

Jacobian analysis for frictional amorphous solids under quasi- static shear

Daisuke Ishima¹, Kuniyasu Saitoh²,
Michio Otsuki³, Hisao Hayakawa¹
¹YITP, ²Kyoto Sangyo Univ., ³Osaka Univ.

Introduction Amorphous solids

Amorphous materials



Forms



Sands



Bubbles

Solid-like

Frictionless amorphous solids

Frictional amorphous solids

Previous researches for frictionless solids

Definition of Hessian $H_{ij}^{\alpha\beta}$

$$H_{ij}^{\alpha\beta} = \frac{\partial^2 U}{\partial r_i^\alpha \partial r_j^\beta} = - \frac{\partial F_i^\alpha}{\partial r_j^\beta},$$

U : Potential energy,

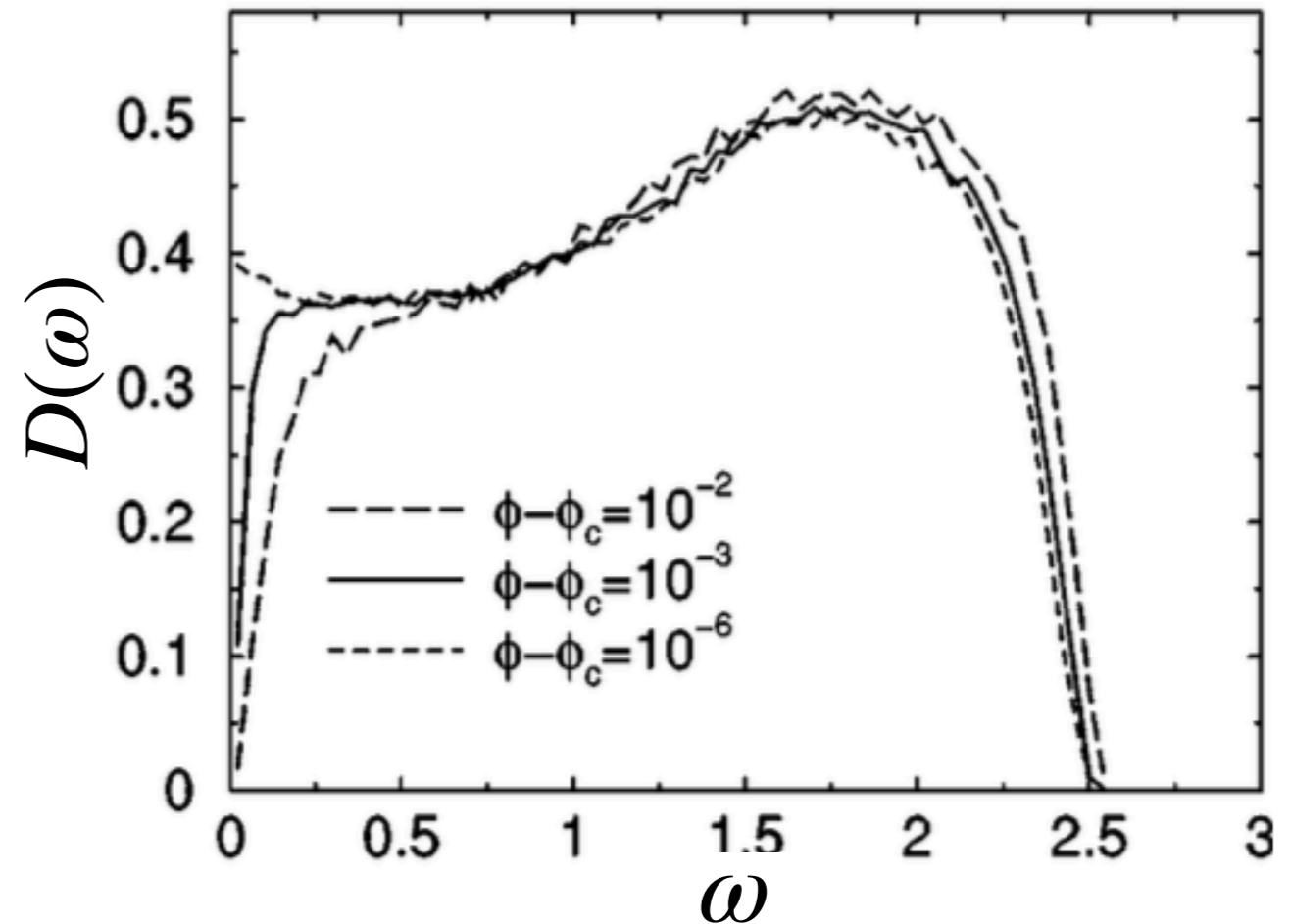
F_i^α : α component of force acting on i -th particle,

r_i^α : α component of i -th particle coordinate.

We obtain DOS from eigenvalues of H .

*Note that zero eigenmodes are related floppy mode or transnational mode.

$D(\omega)$: Density of state (DOS)



C. S. O'Hern et al., Phys. Rev. E **68**, 011306 (2003).

Previous researches for frictional solids

Definition of **Jacobian** $J_{ij}^{\alpha\beta}$

$$J_{ij}^{\alpha\beta} = - \frac{\partial \tilde{F}_i^\alpha}{\partial q_j^\beta},$$

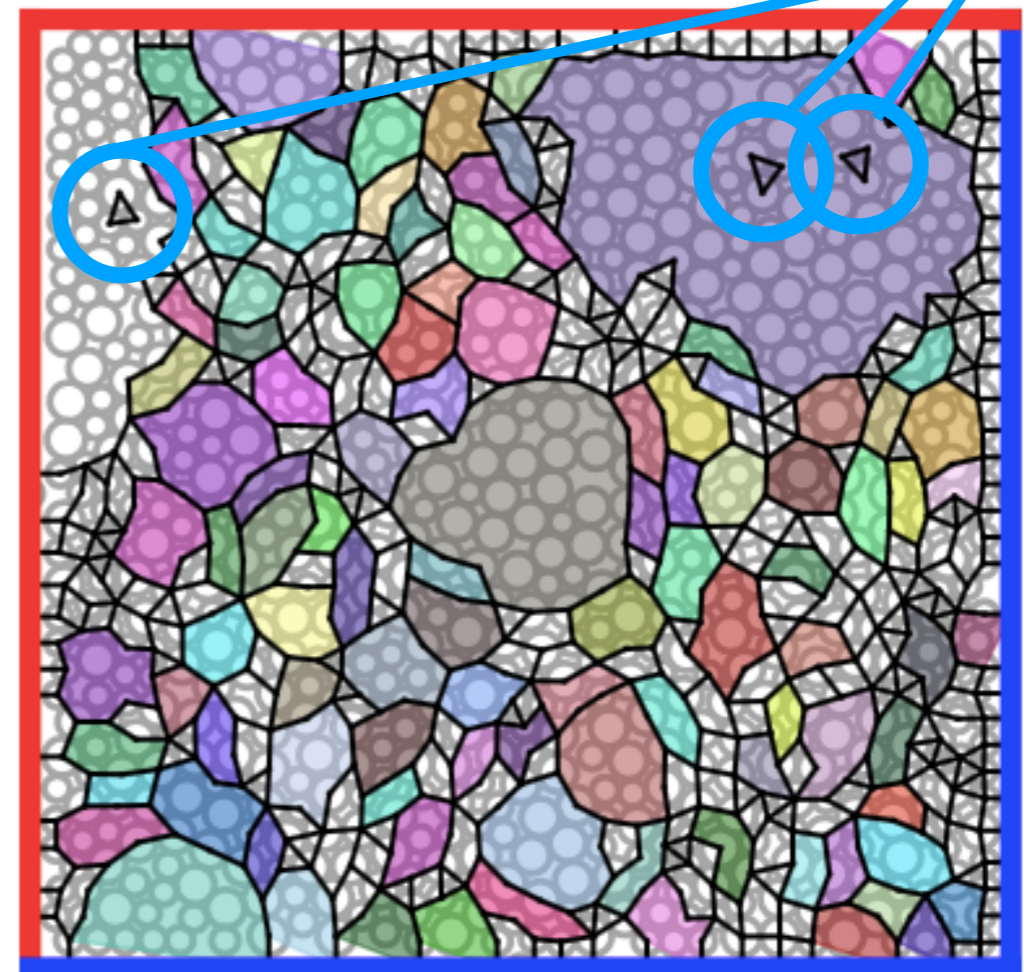
\tilde{F}_i^α : α component of generalized force acting on i -th particle $\vec{\tilde{F}}_i = (F_i^x, F_i^y, T_i)^T$,

q_i^α : α component of generalized i -th particle coordinate $q_i := (r_i^x, r_i^y, \theta_i)$,

T_i : Torque of i th particle,

θ_i : Rotational degree of i th particle.

Colored rigid clusters & floppy holes



They identify the floppy hole* from
Jacobian's zero eigenvalue

*Floppy hole: NOT contribute rigidity

K. Liu et al., Phys. Rev. Lett. 126, 088002 (2021).

Previous researches for frictional solids

Definition of **Jacobian** $J_{ij}^{\alpha\beta}$

$$J_{ij}^{\alpha\beta} = - \frac{\partial \tilde{F}_i^\alpha}{\partial q_j^\beta}, \quad \tilde{F}_i^\alpha : \alpha \text{ component of generalized force acting on } i\text{-th particle } \vec{\tilde{F}}_i = (F_i^x, F_i^y, T_i)^T,$$

$$q_i^\alpha : \alpha \text{ component of generalized } i\text{-th particle coordinate } q_i := (r_i^x, r_i^y, \theta_i),$$

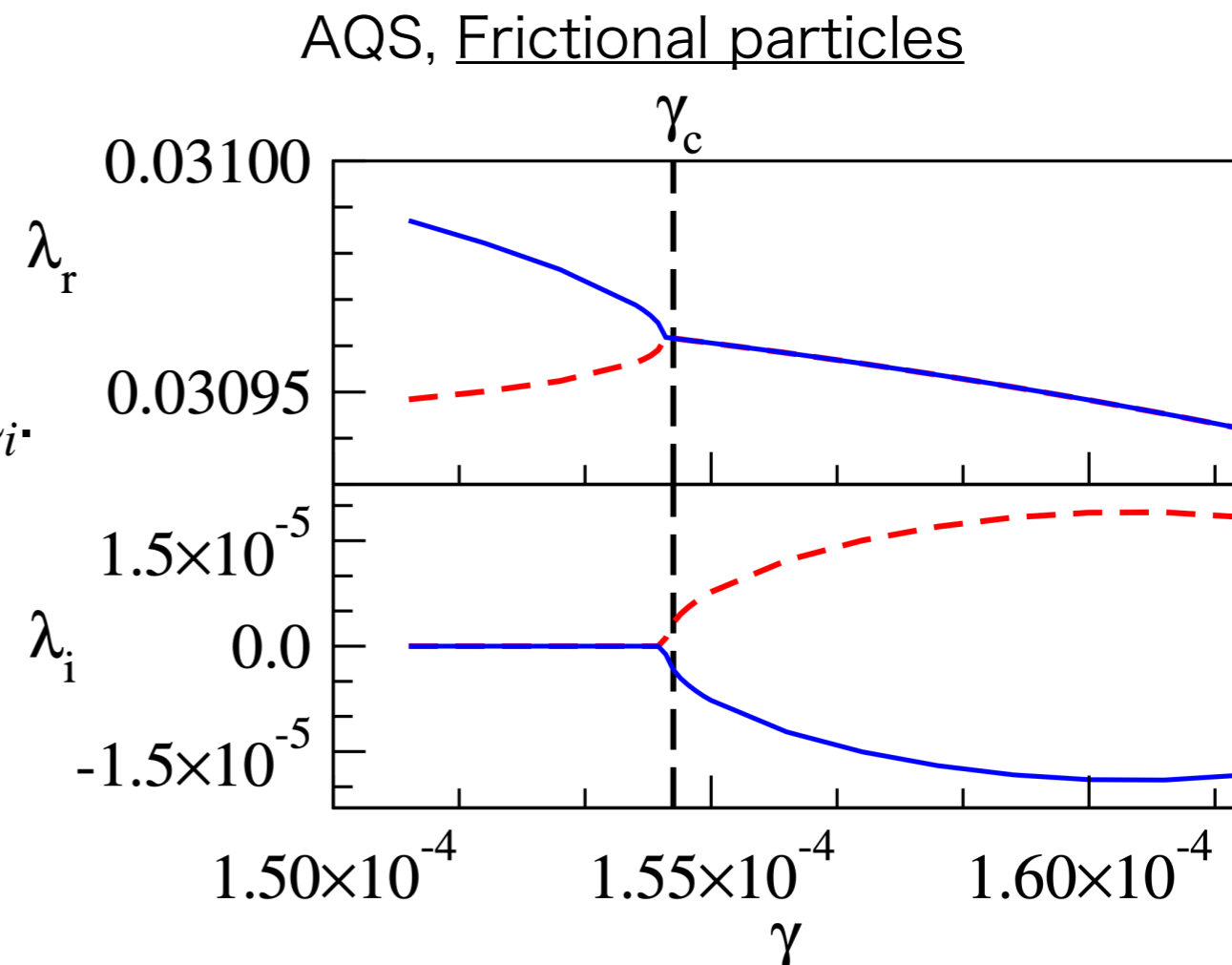
T_i : Torque of i th particle,

θ_i : Rotational degree of i th particle.

Jacobian is an asymmetric matrix.

->It has complex eigenvalue $\lambda = \lambda_r + i\lambda_i$.

->Imaginary parts contribute to oscillatory instability*.



*J. Chatteraj et al., *Phys. Rev. Lett.* **123**, 098003 (2019).

Introduction

	Frictionless materials	Frictional materials
Tool for stability analysis (dynamical matrix)	Hessian: $H_{ij}^{\alpha\beta} = \frac{\partial^2 U}{\partial r_i^\alpha \partial r_j^\beta}$	Jacobian: $J_{ij}^{\alpha\beta} = -\frac{\partial \tilde{F}_i^\alpha}{\partial q_j^\beta}$
To determine floppy mode	○	○
Oscillatory instability	×	○
Shear rigidity G formula with dynamical matrix	○	○ ?

G can be obtained from $H_{ij}^{\alpha\beta}$, Hessian's eigenvalues & Hessian's eigenvectors*.

*A. Lemaître & C. Maloney, *J. Stat. Phys.* **123**, 2 (2006).

Question?

Can we predict G by Jacobian?

Purpose

To obtain the prediction of G in the limit $\gamma \rightarrow 0$

Our numerical protocol

Preparation of initial configuration

1. Preparing the frictionless configuration at density ϕ with energy minimization by FIRE*
2. Incorporating the tangential forces
3. Relaxation by dissipation until $|F_i^\alpha| < F_{\text{Th}}$

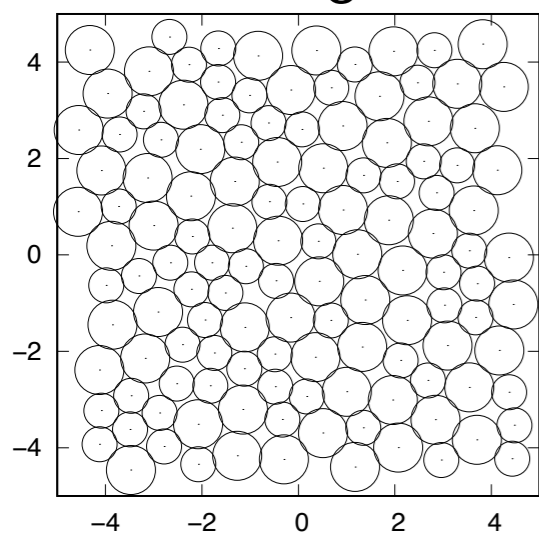
*E. Bitzek et al., *Phys. Rev. Lett.*, 97, 170201 (2006).



Athermal quasistatic shear protocol

- I. Applying affine shear deformation $\Delta\gamma$ to the system with Lees-Edwards periodic boundary condition
- II. Relaxation by dissipation until $|F_i^\alpha| < F_{\text{Th}}$

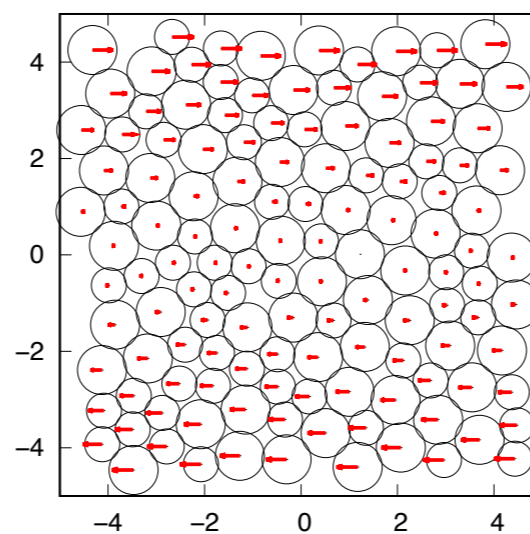
Initial configuration



Step strain $\Delta\gamma$



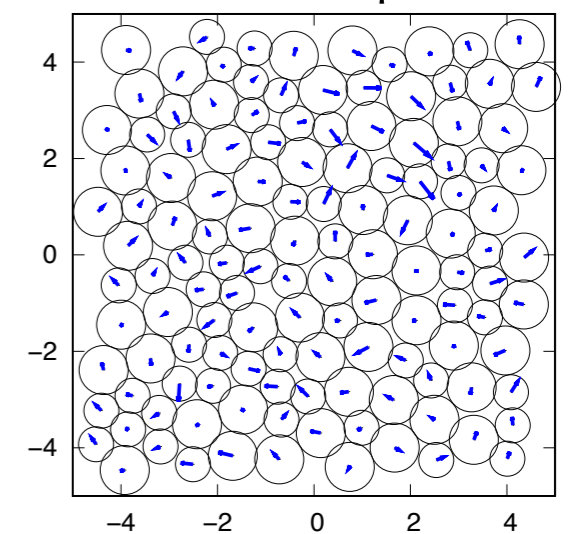
I. Affine deformation



Relaxation



II. Non affine displacement



Numerical methods

Equation of motion

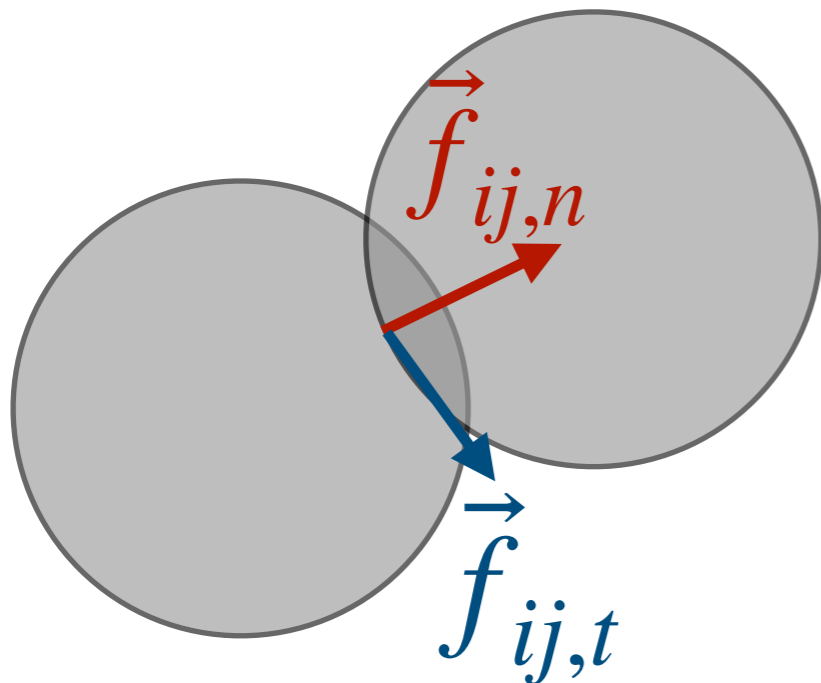
$$m_i \frac{d^2 \vec{x}_i}{dt^2} = \vec{F}_i$$

$$I_i \frac{d^2 \theta_i}{dt^2} = T_i$$

\vec{F}_i : Force of i particle

T_i : Torque of i particle

θ_i : rotational degree of i particle



$$\vec{F}_i = \sum_j \left(\vec{f}_{N,ij} + \vec{f}_{T,ij} \right) \Theta(a_i + a_j - r_{ij}),$$

$$\vec{f}_{N,ij} = k_N \xi_{N,ij}^{3/2} \vec{n}_{ij} - \eta_N \vec{v}_{N,ij},$$

$$\vec{f}_{T,ij} = -k_T \xi_{N,ij}^{1/2} \vec{\xi}_{T,ij} - \eta_T \vec{v}_{T,ij}$$

*nonslip model

Our simulated system

2 dimensional binary disks ($N = 128$),

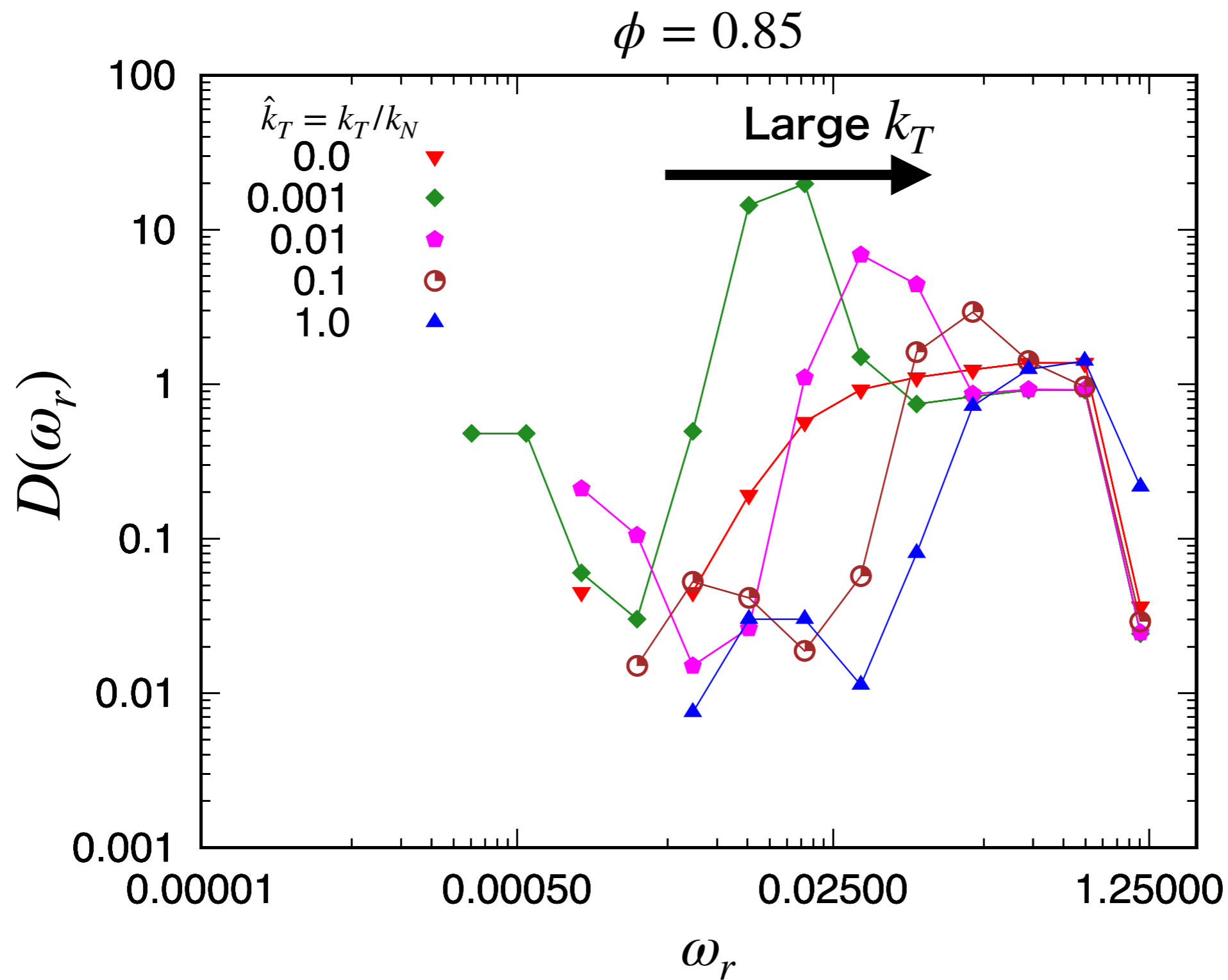
Step strain: $\Delta\gamma = 10^{-10}$,

Threshold value of mechanical equilibrium condition: $F_{Th}/(k_N d_0) = 10^{-14}$,

Density $0.80 \leq \phi \leq 0.90$,

Tangential ratio $0.0 \leq k_T/k_N \leq 10.0$.

Density of State



As k_T increases, low frequency part moves high frequency region*

*C. F. Schreck et al., *Phys. Rev. E*, **85**, 061305 (2012).

Expression of G by J

We obtain shear modulus G by J :

$$G(0) = \frac{1}{2L^2} \sum_{i,j(i \neq j)} \left[\underbrace{y_{ij}^2(0) J_{N,ij}^{xx}(0)}_{\text{Affine shear modulus}} + \sum_{\kappa=x,y} \underbrace{y_{ij}(0) J_{ij}^{\kappa x}(0)}_{\text{Non affine shear modulus}} \frac{du_{ij}^{\kappa}(0)}{d\gamma} + y_{ij}(0) J_{ij}^{\ell x}(0) \left(\frac{du_i^{\ell}(0)}{d\gamma} + \frac{du_j^{\ell}(0)}{d\gamma} \right) \right] \dots \quad (1)$$

Affine shear modulus **Non affine shear modulus**

with $J_{ij}^{\alpha\beta} = -\frac{\partial f_{ij}^{\beta}}{\partial q_i^{\alpha}}$, $J_{N,ij}^{\alpha\beta} = -\frac{\partial f_{N,ij}^{\beta}}{\partial q_i^{\alpha}}$, $u_{ij}^{\alpha} := u_i^{\alpha} - u_j^{\alpha}$, $u_i^{\alpha}(0) = q_i^{\alpha}(\Delta\gamma) - q_i^{\alpha}(0) - \Delta\gamma\delta_{\alpha x}$: non affine displacement.

Calculation methods of G

Cauchy's expression

$$G = \frac{d\sigma_{xy}}{d\gamma}, \quad \sigma_{xy} = -\frac{1}{L^2} \sum_i \sum_{j>i} f_{ij}^x y_{ij}$$

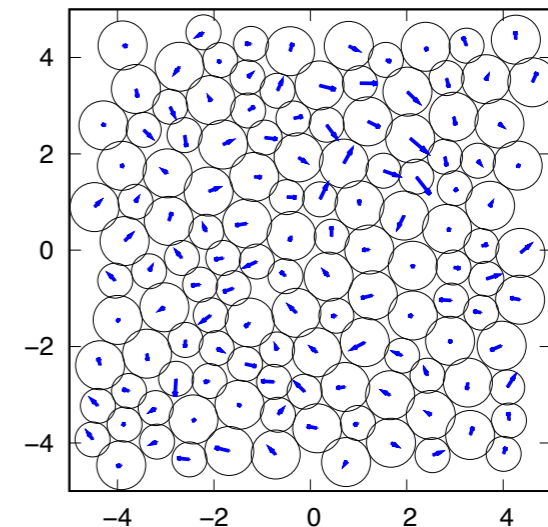
f_{ij}^x : x component of forces from j to i particle,

y_{ij} : y component of displacements from j to i particle.

It needs $f_{ij}^x(0)$, $y_{ij}(0)$, $f_{ij}^x(\Delta\gamma)$, $y_{ij}(\Delta\gamma)$.

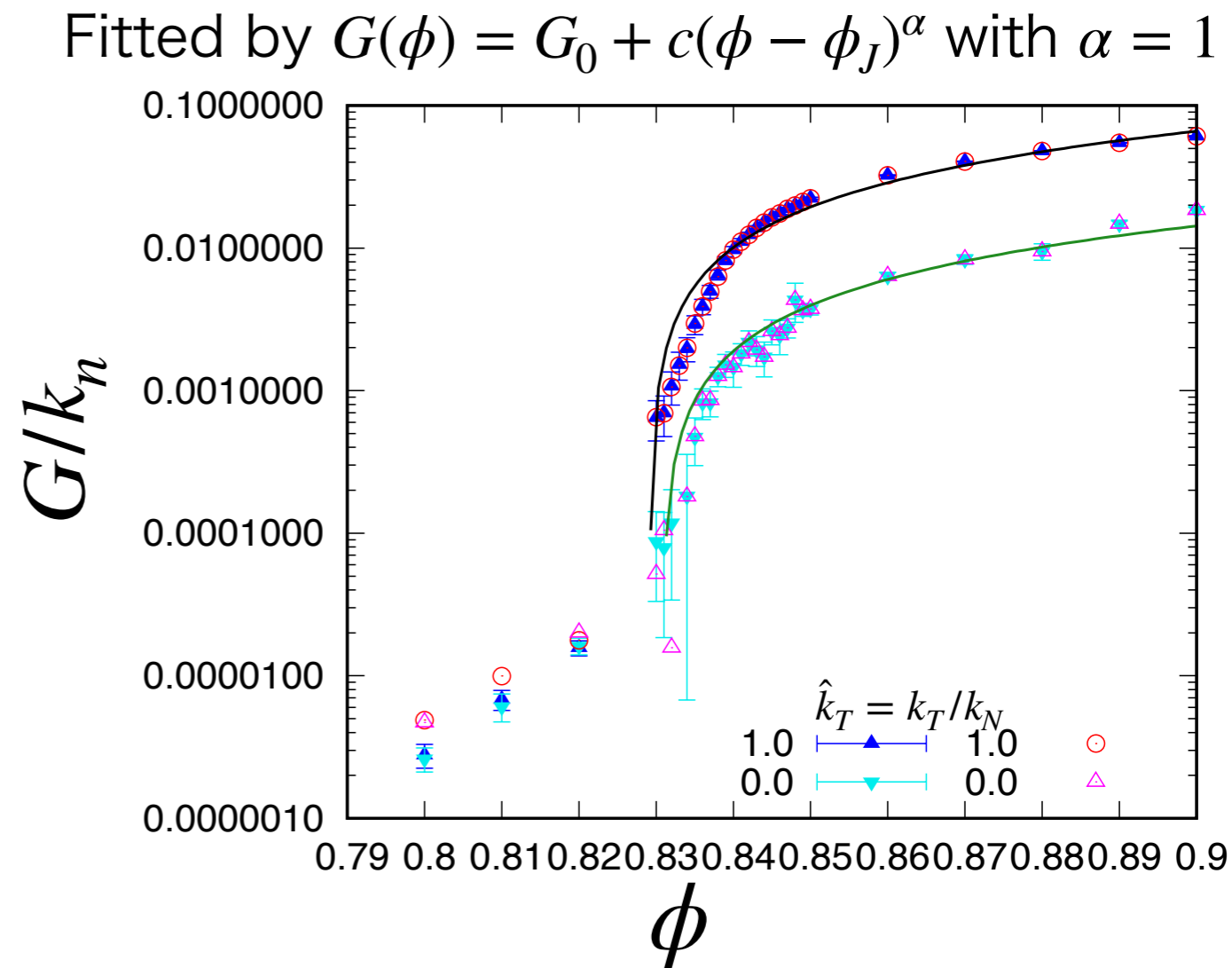
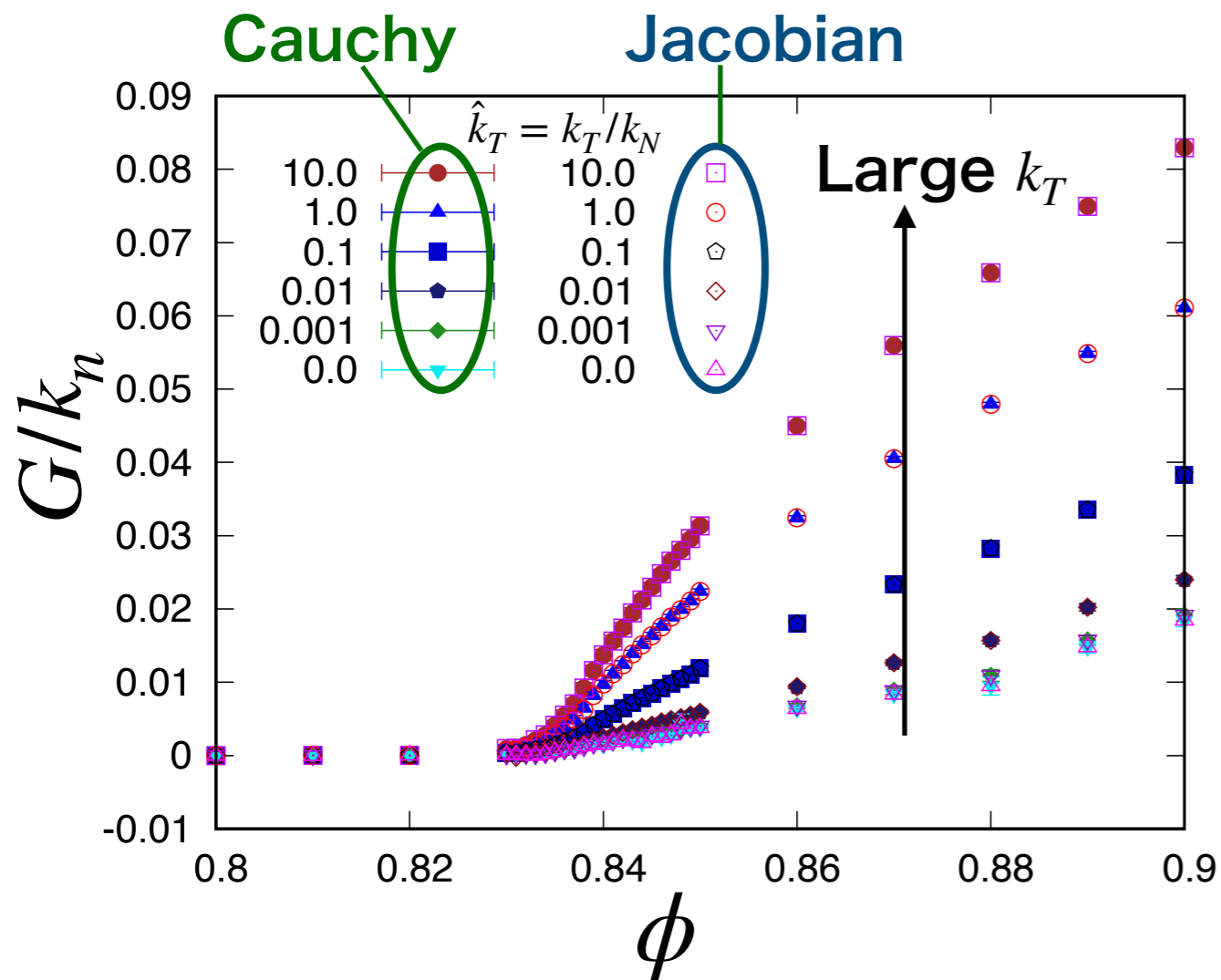
Jacobian's expression

Eq. (1) needs $J_{ij}^{\alpha\beta}(0)$, $y_{ij}(0)$, $u_i^{\alpha}(0)$



Non affine displacement: $u_i^{\alpha}(0)$

ϕ -dependence



Jacobian's expression reproduces ϕ dependence.

$G(\phi)$ has a linear dependence of $\phi - \phi_J^*$.

*C. S. O'Hern et al., *Phys. Rev. Lett.*, **88**, 7 (2002),
E. Somfai et al., *Phys. Rev. E*, **75**, 020301(R) (2007).

Eigenfunction expansion for $k_T = 0$

We obtain shear modulus G by H :

$$G(0) = \frac{1}{2L^2} \sum_{i,j(i \neq j)} \left[y_{ij}^2(0) H_{ij}^{xx}(0) + \sum_{\kappa=x,y} y_{ij}(0) H_{ij}^{\kappa x}(0) \frac{du_{ij}^{\kappa}(0)}{d\gamma} \right] \dots \quad (2)$$

with Hessian: $H_{ij}^{\alpha\beta} = -\frac{\partial f_{N,ij}^{\beta}}{\partial q_i^{\alpha}} = \frac{\partial^2 U_N}{\partial q_i^{\alpha} \partial q_j^{\beta}}$ ($\alpha, \beta = x, y$).

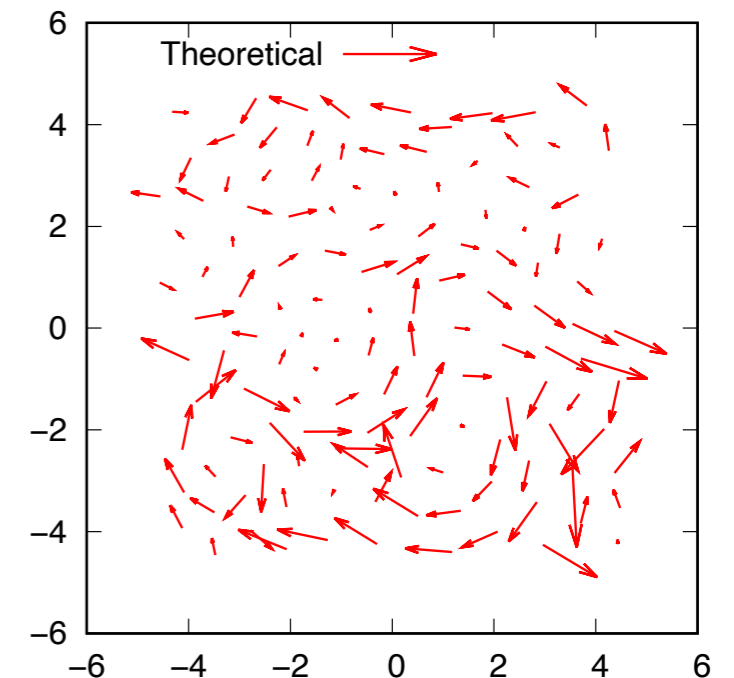
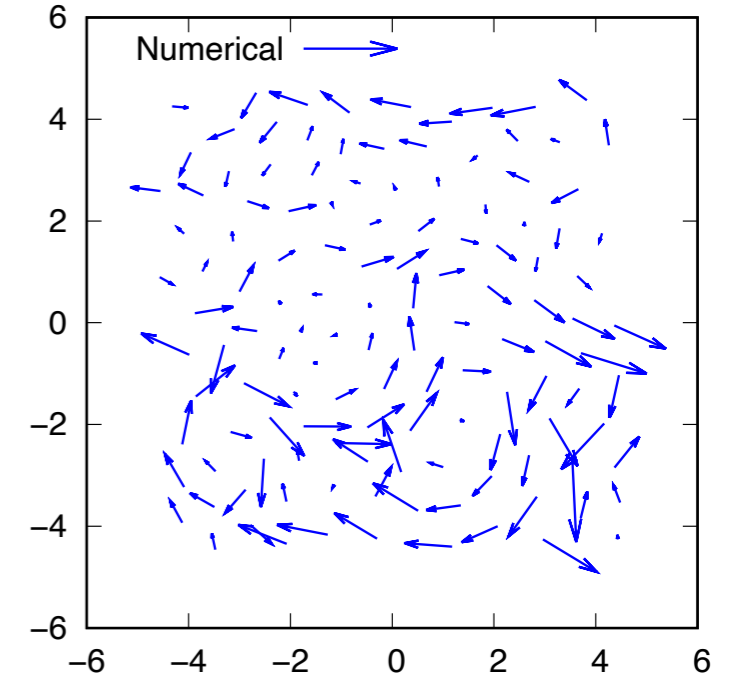
Eigenfunction expansion of $|du/d\gamma\rangle$ by H^* :

$$\left| \frac{du}{d\gamma} \right\rangle = \sum_n \frac{\langle n | \Xi \rangle}{\lambda_n} |n\rangle \quad \dots \quad (3)$$

*A. Lemaître & C. Maloney, *J. Stat. Phys.* **123**, 2 (2006).

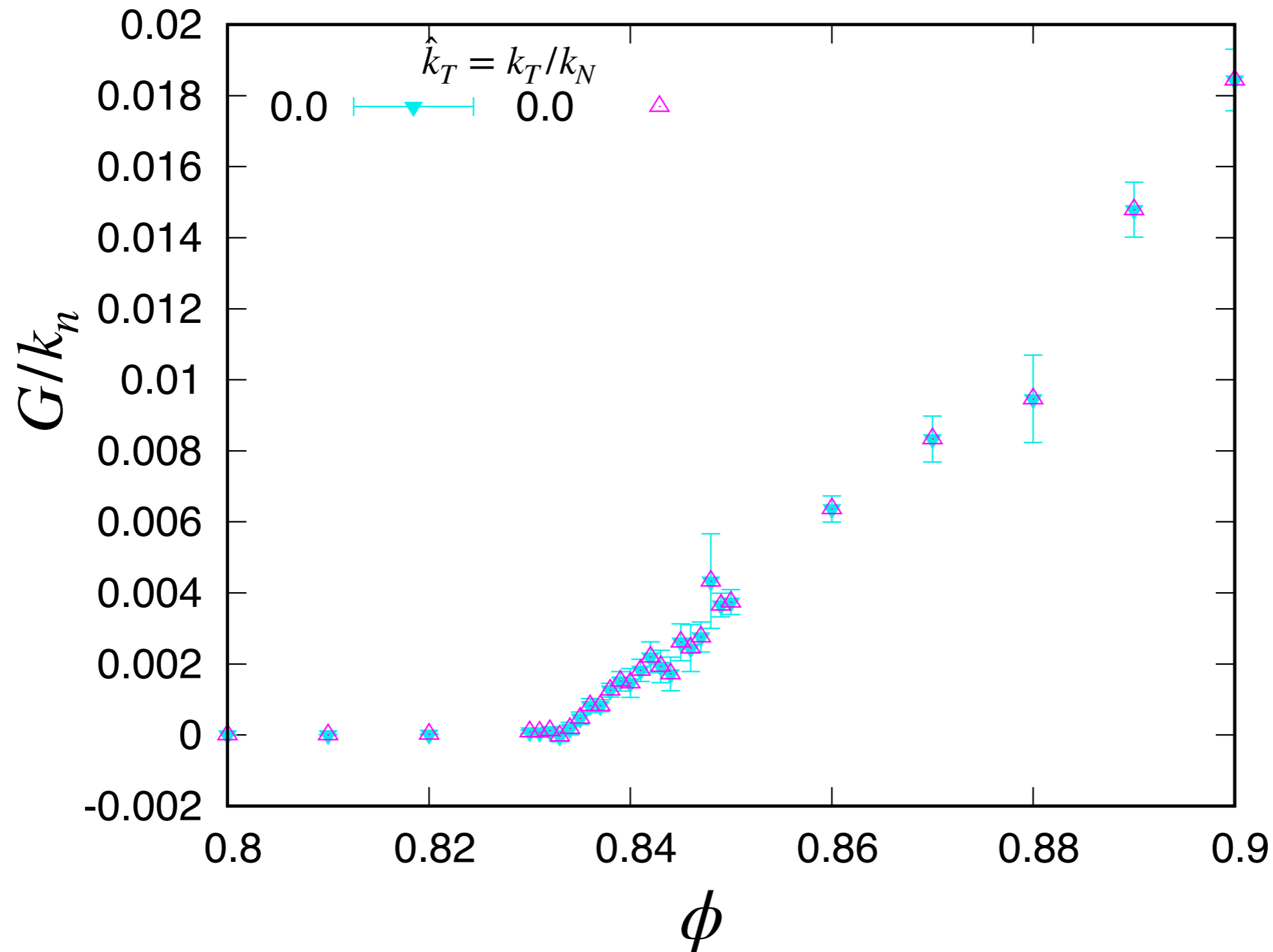
where $\lambda_n, |n\rangle$: n -th eigenvalue & vector, $|\Xi\rangle = \begin{bmatrix} \sum_{j \neq 1} H_{1j}^{xx} \\ \sum_{j \neq 1} H_{1j}^{xy} \\ \vdots \\ \sum_{j \neq N} H_{Nj}^{xx} \\ \sum_{j \neq N} H_{Nj}^{xy} \end{bmatrix}$

Non affine displacement $k_t = 0$



We can predict G from initial information by using Eqs. (2) & (3).

ϕ -dependence for $k_T = 0$ (frictionless)



We can predict $G(\phi)$ from initial information.

Eigenfunction expansion for small k_T

We ignore the tangential part of J for small k_T :

$$\begin{aligned} J &= J_N + J_T \\ &\simeq J_N \quad (k_T \ll k_N) \\ &= H, \end{aligned}$$

$$\text{where } J_N := -\frac{\partial f_N}{\partial q}, J_T := -\frac{\partial f_T}{\partial q}.$$

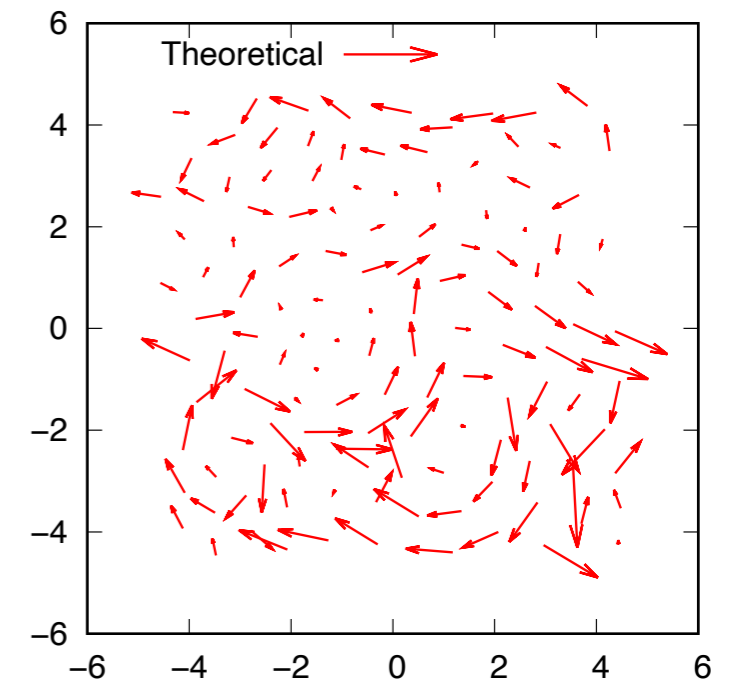
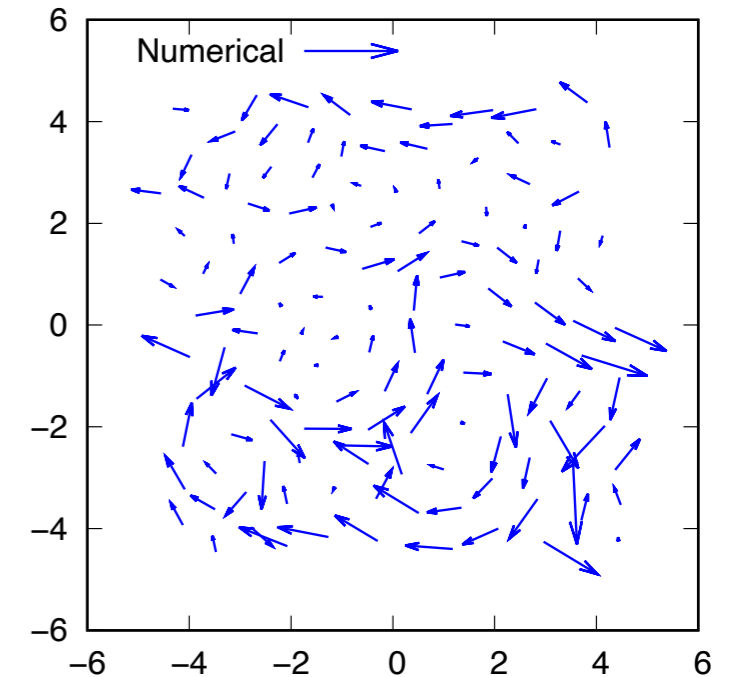
We use Hessian's formula

$$G(0) = \frac{1}{2L^2} \sum_{i,j(i \neq j)} \left[y_{ij}^2(0) H_{ij}^{xx}(0) + \sum_{\kappa=x,y} y_{ij}(0) H_{ij}^{\kappa x}(0) \frac{du_{ij}^{\kappa}(0)}{d\gamma} \right] \dots \quad (2)$$

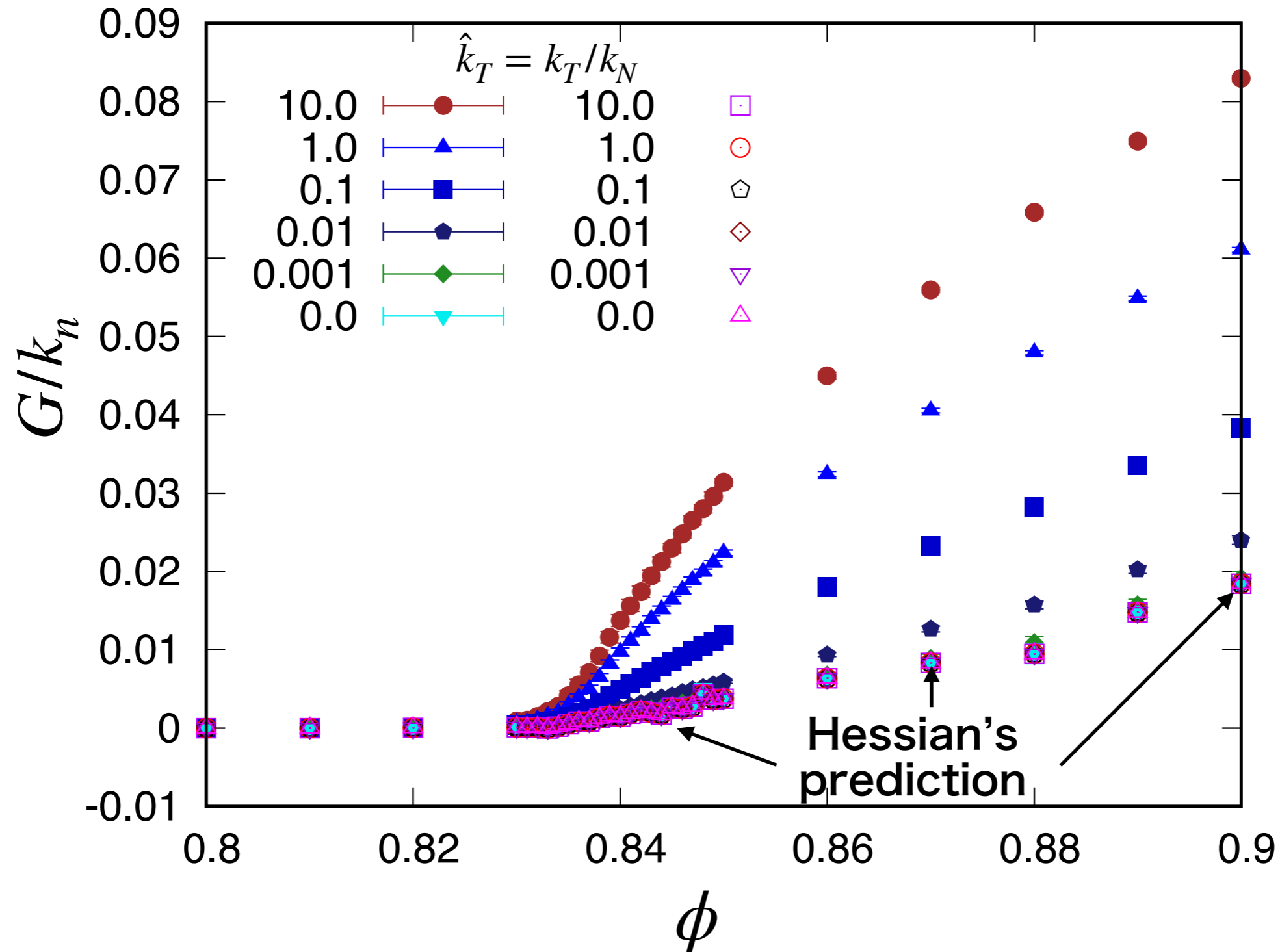
$$\left| \frac{du}{d\gamma} \right\rangle = \sum_n \frac{\langle n | \Xi \rangle}{\lambda_n} |n\rangle \quad \dots \quad (3)$$

Can we predict G from initial information
by using Eqs. (2) & (3)?

Non affine displacement $k_t = 0.001$



ϕ -dependence for $0 \leq k_t/k_n \leq 1.0$



Hessian's approach predicts G at $\hat{k}_T = 0.001$.

We have to consider the tangential part for $k_T > 0.01$.

Summary

Frictional amorphous solids under quasi-static shear are analyzed using the Jacobian.

Density of state $D(\omega_r)$ in the limit $\gamma \rightarrow 0$

- As k_T increases, low frequency part moves high frequency region

Shear modulus G in the limit $\gamma \rightarrow 0$

- Jacobain's representation can reproduce G .
- Hessian's approach predict G for $k_T \leq 0.001$.

Future work

- Expanding non affine displacements $u_i^\alpha(0)$ by eigenfunctions of Jacobian

