(0)$  by eigenfunctions of Jacobian

