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Minimal Model of Stochastic Athermal Systems: Origin of Non-Gaussian Noise

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Outline of my talk

Background

Experimental development for small systems

□Why the Langevin Eq. is important in physics?

□Toward the non-Gaussian type Langevin Eq.

 Main 1: Systematic derivation of non-Gaussian Langevin Eq. & application to granular physics

KK, T.G. Sano, T. Sagawa, H. Hayakawa, Phys. Rev. Lett. **114**, 090601 (2015)

 Main 2 : Full-order solution of non-Gaussian Langevin Eq. with non-linear friction

KK, T.G. Sano, T. Sagawa, H. Hayakawa, J. Stat. Phys. **160**, 1294 (2015)

Experimental development: Quantitative description of fluctuation



Brownian motion: The motion of a small tracer in water

Precise observation of fluctuation (e.g., instantaneous velocity)

 Thanks to the experimental development

Modeling dynamics of small systems is an important issue

Minimal model of the dynamics of a small bead: the Langevin Equation



Fundamental equation for a small bead in water (μm)
 Applicable to physics, chemistry, biology, economics
 Basis toward Thermodynamics for small systems

Why is the Langevin Equation important for mesoscopic systems?



Derivation of the Langevin Equation: the system size expansion (SSE)

Weak coupling

Bath

 $d\hat{v}$

 $= \varepsilon \hat{\eta}(t; \hat{v})$

•••small parameter

 $\hat{\eta}(t; \hat{v})$ · · · Markov jump noise

- \blacklozenge Large system size limit (i.e., Ω-expansion)
 - A single stochastic bath described by Markov jump noise
 - \rightarrow Weak coupling (e.g., ε =mass ratio $\propto 1/\Omega$)
 - Universality in the weak coupling limit

Utilizing the kinetic theory and this expansion, the Langevin Eq. can be derived microscopically.

Example of the System Size Expansion (SSE): Rayleigh Piston



$$\frac{\partial P(V,t)}{\partial t} = \rho S \int_{-\infty}^{\infty} dv_x |v_x - V| \times$$

 $\{P(V',t)\phi_{\rm eq}(v'_x) - P(V,t)\phi_{\rm eq}(v_x)\}$



- Piston's motion in rarefied gas (linearized Boltzmann Eq.)
 - Markov jump process
 - Collision→discontinuous velocity jump of Piston
 - Strong environmental correlation (not even white noise)
 - $V = \text{large} \rightarrow \text{energy outflow to gas}$
 - $V = \text{small} \rightarrow \text{energy inflow from gas}$
- Massive piston limit ($\varepsilon \equiv \sqrt{m/M} \ll 1$)
 - 1. Correlation is renormalized only into viscosity
 - 2. Fluctuation is reduced to white noise
 - 3. Fluctuation is reduced to Gaussian (the CLT)

My interest: Athermal fluctuation Non-Gaussian Langevin Eq.



The aim of this talk



Main 1: Microscopic derivation of NGL Eq.

- 1. Systematic Derivation to leading order
- 2. Application to a granular system
- 3. What does non-Gaussianity means?
- Main 2 : Analytical simplicity
 - . NGL Eq. with non-linear friction
 - 2. Steady distribution for non-linear systems
 - 3. Full-order perturbative solution

NGL Eq. has universality & simplicity, which is required as a minimal model.

Main 1: Asymptotic derivation of NGL Eq.



$$\frac{d\hat{v}}{dt} = \hat{F}_T(t;\hat{v}) + \hat{F}_A(t;\hat{v})$$

$$\begin{cases} \hat{F}_T(t;\hat{v}) = -\gamma \hat{v} + \sqrt{2\gamma T} \hat{\xi}^{\mathrm{G}} \\ \hat{F}_A(t;\hat{v}) = \varepsilon \hat{\eta}_A(t;\hat{v}) \end{cases}$$

 $\gamma \cdots$ Thermal viscous coefficient $\gamma_A \cdots$ Athermal viscous coefficient = $O(\varepsilon)$ Idea: System attached to multiple baths (We apply the SSE twice)

Assumption

- **1**. Weak coupling : $\varepsilon \to 0$
- **2**. Coexistence of both noise : $\,T=arepsilon^2\mathcal{T}\,$

ε-independent

- 3. Large thermal viscosity: $\gamma \gg \gamma_A \iff \gamma$ is ε -independent
- ◆Assumption 1→Environmental correlation disappear (Reduction to white noise)
- \diamond Assumption 3 \rightarrow the CLT is violated



The NGL Eq. is derived systematically to leading order approximation

Separation of origins of the fluctuation and dissipation

A SINGLE BATH (GAUSSIAN)



Expansion for a single bath

The same origin in terms of the fluctuation and dissipation

DOUBLE BATH (NON-GAUSSIAN)



Expansion for double baths

 Different origins in terms of the fluctuation and dissipation

 Fluctuation irrelevant to relaxation becomes non-Gaussian noise



Example: Granular rotor (model)



A non-eq. Rayleigh Piston Linearized Boltzmann Eq. $\frac{\partial P(\omega, t)}{\partial t} = \gamma \left[\frac{\partial}{\partial \omega} \omega + \frac{T}{I} \frac{\partial^2}{\partial \omega^2} \right] P(\omega, t)$ $+\int_{-\infty}^{\infty} dy [P(\omega - y, t)W(y; \omega - y) - P(\omega, t)W(y; \omega)]$ ε-independent Assumption **1.** Weak coupling: $\varepsilon \equiv m/M \ll 1$ 2. Coexistence of both noise: $T = \varepsilon^2 T$ 3. Strong thermal viscosity : $\gamma \gg \gamma_A$ $\frac{d\hat{\Omega}}{dt} = -\gamma\hat{\Omega} + \sqrt{2\gamma T}\hat{\xi}^{\mathrm{G}} + \hat{\xi}^{\mathrm{NG}}, \ \hat{\Omega} \equiv \frac{\hat{\omega}}{\epsilon}$

Rotor's steady distribution



Results based on the MD is presented in T.G. Sano's poster "No. 52." • When the granular velocity dist. is exponential: $\phi(v) \propto e^{-v/v_0}$

• The exact distribution of the rotor's angular velocity Ω

$$\mathcal{P}_{\rm SS}(\tilde{\Omega}) = \int_{-\infty}^{\infty} \frac{ds}{2\pi} \frac{e^{[-is\tilde{\Omega} - v_0 s^2/\tilde{v}(1+s^2)]}}{(1+s^2)^{3v_0/2\tilde{v}}}$$

Numerical data are consistent with our result but not with the Gaussian approximation

Can we extract information from the fluctuation?

- Fluctuation includes some useful information (Fluctuation dissipation theorem: 2nd cumulant=temperature)

Isotropic granular rotor

•Isotropic granular velocity dist. $\phi(v)$

• Rotor's dist. function $P_{SS}(\Omega) \Leftrightarrow$ Granular dist. $\phi(v)$

$$\phi(v) = \int_0^\infty \frac{ds}{\pi |v|} \left[a - \frac{bs^2}{2} - cs^3 \frac{d}{ds} \log \tilde{P}_{SS}(s/F_g) \right] \cos(sv)$$

$$\tilde{P}_{SS}(s) \cdots \text{Fourier representation of } P_{SS}(\Omega), \quad a, b, c, F_g \cdots \text{constants}$$

Numerical demonstration of inverse estimation



• Inverse estimation of the granular dist. $\phi(v)$ from the rotor's steady dist. $P_{SS}(\Omega)$

 Microscopic information of the environment can be inferred from the observation of the tracer (rotor)

Conclusion of Main 1



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Main 2: Analytical solution of NGL. Eq.

$$\frac{d\hat{V}}{dt} = -F(\hat{V}) + \hat{\xi}^{\text{NG}} \qquad \text{Solution:} P_{SS}(V) = ??$$

◆ Main 1: Microscopic derivation of the NGL Eq.
 → We next solve the NGL Eq. in terms of the steady dist.

Main 2 : Perturbative formulation

- 1. Develop a general & perturbative framework for an arbitrary non-linear NGL Eq. for steady distribution
- 2. Full-order solution & its physical meaning (Diagrammatical rep.)



$$\begin{aligned} \frac{d\hat{V}}{dt} &= -F(\hat{V}) + \hat{\xi}^{\mathrm{NG}} \left[\text{Transition rate } W(Y) \right] \\ & \frac{\partial}{\partial v} F(V) P_{\mathrm{SS}}(V) + \int_{-\infty}^{\infty} dY W(Y) \left\{ P_{\mathrm{SS}}(V-Y) - P_{\mathrm{SS}}(V) \right\} = 0 \\ & \left[\frac{is}{2\pi} \int_{-\infty}^{\infty} du \tilde{F}(s-u) \tilde{P}(u) = \Phi(s) \tilde{P}(s) \right] \end{aligned}$$

◆ Master Eq. for the steady dist. (Integro-differential Eq.)
□ $\tilde{P}(s), \tilde{F}(s)$ •••Fourier rep. of the steady dist. & friction
□ $\Phi(s) = \int dY(e^{isY}-1)W(Y)$ •••Cumulant function for the non-Gaussian noise

Construction of the perturbative solution
 & Clarification of the meaning of all the perturbative terms





 \bullet In the large friction limit \rightarrow Analytically solvable?

$$F(V) = \gamma f(V) \qquad \begin{array}{l} \gamma \gg 1 \Longleftrightarrow \mu \equiv 1/\gamma \ll 1 \\ \tilde{P}(s) = 1 + \sum_{n=1}^{\infty} \mu^n \tilde{a}_n(s) \end{array}$$

 $\phi \mu \ll 1 \rightarrow$ The typical number of kicks during relaxation decreases $\rightarrow n$ th-order perturbation corresponds to the *n* times kicks process?

Full-order formal solution

$$\mathcal{I}[s;h(s')] = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{dV(e^{isV}-1)}{f(V)} \int_{-\infty}^{\infty} ds' e^{-is'\mathcal{V}} \frac{\Phi(s')}{is'} h(s')$$

$$\tilde{P}(s) = 1 + \mu \mathcal{I}[s; \mathbf{1}(s')] + \mu^2 \mathcal{I}^2[s; \mathbf{1}(s')] + \dots = [1 - \mu \mathcal{I}]^{-1}[s; \mathbf{1}(s')]$$

We have constructed the full-order perturbative solution

Too formal to be understood...
 (We have not used the probabilistic property)

We next transform the terms to clarify their probabilistic meanings...

The 1st-order solution (1): Probabilistic representation

$$\tilde{P}(s) = 1 + \int_{-\infty}^{\infty} dY W(Y) \int_{0}^{Y} \frac{\mu dV}{f(V)} [e^{isV} - 1] + O(\mu^2)$$

◆ The 1st-order solution is represented with the transition rate W(Y).
 ◆ W(Y) appears only once → Effect of a trajectory with single kicks?



The 1st-order solution (2): Independent kick model (IKM)



Phenomenological picture (IKM): Effect of a single kick during relaxation

• Derivation: The trajectory is assumed to be decomposed into single-kick shapes, and we calculate an average of an arbitrary quantity h(V)

$$\begin{split} \langle h(\hat{V}) \rangle_{\mathrm{SS}} &= \lim_{T \to \infty} \frac{1}{T} \int_0^T dt h(\hat{V}(t)) \simeq \lim_{T \to \infty} \frac{1}{T} \sum_{i=1}^{\hat{N}(T)} \int_0^{\tau^*(\hat{Y}_1)} dt h(V(t;\hat{Y}_1)) \\ &\simeq \int_{-\infty}^\infty dY W(Y) \int_0^{\tau^*(Y)} dt h(V(t;Y)) \end{split}$$

The 1st-order solution (3): Steady distribution for the IKM



This rep. is completely equivalent to the 1st-order solution.
Equivalence between the 1st-order solution & IKM

The 1st-order solution (4): Diagrammatic representation



The 1st-order solution = Single-kicks trajectory (IKM)

Introduction of a diagram

$$(\bullet) = \int_{-\infty}^{\infty} dYW(Y) \int_{0}^{Y} \frac{\mu dV}{f(V)} [e^{isV} - 1]$$

$$(\bullet) = \int_{-\infty}^{\infty} \tilde{P}(s) = 1 + (\bullet)$$

$$(\bullet) = \int_{0}^{Y_{1}} \frac{V_{1}}{V_{1}}$$





Example of the 1st-order solution: Symmetric Poisson + Coulomb friction







Granular rotor under dry friction : Derivation of nonlinear NGL Eq.



Granular rotor under dry friction : The 1st-order solution





- For $\phi(v) = e^{-v/v_0} / 8\pi v_0^3$
- $\blacklozenge\beta^{-1}\ll 1 \Longleftrightarrow \mu \ll 1$
- Numerical validation
- Valid for the range $|\Omega| \le 3.5$ (Only the single kick effect is taken...)

$l \bullet l = 0$	•	$\beta^{-1} = 0.035$
• $M = 0.01$	٠	$\Omega_w^* \simeq 3.5$
• $\tilde{\gamma} = 200$	•	$w = \sqrt{12}$

Conclusion of Part 2: Analytical solution of non-linear NGL Eq.



oulomb friction

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Summary of this talk

MAIN 1: MICROSCOPIC DERIVATION OF NGL EQ. (KINETIC THEORY)

Perturbative derivation of NGL Eq.

- 1. Weak coupling
- 2. Coexistence of thermal & athermal flucs.
- 3. Strong thermal dissipation
- Application to granular rotor
- Information in non-Gaussianity
 Microscopic info. of environment (i.e., granular velocity dist.)

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PART 2: ANALYTICAL SOLUTION OF NGL EQ. WITH NON-LINEAR FRICTION

- Full-order perturbative formula for the steady dist. under nonlinear friction
- High-order terms corresponds to multiple kicks during relaxation
- Diagrammatic representation
- Application to granular rotor under Coulomb friction
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Universality & Analytical simplicity of NGL Eq.